ASX ANNOUNCEMENT
27 July 2023

ASX:CMM

QUARTERLY EXPLORATION & ANNUAL RESOURCE/RESERVE UPDATE

Highlights

Exploration - Mt Gibson Gold Project (MGGP)

- A further 21,203 metres of RC resource definition and extensional drilling was completed at the MGGP since the last update in April 2023.
- Assays received from 99 resource definition holes (19,637 metres) since the last update continue to return exceptional results within and extensional to the current Mineral Resource Estimate (MRE) including:

  Outside current resource

  - *17 metres @ 3.08g/t from 255 metres*
  - *31 metres @ 1.24g/t from 304 metres*
  - *4 metres @ 5.77g/t from 37 metres*
  - *27 metres @ 1.71g/t from 227 metres*
  - *12 metres @ 2.81g/t from 227 metres*
  - *9 metres @ 3.70g/t from 77 metres*

  Within current resource

  - *26 metres @ 4.11g/t from 191 metres*
  - *21 metres @ 4.33g/t from 244 metres*
  - *37 metres @ 2.33g/t from 177 metres*
  - *20 metres @ 5.11g/t from 238 metres*
  - *9 metres @ 9.90g/t from 45 metres*
  - *18 metres @ 4.48g/t from 33 metres*

- A total of 334 aircore holes for 11,074 metres were completed over the historic mineralised heap leach dump within the MGGP mining centre. Encouraging results were returned including:

  - *5 metres @ 8.36g/t from 12 metres*
  - *24 metres @ 0.68g/t from 1 metre*
  - *17 metres @ 1.04g/t from 0 metres*
  - *19 metres @ 0.85g/t from 2 metres*

- The above results and further drilling in the September 2023 quarter will be used to update the MGGP MRE and Ore Reserve Estimate in the December 2023 quarter.
- 12,000 metre regional AC drilling programme to commence across near mine exploration targets in the September 2023 quarter.

Exploration - Karlawinda Gold Project (KGP)

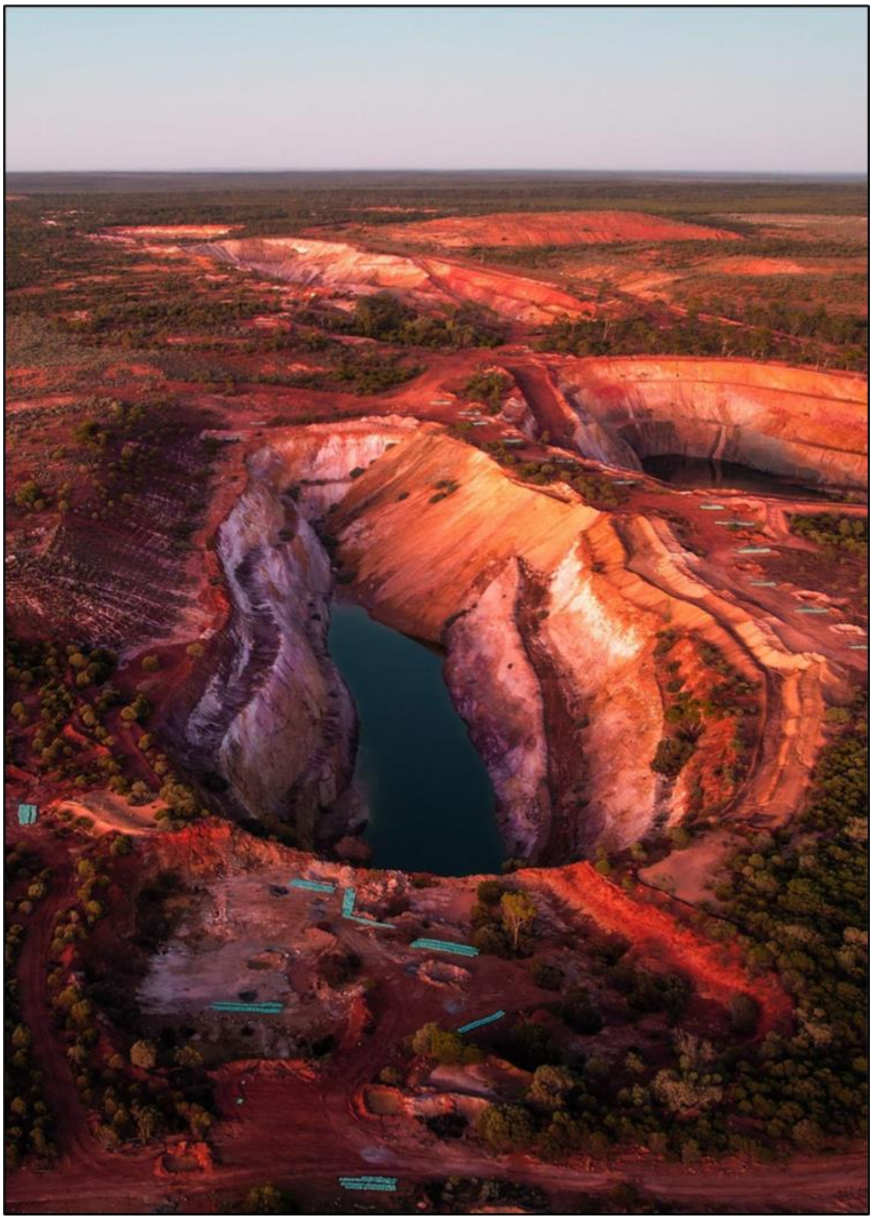
- RC drilling at the newly identified Berwick prospect, 2 kilometres east of the Bibra open pit, continues to report near surface gold mineralisation over a 500 metre strike length.
- A 30 hole (4,768 metres) infill RC drill programme was completed at the Berwick prospect following up previous reported intercepts to facilitate a maiden resource estimate. Significant results received included:

  - *3 metres @ 7.78 g/t from 116 metres*
  - *3 metres @ 7.37 g/t from 45 metres*
  - *9 metres @ 1.80 g/t from 65 metres*
  - *1 metre @ 26.76 g/t from 47 metres*
  - *6 metres @ 3.47 g/t from 50 metres*
  - *3 metres @ 5.34 g/t from 39 metres*

- A total of 22 RC holes for 4,680 metres of infill and extensional drilling was completed at the Vedas prospect located 5 kilometres east of the Bibra open pit with all results pending.
- A 15,000 metre first pass regional AC drilling programme commenced during the quarter across the Jamie Well East, Donomore and Forfar prospects, with all assays pending.

Annual Resource and Reserve Update

- KGP Ore Reserves (ORE) updated only for mining depletion in the nine months to 31 March 2023. The updated KGP ORE of 1,247,000 ounces (2022: 1.34 million ounces) is a modest increase of 5,000 ounces after accounting for mining depletion.
- KGP MRE also updated only for mining depletion in the nine months to 31 March 2023. The updated MRE is 2,228,000 ounces (2022: 2.29 million ounces), again a modest increase of 40,000 ounces after accounting for mining depletion.
- MGGP MRE remains unchanged from the 2,755,000 ounces reported 7 November 2022.
- MGGP ORE remains unchanged from the Maiden ORE reported on 19th April 2023.
- Update to MGGP MRE and ORE expected in the December 2023 quarter to include strong assay results returned from in excess of 50,000 metres of infill and extensional drilling completed since the November 2022 MRE.
- Capricorn group MRE updated to 4,983,000 ounces (2022: 5.05 million ounces) and ORE updated to 2,697,000 ounces (2022: 2.79 million ounces).



Mt Gibson Gold Project historical open pit

Exploration - Mt Gibson Gold Project

Near mine RC Drilling

Exploration activities at the MGGP during the period focussed on progressing the extensional and infill resource drilling that commenced in January 2022. A total of 21,203 metres (110 holes) have been drilled since the last update in April 2023 taking the total RC drilling to date at the project to 163,944 metres (1,078 holes).

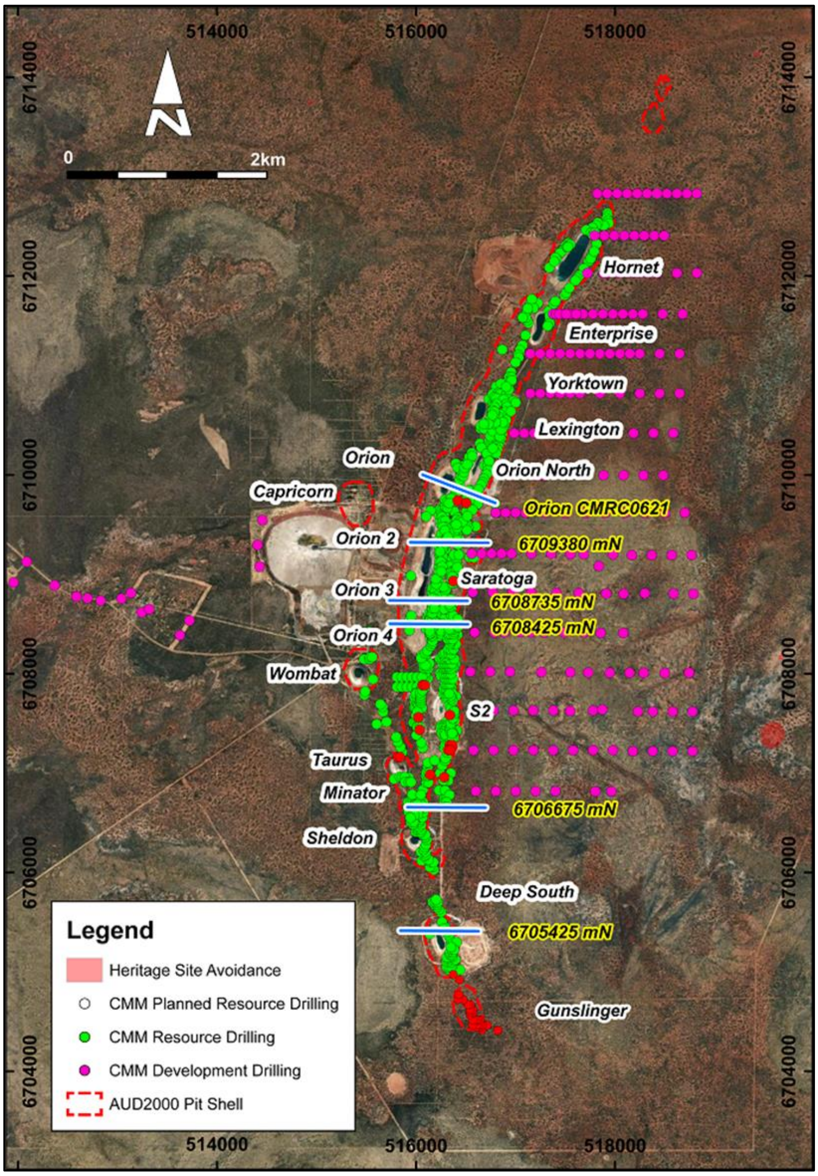


Figure 1. Completed drilling over the MGGP 8km long mine trend along with planned current resource drillng, first pass western exploration holes and sterilisation drilling.

Assays have now been received from the first 771 holes from the ongoing resource definition drilling programme. A total of 1,933 holes for 191,891 metres of resource, regional exploration and mine development drilling has been completed at the MGGP since January 2022. Assays received since the last update continue to return very encouraging results, including:

Hole ID	Easting	Northing	From (m)	Depth (m)	Width	Grade (g/t Au)
CMRC0606	516811	6710588	194	196	2	10.69
CMRC0607	516776	6710351	134	136	2	12.48
CMRC0607*	516741	6710366	227	239	12	2.81
CMRC0610	516742	6710276	109	110	1	33.70

CMRC0613	516736	6710242	43	51	8	4.95
CMRC0614	516726	6710226	74	82	8	3.77
CMRC0615	516712	6710241	144	146	2	14.06
CMRC0616*	516714	6710243	170	174	4	5.87
CMRC0616*	516698	6710250	196	214	18	1.52
CMRC0621	516301	6709869	153	174	21	1.96
CMRC0621	516283	6709880	177	214	37	2.33
CMRC0622	516198	6709602	109	119	10	3.32
CMRC0624	516172	6709410	180	186	6	11.81
CMRC0624*	516151	6709411	227	254	27	1.71
CMRC0625*	516270	6709406	37	42	5	5.77
CMRC0625	516181	6709411	223	235	12	5.84
CMRC0625*	516165	6709412	269	282	13	1.54
CMRC0626	516180	6709376	244	265	21	4.33
CMRC0627	516285	6709349	33	51	18	4.48
CMRC0627	516275	6709348	54	68	14	1.45
CMRC0627	516179	6709355	238	258	20	5.11
CMRC0628	516285	6709326	20	42	22	1.66
CMRC0628	516178	6709336	233	255	22	1.42
CMRC0630*	516035	6708859	226	228	2	10.60
CMRC0633	516066	6708707	187	198	11	2.63
CMRC0639	516223	6708426	84	90	6	9.53
CMRC0643	516338	6708078	56	60	4	5.43
CMRC0645	516307	6708030	100	108	8	2.90
CMRC0650*	516294	6707877	111	120	9	2.84
CMRC0657	516273	6707648	144	149	5	5.04
CMRC0660	516319	6707479	88	90	2	11.95
CMRC0665	516167	6709306	206	216	10	3.95
CMRC0665*	516148	6709306	255	272	17	3.08
CMRC0666	516279	6709304	25	37	12	1.82
CMRC0666	516173	6709307	235	253	18	1.96
CMRC0667	516286	6709325	61	84	23	1.17
CMRC0667	516186	6709331	260	276	16	1.93
CMRC0669	516063	6708794	207	219	12	3.45
CMRC0670	516061	6708742	191	217	26	4.11
CMRC0671	516149	6708681	24	39	15	2.05
CMRC0671	516059	6708686	187	198	11	2.38
CMRC0673	516149	6708635	39	50	11	3.68
CMRC0675	515996	6707730	82	90	8	7.94
CMRC0675	515982	6707730	110	114	4	6.47
CMRC0675	515978	6707730	117	121	4	5.15
CMRC0677	515984	6707784	107	120	13	1.97
CMRC0681	515933	6706538	40	63	23	1.79
CMRC0689	516808	6710387	89	95	6	4.59
CMRC0689	516799	6710390	110	115	5	6.26
CMRC0693*	516267	6706657	77	86	9	3.70
CMRC0693*	516253	6706658	105	115	10	2.13
CMRC0696	515950	6706638	84	95	11	5.39
CMRC0697	515990	6706637	39	44	5	5.62

CMRC0698	515964	6706586	75	82	7	6.96
CMRC0699	515994	6706587	45	54	9	9.90
CMRC0700	516209	6705439	101	108	7	9.48
CMRC0702	516223	6708429	40	42	2	14.22
CMRC0702*	516061	6708441	304	335	31	1.24
CMRC0703	516062	6708484	229	257	28	0.95

significant intercepts outside the current 2022 MRE

A comprehensive table of significant results is included in Appendix 2.

Results of this additional drilling will form the basis to update the 2.755 million ounce MRE targeted for completion in the December 2023 quarter.

Current and previously reported drilling at the depth extremities of the resource optimisation shells (where historic drill density is broader spaced) and below them has returned results consistent with Capricorn's geological interpretations of mineralisation location, widths and grade tenor. Drilling across the project to date indicates that mineralisation remains open down dip and along strike to the north and south with multiple stacked lodes intersected.

S2, Lexington Waste Dump and Orion North trend

Drilling on unmined areas Orion, S2, Saratoga and Deep South trends continues to define zones of high-grade within and outside the updated 2022 resource shell (refer Figure's 2-7). It is ecouraging that early staged drilling at the unmined Saratoga and S2 South trends has identified open near surface mineralisation with the potential to improve the overall economics of the project.

Cross Sections

The plan in Figure 1 above shows the drilling activity from the infill and extensional RC programme and the location of the following long and cross sections.

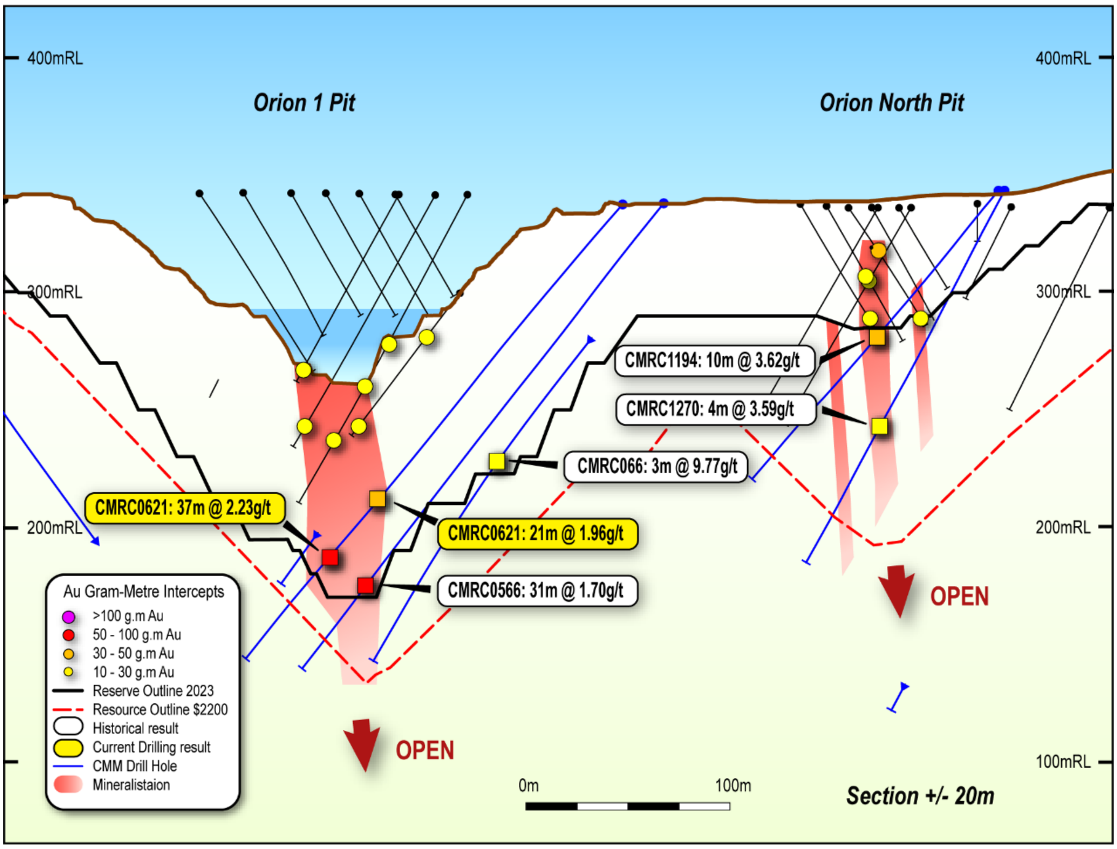


Figure 2. Orion 1 and Orion North Section with significant broad mineralisation intersected.

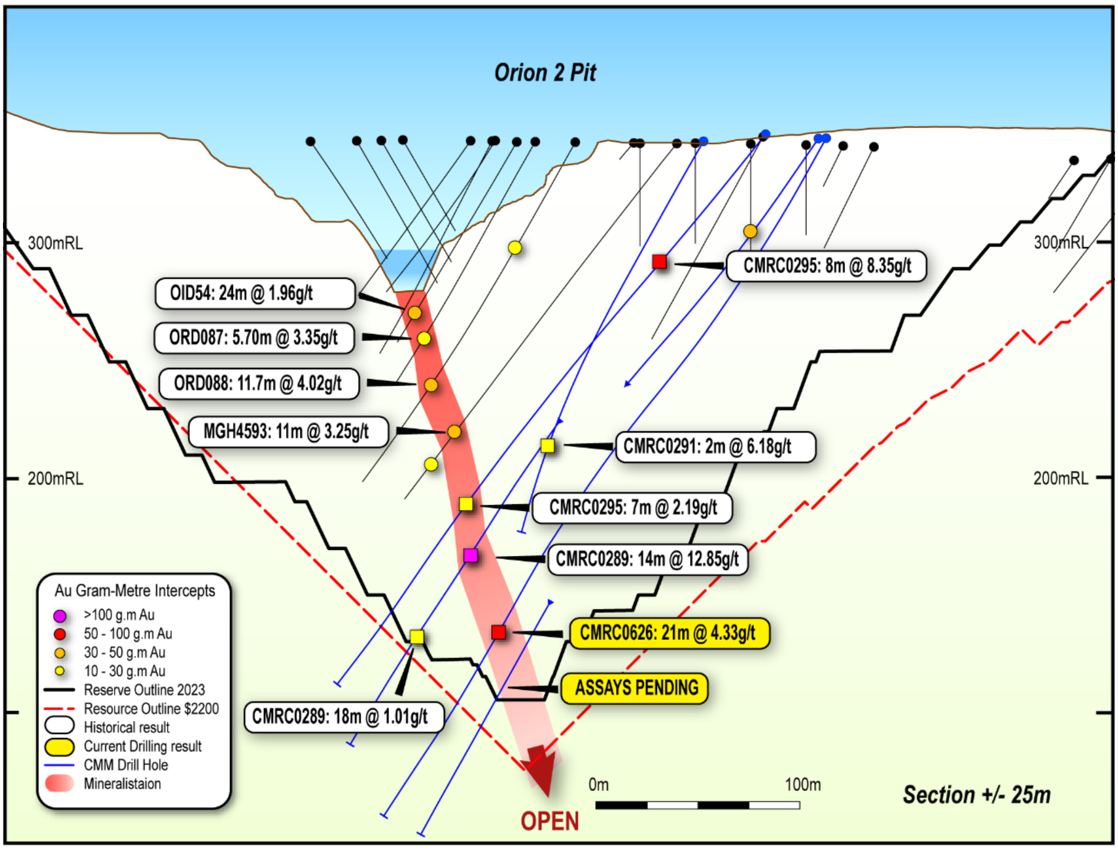


Figure 3. Orion 2 with significant broad high-grade mineralisation open at depth.

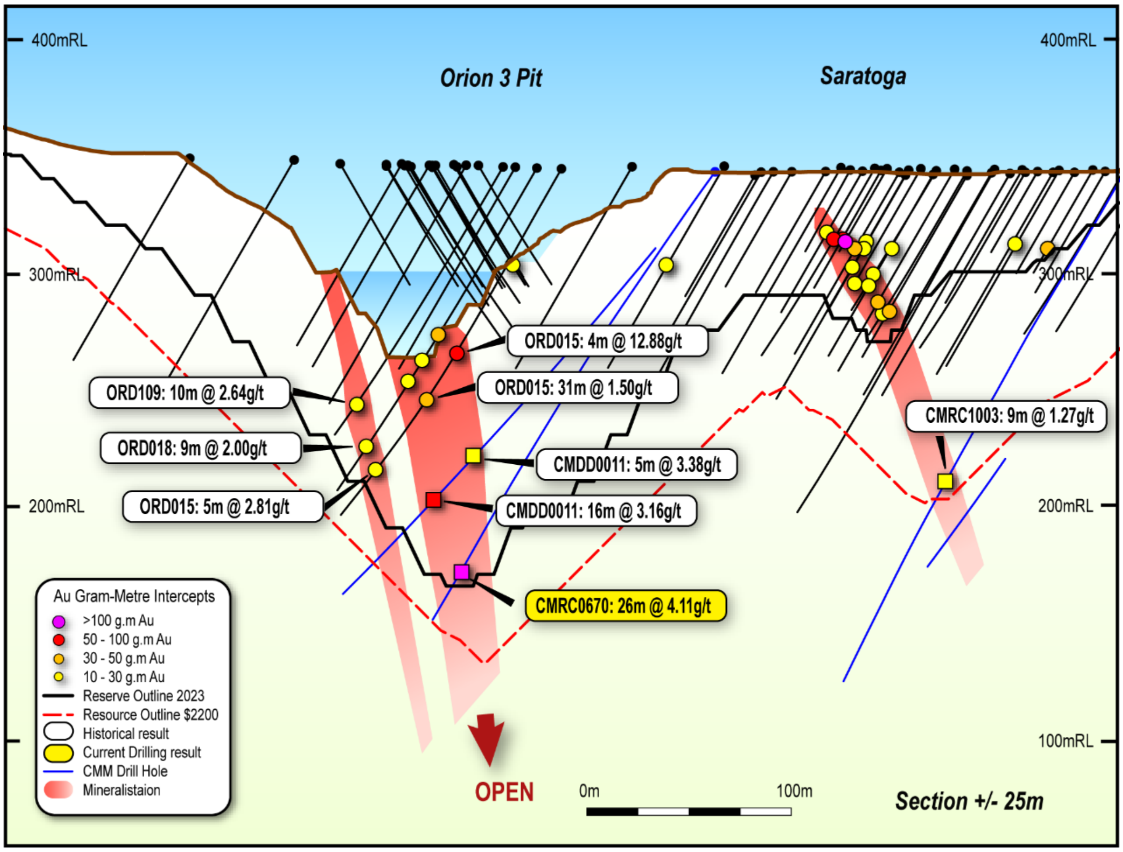


Figure 4. Orion Section with significant broad high-grade mineralisation intersected.

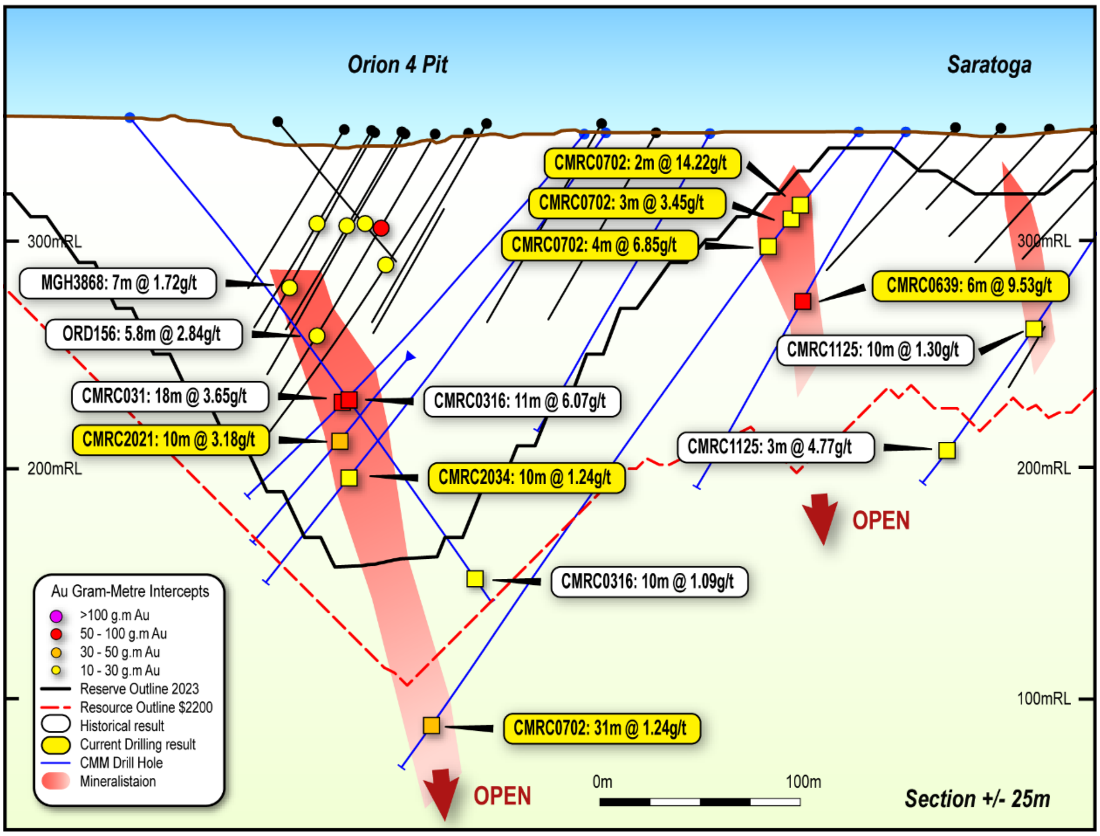


Figure 5. Orion 4 and early-stage near surface Saratoga drilling Section with significant broad high-grade mineralisation intersected outside of the current A$1,900/oz Reserve and A$2,200/oz Resource Outline.

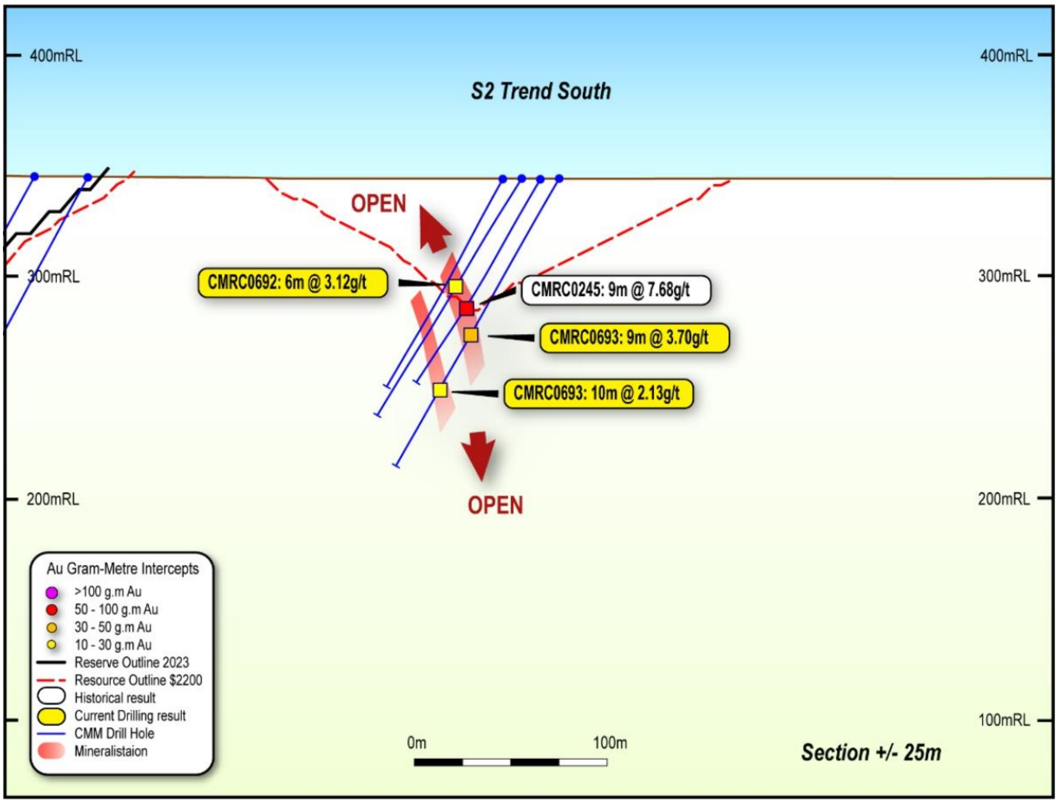


Figure 6. Early-stage near surface drilling along the S2 Trend South Section with significant broad high-grade mineralisation intersected outside of the current A$1,900/oz Reserve and A$2,200/oz Resource Outline.

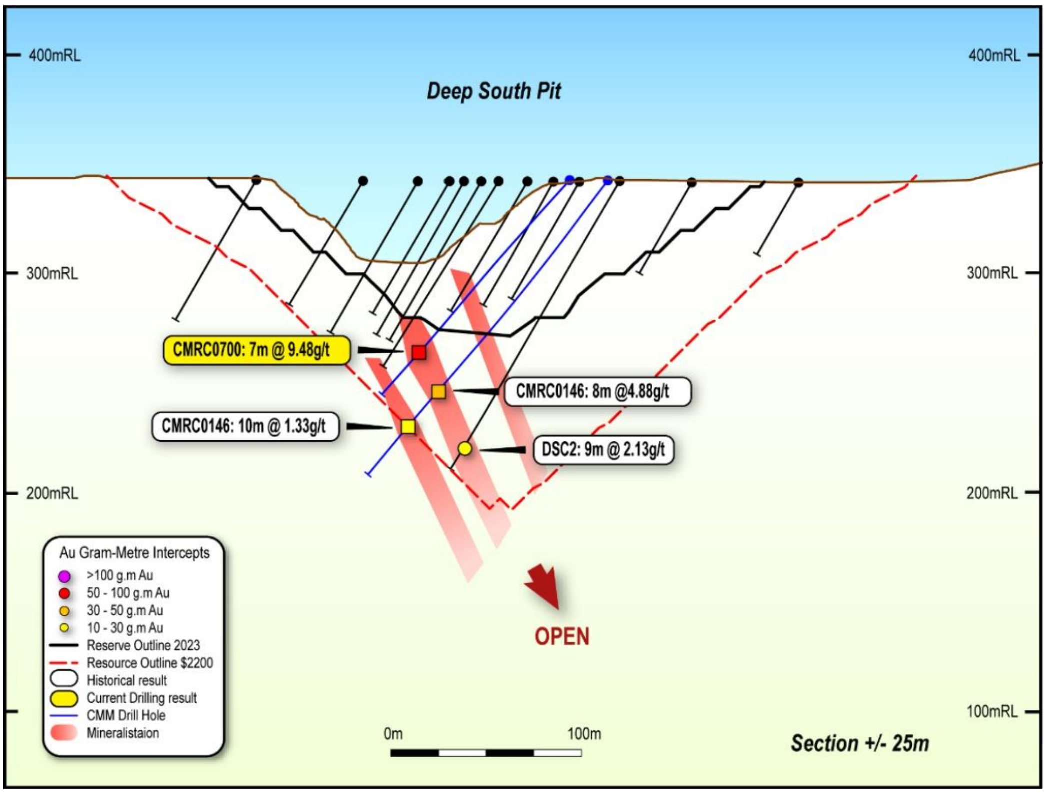


Figure 7. Deep South Section with significant broad high-grade mineralisation intersected outside of the current A$1,900/oz Reserve Outline

Heap Leach Dump Drilling

A 334 hole (11,074 metres) Aircore drilling programme that commenced in the March 2023 quarter was completed over an existing 4 million tonne historic heap leach dump at the MGGP.

The drilling was designed to increase confidence in gold distribution and enable segregation between ore and waste. The results will aid in any future maiden JORC compliant resource estimations. Significant results from this drilling are shown below:

Hole ID	Easting	Northing	From (m)	Depth (m)	Width	Grade (g/t Au)
CMHL111**	515472	6708715	0	17	17	1.04
CMHL119**	515517	6708877	3	9	6	2.12
CMHL120**	515528	6708878	9	14	5	2.78
CMHL141**	515806	6708886	21	23	2	5.94
CMHL151**	515820	6708766	1	25	24	0.68
CMHL155**	515798	6708707	1	16	15	0.84
CMHL161**	515641	6708735	12	17	5	8.36
CMHL167**	515562	6708731	2	21	19	0.85
CMHL232**	515704	6708897	8	21	13	0.90
CMHL274**	515665	6708784	9	13	4	3.33
CMHL278**	515577	6708741	10	24	14	0.74
CMHL297**	515680	6708757	0	8	8	1.47
CMHL303**	515580	6708753	6	21	15	0.72
CMHL319**	515761	6708790	15	28	13	0.87

MGGP heap leach dump.

Regional Exploration

All assays from the first pass Aircore drilling programme at the Outlaw prospect have now been received with no further significant results from those reported in April 2023. Encouraging zones of anomalous gold and pathfinders including Ag, Cu, and As associated with north east striking shear zones within amphibolite rocks have been identified at the prospect. A follow-up RC drilling programme is planned to commence in the September 2023 quarter.

A first pass 12,000m Aircore drill programme at the Mt Gibson and Wombat mine trends is also due to commence in the September 2023 quarter. The Wombat mine trend runs adjacent and parallel to the main Mt Gibson Mine trend. Based on review of historic downhole drill logging and geophysical data, the under explored target area (refer Figure 8) which includes the unmined Capricorn deposit has been identified as having a significant strike potential and geological and structural settings amenable to host further significant mineable deposits.

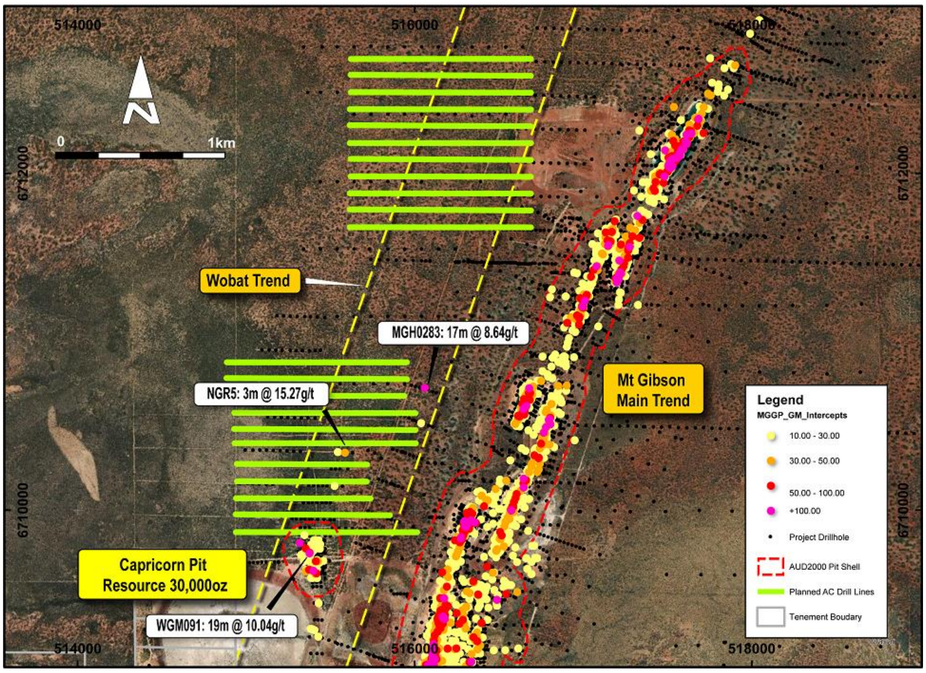


Figure 8. Planned Aircore lines and historic drill results parallel to the Main Mt Gibson mine trend and north of the unmined Capricorn deposit.

First pass drilling is also planned to target the southern extension of Mt Gibson mine trend which hosts the majority of the MGGP 2.755 million ounce MRE (refer Figure 9). Mineralisation is hosted within multiple sets of elongate lodes with strong strike continuity, which anastomose and pinch-swell along strike and to depth. The previously unmined target area sits along strike from the Deep South and Gunslinger deposits as shown below.

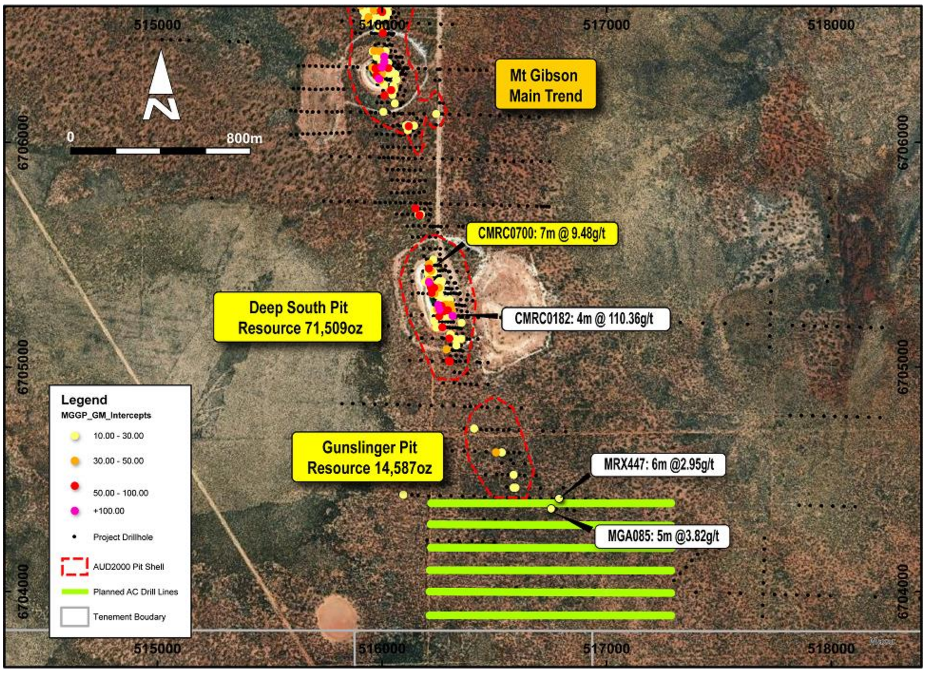


Figure 9: Planned Aircore lines and current Capricorn and historic drill intercepts south of the main Mt Gibson mine trend and Deep South and unmined Gunslinger deposits.

Both target areas represent a unique opportunity to discover economic deposits at surface in close proximity to current known MGGP gold reserves.

Karlawinda Gold Project

Near mine RC Drilling

In the June 2023 quarter, 60 RC holes for 11,841 metres were completed at the Berwick and Vedas prospects. The early success of the two programmes and proximity to the existing operations indicate the potential for both prospects to be developed as satellite resources (refer Figure 10). This phase of drilling focused on infilling previous intercepts which underpinned the mineral resource estimate. Vedas results are pending. Encouraging results at Berwick include:

Hole ID	Easting	Northing	From (m)	Depth (m)	Width (m)	Grade (g/t Au)
KBRC2013	206899	7367438	75	76	1	4.82
KBRC2013	206912	7367447	116	119	3	7.78
KBRC2017	207043	7367300	39	42	3	5.34
KBRC2019	206965	7367257	68	75	7	1.28
KBRC2021	207014	7367315	47	48	1	26.76
KBRC2022	206957	7367283	81	83	2	3.42
KBRC2025	206879	7367206	65	74	9	1.80
KBRC2030	207013	7367349	45	48	3	7.37
KBRC2031	206972	7367327	50	56	6	3.47
KBRC2032	206933	7367304	57	64	7	1.34
KBRC2032	206946	7367313	92	95	3	1.70
KBRC2034	206856	7367261	85	90	5	0.94
KBRC2034	206859	7367263	94	101	7	0.81
KBRC2036	206957	7367354	59	60	1	4.31

KBRC2040	207018	7367196	50	53	3	2.20
KBRC2044	206939	7367426	118	120	2	5.78
KBRC2046	206842	7367367	90	94	4	1.51
KBRC2047	206791	7367337	87	91	4	2.38
KBRC2048	206958	7367192	68	73	5	0.83
KBRC2049	206887	7367397	72	73	1	5.9
KBRC2049	206896	7367403	96	98	2	2.76

A comprehensive table of significant results is included in Appendix 2.

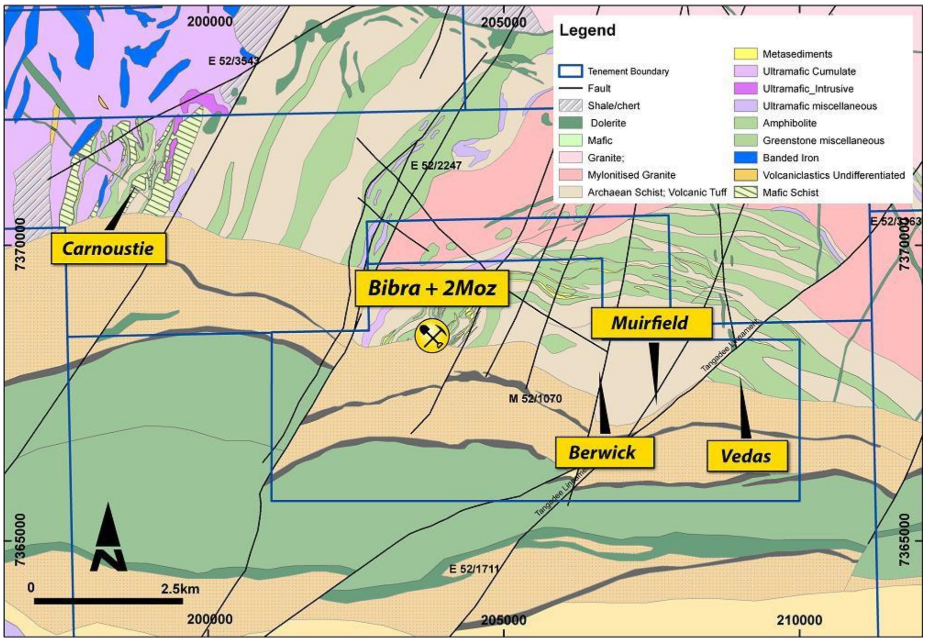


Figure 10. Karlawinda current near mine exploration targets.

Berwick Prospect

During the June 2023 quarter 35 RC holes for 6,387 metres were completed at the Berwick prospect situated approximately 2 kilometres east of the Bibra open pit (refer Figure 10). Previous drilling had identified near surface gold mineralisation over a 500 metre strike. Mineralisation is hosted by silicified bands within migmatite (composite rock found in medium and high-grade metamorphic environments) which appears to be controlled by folding and remains open down dip and along strike.

The latest drilling completed at the prospect infilled previous intercepts to advance the maiden resource estimate. Several promising results were returned from this programme including:

- *3 metres @ 7.78 g/t from 116 metres*
- *3 metres @ 7.37 g/t from 45 metres*
- *9 metres @ 1.80 g/t from 65 metres*
- *1 metre @ 26.76 g/t from 47 metres*
- *6 metres @ 3.47 g/t from 50 metres*
- *3 metres @ 5.34 g/t from 39 metres*

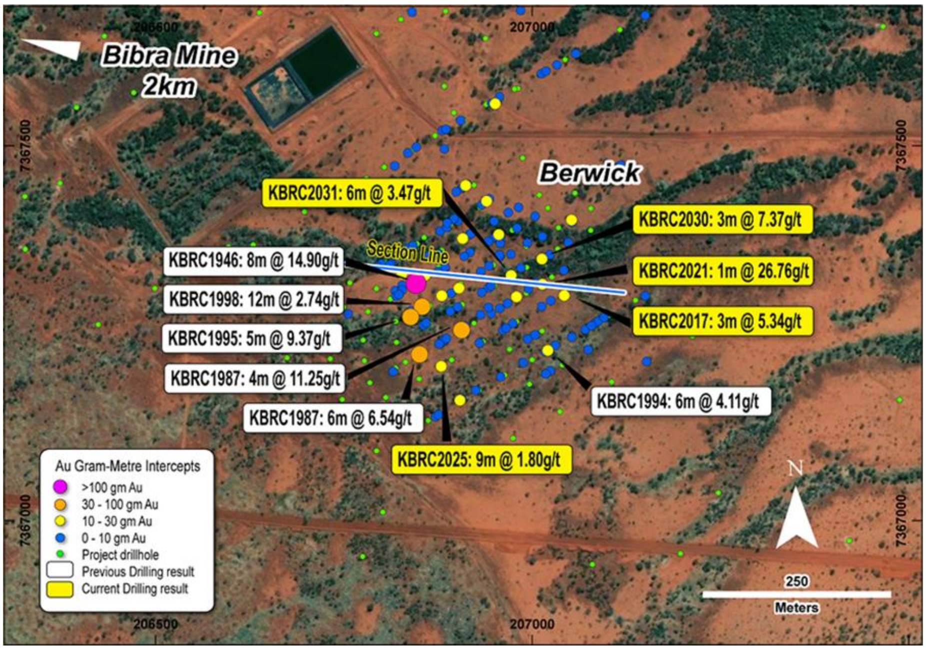


Figure 11. Drilling completed at the Berwick prospect .

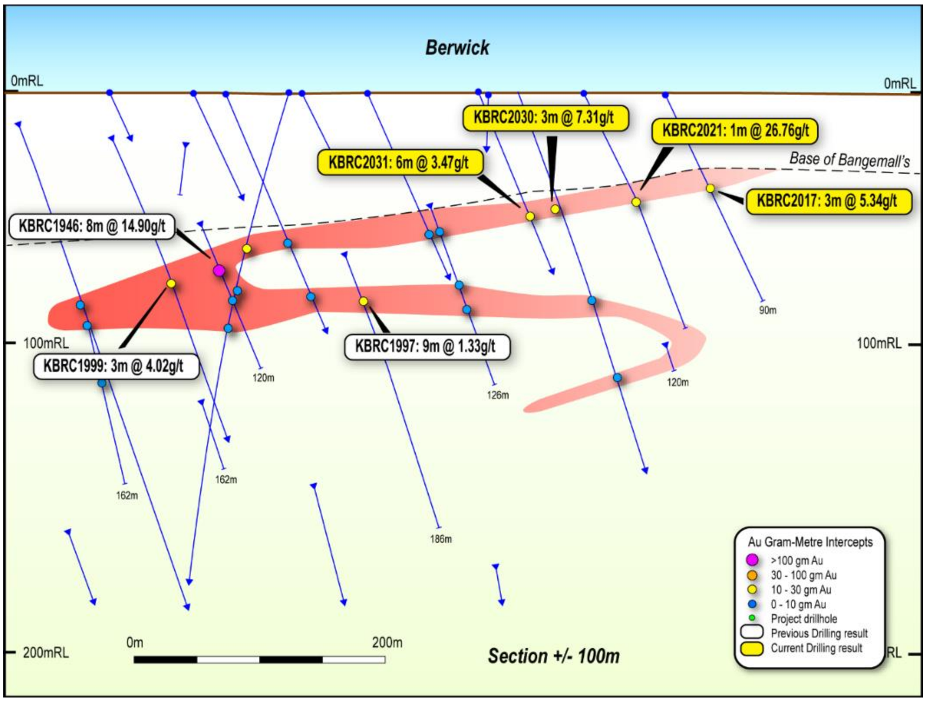


Figure 12: Berwick section with broad and high-grade mineralisation intersected.

Vedas

The Vedas prospect is located 5 km east of the Bibra open pit (refer Figure 10). Previous results confirmed gold mineralisation over a 400 metre strike within moderately north dipping zones of gold mineralisation analogous to the Bibra Deposit.

During the June 2023 quarter, a 25 hole (5,454 metres) infill and extensional RC drilling programme was completed over the prospect. The results from this programme are pending and will form part of a maiden resource estimate in due course.

A follow-up AC programme will commence in the September 2023 quarter testing for extensions of mineralisation following receipt of all assay results.

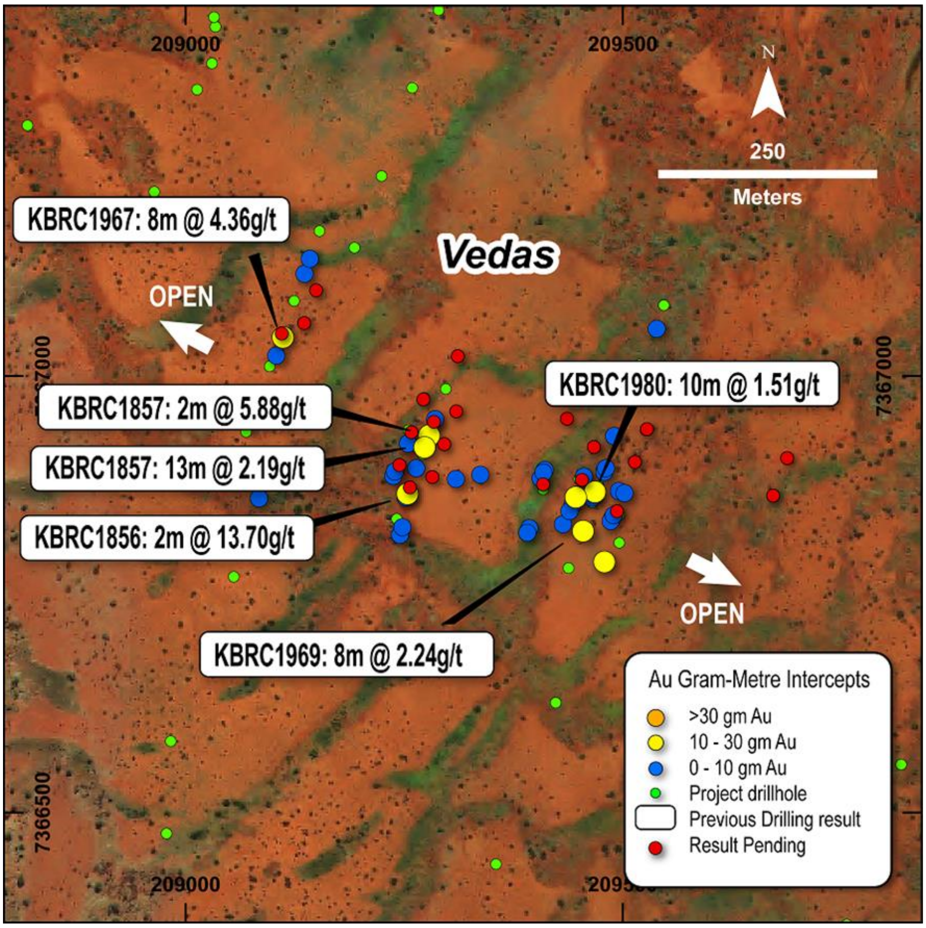


Figure 13. Drilling completed at the Muirfield-Vedas trend.

Regional Exploration

AC Drilling

During the quarter a 15,000 metre first pass regional AC drilling programme commenced across the broader KGP tenement package. First pass drilling was completed at Donomore and infill drilling at Jamie Well East and Forfar Prospects (refer figure 14). The project areas are situated proximal to either the Nanjilgardy Fault or the Sylvania Inlier and Pilbara Craton margin.

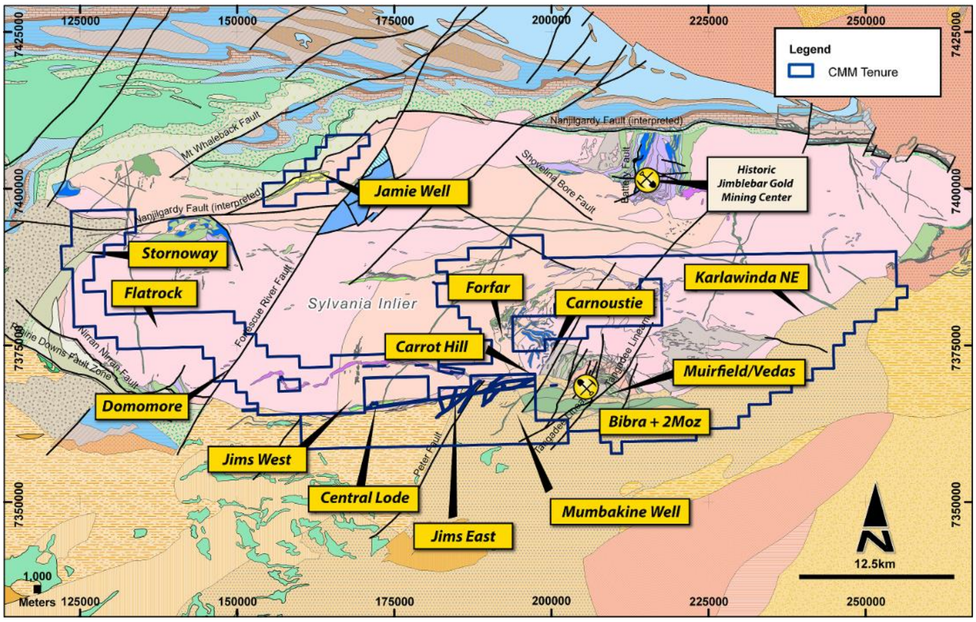


Figure 14. Karlawinda regional and near mine exploration targets

The Nanjilgardy Fault is a regional scale structure that is known to have controls on gold mineralisation in the Pilbara craton, including the Paulsens (ASX: BC8) and Ashburton (ASX: KZR) gold projects. Situated on the southern extents of CMM tenure, the Sylvania Inlier and Pilbara Craton margin is considered a high strain zone with high prospectivity for mineralising fluids with origins from igneous intrusions formed from partial melting of a mantle wedge or enriched fluid remobilisation through regional metamorphism. This Craton boundary is interpreted to play a significant role in the placement of ore forming fluids at the +2Moz Bibra gold deposit.

An AC drilling programme commenced at Donomore during the quarter with 114 AC holes for 6,387 metres completed. The prospect located along the Sylvania Inlier and Pilbara Craton margin, is crosscut by the regional scale Fortescue Fault and situated along strike from the historic Deadmans Flat mine, containing Au-bearing quartz veins. The programme is expected to be completed in the September 2023 quarter with all assays currently pending.

An infill program consisting of 99 AC holes for 4,437 m was completed at Jaime Well, 50 km northeast of Bibra. The program was focused along a low Au anomaly (best result, 4m @ 0.5 g/t from 16m in KBAC2617) trend from 2022 drilling and was successful in intersecting mineralisation indicators within mafics at the contact of shear zones. The program was completed at the end of June 2023 with all assays pending.

Carrot Hill is located 7 km NW of Bibra along the Karlawinda Thrust zone. An AC programme covering 7km^2 will be completed in July 2023. The programme will test coinciding gravity and anomalous high temperature soil pathfinders known to be associated with intrusion related gold systems (Au, As, Cu, Mo, Pb, W).

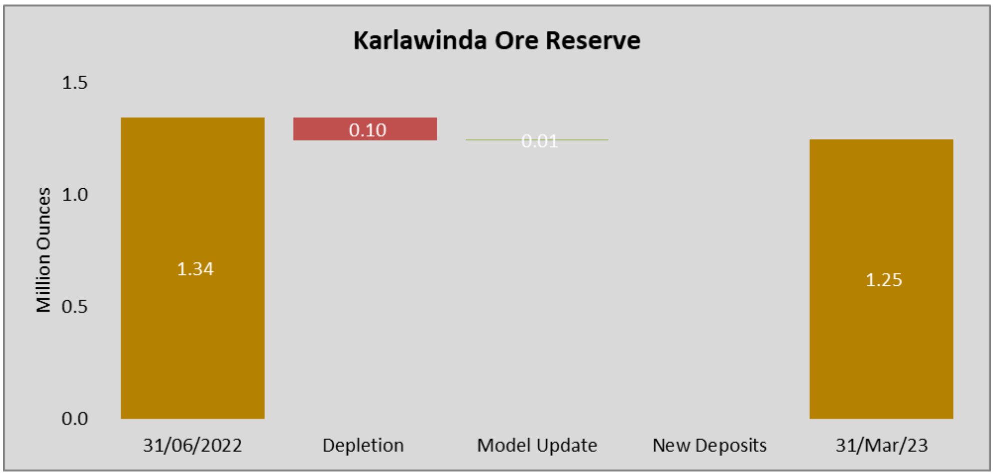
A soil sampling programme was completed on the Mumbakine Well tenement in the June 2023 quarter with 1,347 samples collected. Archaeological heritage surveys for drilling clearance began in June 2023, with broad spaced AC drilling planned to commence next quarter following receipt of all soil sample assay results. An initial 120 hole (5,000 metre) first pass AC programme on 100 x 200 metre spaced drill lines will focus on prospective targets at the Jims Vein and Central Zone prospects.

Ore Reserve Estimation Update – Karlawinda

The KGP ORE has been updated to reflect mining depletion at the Bibra open pit mining operation from the date of the last ORE released on 27 October 2022. The updated ORE also incorporates in pit drilling data from the date of the previous ORE into the model. The ORE is quoted above a detailed pit design, and below the end of March 2023 pit surface. This surface was generated by qualified site-based surveyors using drone technology. No open pit optimisations or design work was completed as part of this update, as the operation is continuing on the current design and there are no material changes to any input parameters or new drill data at depth.

			Proved			Probable			Total Ore Reserve		
Deposit	Type	Cut-Off	Tonnes (Mt)	Gold Grade (g/t)	Gold Metal (koz)	Tonnes (Mt)	Gold Grade (g/t)	Gold Metal (koz)	Tonnes (Mt)	Gold Grade (g/t)	Gold Metal (koz)
Bibra	Open Pit	0.3 <	-	-	-	35.1	0.9	960	35.1	0.9	960
Southern Corridor	Open Pit	0.3 <	-	-	-	10.7	0.7	240	10.7	0.7	240
Stockpiles	Stockpiles	0.3 <	-	-	-	3.4	0.4	47	3.4	0.4	47
Total	Total		-	-	-	49.2	0.8	1,247	49.2	0.8	1,247

Notes:
1. *Ore Reserves are a subset of Mineral Resources.*
2. *Ore Reserves are estimated using a gold price of A$1900/ounce.*
3. *Ore Reserves are estimated using a cut-off grade between 0.3g/t and 0.4g/t Au.*
4. *The above data has been rounded to the nearest 100,000 tonnes, 0.1 g/t gold grade and 1,000 ounces. Errors of summation may occur due to rounding.*



Mineral Resource Estimate Update – Karlawinda

Capricorn has updated the MRE at its 100%-owned KGP mining operation in WA to include a further 542 metres of resource definition drilling at Bibra immediately below the current March 2023 mining surface within the ORE pit designs. This drilling was aimed at providing some more ore-material for confirmatory testwork in fresh rock ore. There is also an additional 69,523 metres of Bibra grade control drilling data which assists in the definition of all near term ore.

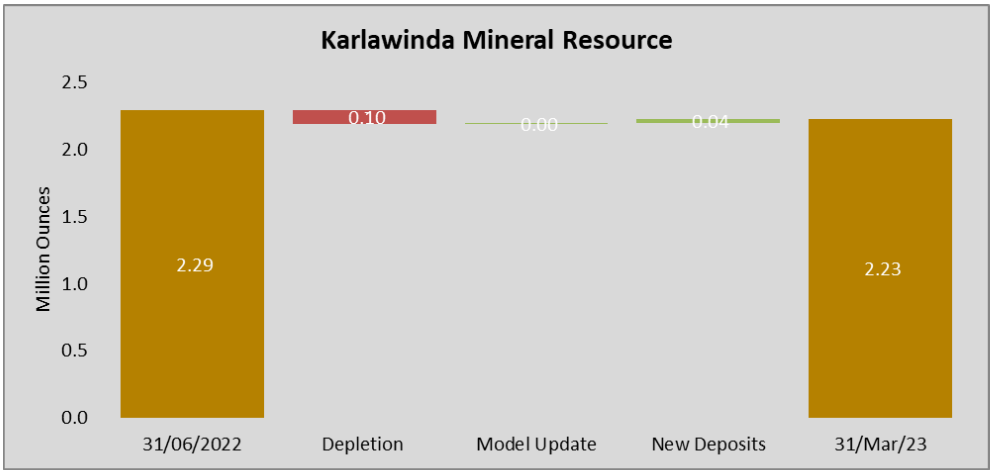
31,333 metres of new resource drilling has been utilised along with 19,290 metres of older drilling to estimate the KGP East area which includes Berwick and Muirfield on the eastern side of the TSF at KGP. Further drilling here in late 2023 is expected to generate testwork samples with the aim of bringing KGP East into Reserves as a satellite pit.

The recent drilling at KGP East has contributed to a modest increase in Mineral Resources after depletion. Whilst not yet material, this discovery proves the existence of further satellite resources proximal to the existing Karlawinda processing plant, and further supports the interpretation of the larger regional exploration area and shows the high likelihood of finding further gold mineralisation.

The 2023 MRE is reported using the ORE variable cut off grades of 0.3g/t for Laterite, 0.3g/t for Oxide, 0.4g/t for transitional and 0.4g/t for fresh material. The cut off grades have been used to ensure the new ORE sits wholly inside the reported MRE. The updated KGP MRE is 97.4 MT at 0.7g/t for 2,228,000 ounces and notably 84% of the MRE is classified in the Indicated category (80.4 million tonnes @ 0.7g/t Au for 1.88 million ounces).

			Measured			Indicated			Inferred			Total Mineral Resources		
Deposit	Type	Cut-Off	Tonnes (Mt)	Gold Grade (g/t)	Gold Metal (koz)	Tonnes (Mt)	Gold Grade (g/t)	Gold Metal (koz)	Tonnes (Mt)	Gold Grade (g/t)	Gold Metal (koz)	Tonnes (Mt)	Gold Grade (g/t)	Gold Metal (koz)
Bibra	Open Pit	0.3 <	-	-	-	50.3	0.8	1,277	4.7	0.7	106	55.0	0.8	1,383
Southern Corridor	Open Pit	0.3 <	-	-	-	22.4	0.7	476	11.5	0.6	230	34.0	0.6	706
Easky	Open Pit	0.3 <	-	-	-	3.0	0.5	47	0.7	0.5	11	3.6	0.5	57
KGP East	Open Pit		-	-	-	1.3	0.8	33	0.1	0.9	2	1.4	0.8	35
Stockpiles	Stockpiles	0.3 <	-	-	-	3.4	0.5	47	-	-	-	3.4	0.4	47
Total	Total		-	-	-	80.4	0.7	1,880	17.0	0.6	349	97.4	0.7	2,228

Notes:
1. *Mineral Resources are estimated using a gold price of A$2200/ounce.*
2. *Mineral Resources are estimated using a cut-off grade between 0.3g/t and 0.4g/t Au.*
3. *The above data has been rounded to the nearest 100,000 tonnes, 0.1 g/t gold grade and 1,000 ounces. Errors of summation may occur due to rounding.*



Group Reserve and Resource Update

There have been no changes to the MGGP ORE or MRE as reported 19 April 2023 with an update expected in the December 2023 quarter to incorporate new drilling data since the last update.

The company's group ORE now stands at 2,697,000 ounces, a decrease of 3% from 2,794,000 ounces (increase of 5,000 ounces (0.2%) after accounting for mining depletion). Group MRE now stand at 4,983,000 ounces, a decrease of 1% from 5,046,000 ounces (increase of 40,000 ounces (1%) after accounting for mining depletion of 102,000 ounces).

GROUP OPEN PIT ORE RESERVE ESTIMATE

Gold			Proved			Probable			Total Ore Reserve		
Project	Type	Cut-Off (g/t)[2]	Tonnes (Mt)	Gold Grade (g/t)	Gold Metal (koz)	Tonnes (Mt)	Gold Grade (g/t)	Gold Metal (koz)	Tonnes (Mt)	Gold Grade (g/t)	Gold Metal (koz)
Karlawinda	Open-Pit	> 0.4	-	-	-	49.2	0.8	1,247	49.2	0.8	1,247
Mount Gibson[5]	Open-Pit	> 0.4	-	-	-	48.7	0.9	1,450	48.7	0.9	1,450
Total	Grand Total	-	-	-	-	97.9	0.9	2,697	97.9	0.9	2,697

Notes:
1. *Ore Reserves are a subset of Mineral Resources.*
2. *Ore Reserves are estimated using a gold price of A$1900/ounce.*
3. *Ore Reserves are estimated using a cut-off grade between 0.3g/t and 0.4g/t Au.*
4. *The above data has been rounded to the nearest 100,000 tonnes, 0.1 g/t gold grade and 1,000 ounces. Errors of summation may occur due to rounding.*
5. *As reported 19th April 2023*

GROUP OPEN PIT MINERAL RESOURCE ESTIMATE

			Indicated			Inferred			Total Mineral Resources		
Deposit	Type	Cut-Off	Tonnes (Mt)	Gold Grade (g/t)	Gold Metal (koz)	Tonnes (Mt)	Gold Grade (g/t)	Gold Metal (koz)	Tonnes (Mt)	Gold Grade (g/t)	Gold Metal (koz)
KGP	Open Pit	0.3 <	80.4	0.7	1,880	17.0	0.6	349	97.4	0.7	2,228
MGGP[4]	Open Pit	0.4	76.0	0.9	2,106	28.9	0.7	649	104.9	0.8	2,755
Total	Total		156.4	0.8	3,986	45.9	0.7	998	202.2	0.8	4,983

Notes:
1. *Mineral Resources are estimated using a gold price of A$2200/ounce.*
2. *Mineral Resources are estimated using a cut-off grade between 0.3g/t and 0.4g/t Au.*
3. *The above data has been rounded to the nearest 100,000 tonnes, 0.1 g/t gold grade and 1,000 ounces. Errors of summation may occur due to rounding.*
4. *As reported 19th April 2023*

This announcement has been authorised for release by the Capricorn Metals Ltd board.

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Forward Looking Statements

This announcement may contain certain “forward-looking statements” which may not have been based solely on historical facts, but rather may be based on the Company’s current expectations about future events and results. Where the Company expresses or implies an expectation of belief as to future events or results, such expectation or belief is expressed in good faith and believed to have a reasonable basis. The detailed reasons for that conclusion are outlined throughout this announcement and all material assumptions are disclosed.

However, forward looking statements are subject to risks, uncertainties, assumptions and other factors, which could cause actual results to differ materially from future results expressed, projected or implied by such forward-looking statements.

Such risks include, but are not limited to resource risk, metals price volatility, currency fluctuations, increased production costs and variances in ore grade or recovery rates from those assumed in mining plans, as well as governmental regulation and judicial outcomes.

For a more detailed discussion of such risks and other factors, see the Company’s Annual Reports, as well as the Company’s other filings. Readers should not place undue reliance on forward looking information. The Company does not undertake any obligation to release publicly any revisions to any “forward looking statement” to reflect events or circumstances after the date of this announcement, or to reflect the occurrence of unanticipated events, except as may be required under applicable securities laws.

Competent Persons Statement

The information in this report that relates to the KGP Mineral Resource Estimate is based on information compiled by Mr. Jarrad Price who is Resource Geologist and an employee of the Company. Mr. Jarrad Price is a current Member of the Australian Institute of Geoscientists and has sufficient experience, which is relevant to the style of mineralisation and types of deposit under consideration and to the activities undertaken, to qualify as a Competent Person as defined in the 2012 Edition of the “Australasian Code of Reporting of Exploration Results, Mineral Resources and Ore Reserves”. Mr. Price consents to the inclusion in the report of the matters based on the information in the form and context in which it appears.

The information in this report that relates to the KGP Ore Reserve Estimate is based on information compiled by Mr Quinton de Klerk. Mr de Klerk is a full-time employee of Cube Consulting Pty Ltd and is a Fellow of the Australian Institute of Mining and Metallurgy. Mr de Klerk has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and to the activity currently being undertaken to qualify as a Competent Person as defined in the 2012 Edition of the “Australasian Code of Reporting of Exploration Results, Mineral Resources and Ore Reserves”. Mr. de Klerk consents to the inclusion in this report of the matters based on the information in the form and context in which it appears.

The information in this report that relates to Exploration Results is based on information compiled or reviewed by Mr. William Higgins who is a full-time employee of the Company. Mr. Higgins is a current Member of the Australian Institute of Geoscientists and has sufficient experience, which is relevant to the style of mineralisation and types of deposit under consideration and to the activities undertaken, to qualify as a Competent Person as defined in the 2012 Edition of the “Australasian Code of Reporting of Exploration Results, Mineral Resources and Ore Reserves”. Mr. Higgins consents to the inclusion in the report of the matters based on the information in the form and context in which it appears.

The detailed information relating to the MGGP Ore Reserves and Mineral Resources reported in this announcement were announced in the Company’s ASX announcements dated 7 November 2022 and 19 April 2023. The Company confirms that it is not aware of any new information or data that materially affects the information included in the ASX announcements dated 7 November 2022 and 19 April 2023 and all material assumptions and technical parameters underpinning the estimates in the relevant market announcements continue to apply and have not materially changed. The Company confirms that the form and context in which the Competent Persons’ findings are presented have not materially changed from previous market announcements. The reports are available to view on the ASX website and on the Company’s website at www.capmetals.com.au .

The Competent Person’s consents remain in place for subsequent releases by the Company of the same information in the same form and context, until the consent is withdrawn or replaced by subsequent report and accompanying consent.

APPENDIX 1 – ORE & MRE ADDITIONAL INFORMATION

KGP Ore Reserve Estimation Update - Additional Information

KGP Location and Tenure

The KGP is located in the Pilbara region of Western Australia, 65km by road south-east of the town of Newman.

The KGP is an operating gold project which includes the Bibra deposit and numerous outstanding exploration targets including Forfar, Muirfield and Jims West. The project covers a total area of approximately 2,052km^2.

Construction of the KGP commenced in December 2019 and was completed in the June 2021 quarter with the successful commissioning of the processing plant culminating in first gold poured at the end of June 2021. Steady state operations were achieved by the end of the September 2021 quarter.

The Bibra deposit is covered by mining lease M52/1070 100% held by Greenmount Resources Pty Ltd, (Greenmount) a wholly owned subsidiary of Capricorn. M52/1070 is a granted mining lease of sufficient size to cover the Bibra resource area and with the granted ancillary miscellaneous licences the associated infrastructure for the mining operation. M52/1070 was excised upon grant from exploration licence E52/1711.

Western Australia is recognised globally as a low risk mining jurisdiction.

The Nyiyaparli People hold Native Title over M52/1070 and the ancillary miscellaneous licences. There are no known heritage or environmental impediments over the mining lease. Capricorn has a Land Access Agreement with the Nyiyaparli People over the mining lease and all other project tenure. No known social or environmental impediments exist with respect to the proposed mining operation.

Regional Infrastructure

The project is within economic distances of existing infrastructure in the east Pilbara region. The town of Newman contains significant engineering, mining support services and key infrastructure including a major airport. The project operates as a Fly In-Fly Out (FIFO) operation. Services and consumable supplies are delivered by existing roads and a 40km access road from the Great Northern Highway to the project.

The mining and exploration tenure held by Capricorn cover all project requirements. The mining area lies at the northern boundary of the Weelerrana pastoral lease and the Company has a co-operative working relationship with all pastoralists over the project area.

Bibra Deposit Geology

At Bibra, mineralisation is shoot-controlled along a series of dominant low-angle, north-east trending mineralised faults that combine to make up a very large-scale mineralised system. The system is hosted in a sequence of Archaean greenstones metamorphosed to amphibolite facies. The greenstones comprise a mafic volcanic sequence with interbedded sedimentary and volcanoclastic units.

The deposit has been defined by drilling over a 1.8km strike length and is drilled to 800m down-dip where it is still mineralised and open down-dip. The mineralised shoots are present in drilling as broad zones up to 50m wide and are continuous down plunge. It is thought the shoots are developed in dilation zones along the main structures. A large laterite and oxide weathering zone is developed over the primary geology and this is mineralised in the near surface, up-dip position of the main shoots of primary mineralisation. A thin veneer of transported sandy soil covers the deposit and is typically less than 3m thick, the transition/fresh rock boundary is about 60m below surface.

Geological logging suggests alteration consisting of biotite, carbonate and magnetite mineralisation forms a halo surrounding the intense silica, pyrite and gold mineralisation. The metamorphic overprint of the mineralisation may have altered some of the primary alteration and mineralisation to the present day mineral species.

Confidence in the geological interpretation is high. The stratigraphy is consistent and can be correlated between holes and along strike.

Geological logging and structural measurements from drillholes have been used to construct the geological resource model. Sections were interpreted, digitised and a three dimensional (3D) wireframe model constructed.

Mining Assumptions

The Bibra deposit is mined by open pit mining methods using conventional mining equipment. The selected mining method, design and extraction sequence are tailored to suit orebody characteristics, minimise dilution and ore loss, defer waste movement, minimise rates of vertical mining advance, utilise planned process plant capacity and expedite free cash generation in a safe manner. The open pit has been scheduled based on achieved mining productivity and rates along with consistent material movements.

The mining operating costs have been calculated from contracted and extrapolated rates for drilling, blasting, loading and haulage which require the contractor to provide all equipment. Grade control and ancillary costs have been based on actual costs.

Mining dilution and mining recovery modifying factors are accounted for in the estimation of the MRE mainly from the low cut-off used for the estimation domains and the block size estimated at SMU dimensions. This is supported by reconciliation data.

The KGP ORE has been updated to reflect mining depletion since the ORE reported on 27 October together with a modest model update incorporating in pit drilling date from current grade control programmes. The ORE is quoted above a detailed pit design, and below the end of March 2023 pit surface. This surface was generated by qualified site-based surveyors using drone technology. No open pit optimisations or design work was completed as part of this update, as the operation is committed to the current design and there are no material changes to any input parameters or new drill data at depth.

Geotechnical Modelling

Geotechnical modelling has been completed by an external consultant based on field logging and laboratory testing of selected diamond drill core samples from 18 drilled for purpose geotechnical diamond drillholes. The open pit designs are based on the recommended geotechnical design parameters and assume dry slopes based on the assumption of adequate dewatering and/or depressurisation ahead of mining.

The low-angle dip of the deposit (28^{o} to West) allows for a designed overall batter angle on the Footwall (Eastern side of pit) between ramps of 25 ^{o}. The western wall (Hanging Wall) of the pit is designed to have an overall slope angle of 49.8^{o}. Identical slope angles are used in the Southern Corridor pit, following analysis of two geotechnical diamond drillholes.

A separate hydrogeological report was prepared by independent consultants which considered the requirements to effectively dewater the open pit and pit slopes. This study was supported by the development of test bores and field test pumping analysis. The water quality of the defined aquifer at Karlawinda is low in total dissolved salts and only requires minor treatment to make potable.

Mining Infrastructure

The mine plan includes waste rock dumps, a ROM pad, a surface water diversion channel, surface dewatering bores, light and heavy vehicle workshop facilities, explosives storage, supply facilities, technical services facilities, accommodation camp, airstrip and administration facilities.

Metallurgical and Processing Assumptions

An optimised flowsheet, mass and water balances, equipment selection, and plant designs and layouts were all developed to FS standard based upon several phases of testwork.

The testwork was conducted on 35 composites (30 variability and 5 master) prepared from 779 meters of diamond drill core, totalling 90 intervals from 52 drill holes. These samples amount to 4,103kg and represent the four main weathering horizons in the Bibra deposit.

The test work demonstrated Bibra ore contains a gravity recoverable gold component and is free milling with high gold extractions achievable by conventional cyanidation. Production to date supports the metallurgical and processing assumptions.

Flowsheet

The metallurgical flowsheet used is commonly used in the Australian and international gold mining industry and is well-tested and proven technology.

It comprises of a comminution circuit which consists of a three stage crushing plant providing crushed ore to a crushed ore stockpile followed by a milling circuit which consists of a 7.5MW ball mill and cyclone classification. Gold recovery involves a conventional gravity circuit and Carbon-in-Leach (CIL) circuit. Gold is recovered by standard elution and electrowinning techniques prior to smelting. The tailings are placed in an Integrated Waste Landform (IWL) and water recovered and recycled. Reagent consumptions are all relatively low.

Comminution

The comminution circuit for the KGP is able to suitably treat the range of ores over the project life with the throughput rates of 4MTPA for fresh ore and 5MTPA in oxide ore.

Metallurgical Recovery

Over 120 leach tests were performed on the various Bibra ores over the various testwork programs. The work showed that all ores were free milling, have a lower sensitivity to grind size, and with the gravity gold component removed is fast leaching with low reagent consumptions.

Estimated plant gold recovery ranges from 91% to 94% depending on grind size, head grade and ore type. An average of 25% of gold from oxide ore and 45% from fresh ore is estimated to be recovered by gravity methods. No deleterious elements of significance have been determined from metallurgical test work and mineralogy investigations. Production to date supports the metallurgical assumptions.

Tailings Disposal

Tailings disposal is within an Integrated Waste Landform (IWL) whereby tailings are encapsulated by mining waste, rather than having separate waste dumps and tailings facilities.

Infrastructure

The workforce is Fly In-Fly Out (FIFO) and based at a dedicated camp on the mining lease during rostered days on. An onsite airstrip is used.

Pump monitoring and modelling of the yield from the KGP borefield indicate that there is sufficient groundwater to service the needs of the Project for the life-of-mine.

Power is generated on site utilising natural gas reticulated from the GGP.

Cost and Economic Assumptions

The operating cost estimate is appropriate for the current market in Western Australia. Cost inputs have been based on a reference to actual costs, contracted rates, quotations and/or estimates by competent specialists.

Gold bullion transportation and refining charges are derived on the basis of a quote provided by a leading Australian gold refinery.

An allowance has been made for all royalties, including an allowance of 2.5% of revenue for royalties payable to the Western Australian State Government and a 2.0% allowance for the current commercial third party royalty. The terms of the royalty payable to the other private party is covered by confidentiality restrictions.

A Life-of-mine (LOM) gold price forecast of A$1,900/ounce is applied in the Ore Reserve estimation process. This price forecast was established by Capricorn based on historical A$ gold price trends over the last five years and by comparison against peer companies. Net present value (NPV) and free cashflow analysis of the ORE based on the key assumptions used in the estimate and sensitivity analysis of them indicates that the project retains a suitable profit margin against reasonable future commodity price assumptions.

Social and Environmental

Flooding risk has been analysed by an independent external expert and deemed to be minimal.

No significant flora or fauna species, including subterranean species have been identified that would be significantly impacted by the Project in a manner that could not be adequately managed.

Waste rock and tailings characterisation work has been completed and all waste types and tailings are non-acid forming and have limited metal leachate potential.

All mining tenure required for the project has been obtained. Approvals required to enable the project to operate have been obtained.

KGP Mineral Resource Estimation Update - Additional Information

Mineral Resource Estimation Methodology and Data

Bibra is part of a large-scale Archaean aged gold mineralised system. The geology at Bibra predominantly comprises a sequence of alternating Archaean amphibolites and quartz-feldspar-chlorite-garnet schists with the majority of mineralisation hosted in silicified and magnetite altered, mylonitised “psmammites”. Gold mineralisation has developed on at least two parallel, 40m thick, shallow dipping sandstone units, which dip to the west-north-west at 22°. Laterite mineralisation has developed over the structures close to surface. Outside of the main mineralisation some smaller discrete lodes occur in the hanging wall. Mineralisation continues south of the main pit area into the Southern Corridor where mineralisation is hosted in volcanoclastic sandstones with broad lower grade mineralisation with zones of high grade mineralisation. The primary mineralisation is marked by 3-10% sulphides, subhedral magnetite grains, quartz veins/veinlets, and gold. Gold mineralisation is strata-form with lineations identified as controlling higher-grade shoots. The overall footprint of the mineralisation covers an area of 1800m (local grid N) by 1800m (local grid E). The deposit is oxidised to average depths of 50-70m.

Drilling Techniques

In total 486,527 metres of drilling has been completed within the constraints of the Bibra resource consisting of 92 Diamond holes (13,983m/ 3%) and 1,550 resource drilling Reverse Circulation drillholes (215,953m/ 44%), 14,396 grade control drillholes (256,591m/ 53%).

The KGP East project area consists of 68 AC holes for 3,761m, 259 RC holes for 37,185m and 30 DD holes for 9,677m for a total of 357 holes for 50,623m. These drill holes are separate and additional to the Bibra resource area drillholes quoted above.

The drilling database for both areas consists of high quality RC and diamond drillholes with holes drilled at approximate spacings of 25m x 25m to 25m x 50m in the Indicated category area and 50m x 50m to 100m x 100m in the Inferred category area. Grade control drilling at Bibra is spaced at 10m x 5m in stage 1 & 2, and 7.5m x 7.5m in all other areas. Deeper holes and wider spaced drilling targeting along strike, down-dip and down-plunge extensions of the mineralisation have also been completed outside of the classified resource area and included in the model. However, currently this material remains unclassified/not reported and is a target for future resource development drilling.

Sampling and Sub-Sampling Techniques

Drilling at KGP and KGP East has been completed by both Independence Group (IGO) and Capricorn Metals Group (CMM). The methods of collection have been very similar in terms of sampling procedures, drilling methods and sampling quality.

2kg - 3kg samples RC were split from dry 1m bulk samples. The sample was initially collected from the cyclone in an inline collection box with independent upper and lower shutters. Once the metre was completed, the drill bit was lifted off the bottom of the hole, to create a gap between sample, when the gap of air reached the collection box the top shutter was closed off. Once the top shutter was closed, the bottom shutter was opened, and the sample was dropped under gravity through a Metzke cone splitter. Once drilling reached fresh rock a fine spray of water was used to suppress dust and limit the loss of fines through the cyclone chimney. A second 2kg-3kg sample was collected at the same time as the original sample as a field duplicate.

The diamond drillholes were saw cut, with one half being sent to the laboratory. Diamond core was sampled dominantly to 1 metre intervals, some smaller samples were collected where the core was sampled to geological/mineralisation contacts.

QAQC protocols have been executed to a high standard. QA/QC programs were implemented to test the quality of drilling, assaying and logging. In the drilling programs, samples were weighed to determine drillhole quality through the analysis of sample recovery and split ratio. It was shown through the gathering of this information, that the drilling was completed to a high standard with overall recovery greater than 80% and the split ratio through the splitter showing no material bias.

Sample Analysis Method

RC and diamond core samples were sent to MinAnalytical, ALS, Intertek, Genalysis, Jinning or Aurum laboratories in Perth, where the samples were oven dried at 105°C. After drying, the core was crushed to a nominal 2mm and then both RC and diamond core were pulverised LM5 mills to 5 minutes to achieve 85% passing 75µm to provide a pulp sample for analysis. All samples submitted by CMM were analysed for Au using the FA50/MS technique, which is a 50g lead collection fire assay. The samples submitted by IGO were analysed by FA50/AAS which is a 50g lead collection fire assay.

Field duplicates were collected at a ratio of 1:20 through the mineralised zones (1:40 elsewhere) and collected at the same time as the original sample through the B chute of the cone splitter. OREAS certified reference material (CRM) and matrix matched CRMs were inserted at a ratio of 1:20 through the mineralised zone (1:40 elsewhere), and 1:40 through all zones after 2019. The grade ranges of the CRMs were selected based on grade populations and economic grade ranges. The duplicate and CRMs were submitted to the lab using unique sample IDs.

Estimation Methodology

Three-dimensional wireframes were created to constrain the mineralisation and allocate geology to the block model. Surpac software was used for the wireframing of the ore and weathering profiles, Micromine software was used for the wireframing of geology by the exploration department. The mineralisation wireframe models were built using sectional interpretation and visualization of the mineralisation in three-dimensions. The sectional mineralisation strings were defined with a cut-off grade of 0.1g/t Au. There are four main mineralisation domains and a Laterite domain. Located outside the Main Bibra Pit area, there are several other resource areas such as Easky, which were included in the estimate. The area previously referred to as Tramore has been included within the Southern Corridor area for this estimation update. Berwick and Muirfield from KGP East includes two mineralisation domains. The geological interpretation wireframes were built by on-site explorration geologists to ensure the interpretation consistency. Geological logging and structural measurements from drillholes has been used to construct the geological model. Geological continuity has been assumed along strike and down-dip.

A block model was created to encompass the Bibra mineralisation and prospects in close proximity. 10 X by 10 Y by 5 Z is the parent block size, with sub-blocking only in the Z direction to reflect the flat lying geometry of the laterite portion of the deposit. The KGP East block model has a 5 X by 5 Y by 2.5 Z block size with no sub-blocking. Variography was undertaken on domains using Snowden Supervisor software and that variography was used to undertake Kriging neighborhood analysis to optimise the block size, search distances and min/max sample numbers used. Search ellipses were also developed from the variography. The block model grades were estimated using ordinary kriging grade interpolation techniques constrained within the mineralisation wireframes. All work was completed in the local grid co-ordinate system. The estimation was completed in three passes with the following parameters;

- ***Pass 1 non laterite:*** 16/64 min and max samples using an octant search, 40m (25m for KGP East) search distance in the major direction, maximum of 4 samples used per hole, and a maximum of 1 adjacent octant failing to have the required composites. Block size estimated into is 10m/10m/5m XYZ.
- ***Pass 1 laterite:*** 16/24 min and max samples using an ellipsoid search, 40m search

distance in the major direction, maximum of 4 samples used per hole. Block size estimated into is 10m/10m/2.5m XYZ.

- ***Pass 2 non laterite:*** 16/64 min and max samples using an octant search, 60m (50m for KGP East) search distance in the major direction, maximum of 4 samples used per hole, and a maximum of 1 adjacent octant failing to have the required composites. Block size estimated into is 10m/10m/5m XYZ.
- ***Pass 2 laterite:*** 16/24 min and max samples using an ellipsoid search, 60m search distance in the major direction, maximum of 4 samples used per hole. Block size estimated into is 10m/10m/2.5m XYZ.
- ***Pass 3 non laterite:*** 8/64 min and max samples using an octant search, 100m (100m for KGP East) search distance in the major direction, maximum of 4 samples used per hole, and a maximum of 1 adjacent octant failing to have the required composites. Block size estimated into is 10m/10m/5m XYZ.
- ***Pass 3 laterite:*** 16/24 min and max samples using an ellipsoid search, 100m search distance in the major direction, maximum of 4 samples used per hole. Block size estimated into is 10m/10m/2.5m XYZ.

Top-cuts were applied to sample composites, with a high grade restriction utilised to limit the influence of higher grade data, particularly outside of the high grade zones. The high grade restriction is an indicator estimate completed at 1 g/t.

Density assumptions were based on 3,976 samples water immersion method density readings. Average densities for oxidation profiles were assigned to the block model.

The grade estimate was checked against the input drilling/composite data both visually on section (cross and long section) and in plan, and statistically on swath plots as well as against production and grade control (for Bibra).

Resource Classification Criteria

The Indicated and Inferred classification reflects the relative confidence in the estimate, the confidence in the geological interpretation, the drilling spacing, input data, the assay repeatability and the continuity of the mineralisation.

The strategy adopted in the current study uses category 1 and 2 from the 3-pass octant search strategy to guide interpretation of a classification surface where Indicated is above the surface and Inferred being below. This results in a geologically sensible classification whereby Category 1 and 2 are surrounded by data in close proximity. Category 3 blocks may occur on the peripheries of drilling but are still related to drilling data within reasonable distances. No measured has been applied in the classification method. This classification reflects the Competent Person’s view of the deposit.

Mining and Metallurgical Methods and Parameters

This information is contained within the KGP Ore Reserve Additional Information section of this release.

APPENDIX 2 – SIGNIFICANT RESULTS

Mt Gibson

Hole No	Easting	Northing	RL	Hole Depth	Dip/Azi	From	To	Width	Grade (g/t Au)
CMHL092	515752.2	6708873.6	377.6	30	-90/0.1	11	24	13	0.65
CMHL093	515786.9	6708852.7	377.5	30	-90/0.1	5	15	10	0.58
CMHL094	515786.8	6708842.6	377.7	26	-90/0.1	0	1	1	0.54
CMHL094	515786.8	6708842.6	377.7	26	-90/0.1	7	8	1	0.54
CMHL094	515786.8	6708842.6	377.7	26	-90/0.1	11	12	1	0.65
CMHL095	515787.4	6708829.5	377.7	30	-90/0.1	5	11	6	0.50
CMHL095	515787.4	6708829.5	377.7	30	-90/0.1	15	16	1	0.51
CMHL096	515787.9	6708815.0	377.7	33	-90/0.1	2	4	2	0.58
CMHL096	515787.9	6708815.0	377.7	33	-90/0.1	7	11	4	0.67
CMHL096	515787.9	6708815.0	377.7	33	-90/0.1	21	22	1	0.56
CMHL096	515787.9	6708815.0	377.7	33	-90/0.1	29	30	1	0.57
CMHL097	515788.0	6708804.7	377.8	33	-90/0.1	19	23	4	0.72
CMHL097	515788.0	6708804.7	377.8	33	-90/0.1	29	30	1	1.32
CMHL098	515788.5	6708791.5	377.9	33	-90/0.1	8	9	1	0.90
CMHL098	515788.5	6708791.5	377.9	33	-90/0.1	12	23	11	0.70
CMHL098	515788.5	6708791.5	377.9	33	-90/0.1	27	30	3	1.21
CMHL099	515791.1	6708779.1	377.7	33	-90/0.1	10	12	2	0.72
CMHL099	515791.1	6708779.1	377.7	33	-90/0.1	22	23	1	0.93
CMHL099	515791.1	6708779.1	377.7	33	-90/0.1	27	32	5	1.09
CMHL100	515790.0	6708750.8	377.2	33	-90/0.1	14	15	1	0.71
CMHL100	515790.0	6708750.8	377.2	33	-90/0.1	20	21	1	0.57
CMHL100	515790.0	6708750.8	377.2	33	-90/0.1	29	32	3	0.93
CMHL101	515753.3	6708708.9	375.0	30	-90/0.1	12	19	7	0.84
CMHL101	515753.3	6708708.9	375.0	30	-90/0.1	27	30	3	0.61
CMHL102	515724.8	6708707.9	374.8	27	-90/0.1	3	6	3	0.59
CMHL102	515724.8	6708707.9	374.8	27	-90/0.1	16	17	1	0.57
CMHL103	515702.1	6708706.7	374.2	27	-90/0.1	15	19	4	0.76
CMHL104	515674.6	6708707.1	375.3	27	-90/0.1	14	15	1	1.05
CMHL105	515651.0	6708706.5	374.6	24	-90/0.1	7	8	1	1.92
CMHL105	515651.0	6708706.5	374.6	24	-90/0.1	11	12	1	1.31
CMHL105	515651.0	6708706.5	374.6	24	-90/0.1	15	20	5	0.66
CMHL106	515625.1	6708707.5	373.1	24	-90/0.1	5	9	4	0.61
CMHL106	515625.1	6708707.5	373.1	24	-90/0.1	12	18	6	0.59
CMHL107	515602.1	6708705.5	374.2	24	-90/0.1	5	7	2	0.87
CMHL107	515602.1	6708705.5	374.2	24	-90/0.1	15	18	3	0.52
CMHL108	515552.4	6708703.3	375.2	24	-90/0.1	6	11	5	0.66
CMHL108	515552.4	6708703.3	375.2	24	-90/0.1	22	23	1	2.76
CMHL109	515530.6	6708703.7	375.3	27	-90/0.1	12	21	9	0.71
CMHL110	515502.5	6708704.2	375.6	27	-90/0.1	4	7	3	0.51
CMHL111	515472.6	6708715.8	379.3	30	-90/0.1	0	17	17	1.04
CMHL113	515463.9	6708738.8	379.6	30	-90/0.1	0	1	1	0.54
CMHL113	515463.9	6708738.8	379.6	30	-90/0.1	5	6	1	0.57
CMHL113	515463.9	6708738.8	379.6	30	-90/0.1	16	17	1	0.71
CMHL114	515466.1	6708764.8	380.4	33	-90/0.1	1	2	1	0.59
CMHL114	515466.1	6708764.8	380.4	33	-90/0.1	24	25	1	1.41
CMHL114	515466.1	6708764.8	380.4	33	-90/0.1	24	26	2	0.96
CMHL115	515466.0	6708817.6	379.5	36	-90/0.1	17	18	1	0.76
CMHL115	515466.0	6708817.6	379.5	36	-90/0.1	29	30	1	0.50
CMHL117	515480.2	6708861.4	377.9	29	-90/0.1	7	10	3	0.58

Hole No	Easting	Northing	RL	Hole Depth	Dip/Azi	From	To	Width	Grade (g/t Au)
CMHL117	515480.2	6708861.4	377.9	29	-90/0.1	20	21	1	0.82
CMHL118	515506.0	6708875.3	376.2	30	-90/0.1	0	3	3	1.40
CMHL118	515506.0	6708875.3	376.2	30	-90/0.1	1	2	1	2.85
CMHL118	515506.0	6708875.3	376.2	30	-90/0.1	23	24	1	0.59
CMHL119	515517.9	6708877.4	376.0	30	-90/0.1	3	9	6	2.12
CMHL120	515528.1	6708878.7	375.9	30	-90/0.1	9	14	5	2.78
CMHL120	515528.1	6708878.7	375.9	30	-90/0.1	10	14	4	3.27
CMHL121	515539.5	6708879.7	376.1	30	-90/0.1	4	8	4	0.58
CMHL121	515539.5	6708879.7	376.1	30	-90/0.1	23	24	1	0.54
CMHL122	515554.6	6708879.5	376.3	30	-90/0.1	2	4	2	0.72
CMHL122	515554.6	6708879.5	376.3	30	-90/0.1	9	10	1	1.47
CMHL122	515554.6	6708879.5	376.3	30	-90/0.1	9	14	5	0.84
CMHL122	515554.6	6708879.5	376.3	30	-90/0.1	13	14	1	1.13
CMHL123	515565.4	6708880.5	376.6	33	-90/0.1	4	10	6	0.49
CMHL124	515580.1	6708880.5	377.0	30	-90/0.1	4	11	7	0.52
CMHL124	515580.1	6708880.5	377.0	30	-90/0.1	24	25	1	1.16
CMHL124	515580.1	6708880.5	377.0	30	-90/0.1	28	30	2	0.70
CMHL125	515591.6	6708880.4	376.8	30	-90/0.1	9	11	2	0.65
CMHL125	515591.6	6708880.4	376.8	30	-90/0.1	29	30	1	0.66
CMHL126	515602.4	6708880.7	376.4	30	-90/0.1	4	5	1	0.64
CMHL127	515616.7	6708881.4	375.9	30	-90/0.1	27	28	1	0.59
CMHL129	515641.8	6708883.2	375.5	30	-90/0.1	14	16	2	0.66
CMHL129	515641.8	6708883.2	375.5	30	-90/0.1	20	21	1	0.65
CMHL130	515654.1	6708883.7	375.4	30	-90/0.1	4	10	6	0.75
CMHL130	515654.1	6708883.7	375.4	30	-90/0.1	6	8	2	1.10
CMHL130	515654.1	6708883.7	375.4	30	-90/0.1	18	19	1	0.55
CMHL131	515666.6	6708883.4	375.4	30	-90/0.1	7	9	2	0.55
CMHL131	515666.6	6708883.4	375.4	30	-90/0.1	17	18	1	0.51
CMHL132	515679.2	6708883.7	375.4	30	-90/0.1	15	16	1	0.77
CMHL133	515689.0	6708883.9	375.4	30	-90/0.1	18	20	2	3.24
CMHL133	515689.0	6708883.9	375.4	30	-90/0.1	18	21	3	2.43
CMHL134	515702.4	6708885.3	375.1	27	-90/0.1	10	11	1	0.70
CMHL134	515702.4	6708885.3	375.1	27	-90/0.1	17	22	5	0.81
CMHL135	515715.2	6708885.6	375.0	21	-90/0.1	17	18	1	2.42
CMHL135	515715.2	6708885.6	375.0	21	-90/0.1	17	21	4	1.14
CMHL137	515740.1	6708886.4	374.2	27	-90/0.1	9	10	1	0.56
CMHL137	515740.1	6708886.4	374.2	27	-90/0.1	18	20	2	0.76
CMHL138	515751.5	6708886.9	373.8	27	-90/0.1	19	20	1	1.48
CMHL139	515764.3	6708886.8	373.6	27	-90/0.1	5	8	3	0.99
CMHL139	515764.3	6708886.8	373.6	27	-90/0.1	6	7	1	1.05
CMHL139	515764.3	6708886.8	373.6	27	-90/0.1	12	13	1	0.57
CMHL140	515790.3	6708885.2	372.9	30	-90/0.1	3	7	4	1.23
CMHL140	515790.3	6708885.2	372.9	30	-90/0.1	3	13	10	0.77
CMHL141	515806.2	6708886.6	372.5	27	-90/0.1	4	5	1	0.86
CMHL141	515806.2	6708886.6	372.5	27	-90/0.1	12	17	5	1.04
CMHL141	515806.2	6708886.6	372.5	27	-90/0.1	15	17	2	1.27
CMHL141	515806.2	6708886.6	372.5	27	-90/0.1	21	23	2	5.94
CMHL142	515804.4	6708869.9	372.6	27	-90/0.1	0	5	5	0.72
CMHL142	515804.4	6708869.9	372.6	27	-90/0.1	8	16	8	0.75
CMHL143	515805.6	6708863.0	372.5	27	-90/0.1	2	3	1	0.53
CMHL143	515805.6	6708863.0	372.5	27	-90/0.1	7	12	5	0.67
CMHL144	515809.7	6708851.1	371.4	27	-90/0.1	1	2	1	0.71
CMHL144	515809.7	6708851.1	371.4	27	-90/0.1	14	16	2	0.57
CMHL146	515815.0	6708830.5	371.3	27	-90/0.1	7	11	4	0.44

Hole No	Easting	Northing	RL	Hole Depth	Dip/Azi	From	To	Width	Grade (g/t Au)
CMHL146	515815.0	6708830.5	371.3	27	-90/0.1	18	19	1	0.81
CMHL146	515815.0	6708830.5	371.3	27	-90/0.1	23	24	1	0.59
CMHL147	515817.5	6708817.4	371.2	28	-90/0.1	11	18	7	0.97
CMHL148	515819.3	6708804.4	370.8	27	-90/0.1	2	7	5	1.08
CMHL148	515819.3	6708804.4	370.8	27	-90/0.1	14	15	1	0.91
CMHL148	515819.3	6708804.4	370.8	27	-90/0.1	22	24	2	0.78
CMHL149	515820.1	6708789.2	370.3	27	-90/0.1	2	3	1	1.92
CMHL149	515820.1	6708789.2	370.3	27	-90/0.1	13	14	1	1.22
CMHL150	515820.6	6708777.5	369.8	24	-90/0.1	0	2	2	0.94
CMHL150	515820.6	6708777.5	369.8	24	-90/0.1	6	8	2	0.85
CMHL150	515820.6	6708777.5	369.8	24	-90/0.1	16	24	8	0.57
CMHL151	515820.9	6708766.6	369.8	27	-90/0.1	1	25	24	0.68
CMHL152	515821.0	6708753.7	370.1	23	-90/0.1	1	3	2	1.05
CMHL153	515820.7	6708741.8	370.1	24	-90/0.1	1	2	1	0.75
CMHL153	515820.7	6708741.8	370.1	24	-90/0.1	18	19	1	0.56
CMHL153	515820.7	6708741.8	370.1	24	-90/0.1	22	23	1	0.65
CMHL154	515813.5	6708725.6	370.2	24	-90/0.1	10	12	2	0.75
CMHL154	515813.5	6708725.6	370.2	24	-90/0.1	23	24	1	0.50
CMHL155	515798.4	6708707.5	370.0	24	-90/0.1	1	16	15	0.84
CMHL155	515798.4	6708707.5	370.0	24	-90/0.1	6	7	1	1.66
CMHL155	515798.4	6708707.5	370.0	24	-90/0.1	10	12	2	1.82
CMHL155	515798.4	6708707.5	370.0	24	-90/0.1	15	16	1	1.51
CMHL155	515798.4	6708707.5	370.0	24	-90/0.1	20	24	4	0.72
CMHL155	515798.4	6708707.5	370.0	24	-90/0.1	22	23	1	1.06
CMHL156	515730.1	6708731.8	380.1	33	-90/0.1	6	7	1	0.65
CMHL156	515730.1	6708731.8	380.1	33	-90/0.1	30	33	3	1.04
CMHL156	515730.1	6708731.8	380.1	33	-90/0.1	31	32	1	1.34
CMHL157	515710.4	6708732.2	379.9	33	-90/0.1	7	11	4	0.58
CMHL157	515710.4	6708732.2	379.9	33	-90/0.1	15	16	1	0.55
CMHL158	515683.9	6708733.1	380.9	33	-90/0.1	0	3	3	0.48
CMHL158	515683.9	6708733.1	380.9	33	-90/0.1	9	12	3	0.57
CMHL158	515683.9	6708733.1	380.9	33	-90/0.1	21	24	3	1.19
CMHL158	515683.9	6708733.1	380.9	33	-90/0.1	23	24	1	2.12
CMHL159	515664.9	6708733.2	381.3	33	-90/0.1	4	5	1	0.63
CMHL159	515664.9	6708733.2	381.3	33	-90/0.1	17	20	3	0.52
CMHL159	515664.9	6708733.2	381.3	33	-90/0.1	24	25	1	0.58
CMHL160	515654.3	6708733.9	381.4	33	-90/0.1	0	1	1	0.66
CMHL160	515654.3	6708733.9	381.4	33	-90/0.1	10	22	12	0.63
CMHL160	515654.3	6708733.9	381.4	33	-90/0.1	12	13	1	1.91
CMHL160	515654.3	6708733.9	381.4	33	-90/0.1	26	27	1	0.54
CMHL161	515641.9	6708735.0	382.2	33	-90/0.1	1	8	7	0.85
CMHL161	515641.9	6708735.0	382.2	33	-90/0.1	4	7	3	1.28
CMHL161	515641.9	6708735.0	382.2	33	-90/0.1	12	17	5	8.36
CMHL161	515641.9	6708735.0	382.2	33	-90/0.1	13	17	4	10.29
CMHL161	515641.9	6708735.0	382.2	33	-90/0.1	23	25	2	0.56
CMHL162	515628.9	6708735.9	383.3	36	-90/0.1	4	7	3	0.72
CMHL162	515628.9	6708735.9	383.3	36	-90/0.1	6	7	1	1.23
CMHL162	515628.9	6708735.9	383.3	36	-90/0.1	12	16	4	0.70
CMHL162	515628.9	6708735.9	383.3	36	-90/0.1	21	22	1	0.87
CMHL162	515628.9	6708735.9	383.3	36	-90/0.1	26	27	1	0.68
CMHL163	515614.8	6708735.3	383.9	36	-90/0.1	3	5	2	0.64
CMHL163	515614.8	6708735.3	383.9	36	-90/0.1	13	20	7	0.61
CMHL163	515614.8	6708735.3	383.9	36	-90/0.1	15	16	1	1.32
CMHL163	515614.8	6708735.3	383.9	36	-90/0.1	24	25	1	0.50

Hole No	Easting	Northing	RL	Hole Depth	Dip/Azi	From	To	Width	Grade (g/t Au)
CMHL164	515603.6	6708734.4	384.0	36	-90/0.1	3	5	2	0.71
CMHL164	515603.6	6708734.4	384.0	36	-90/0.1	9	12	3	1.02
CMHL164	515603.6	6708734.4	384.0	36	-90/0.1	15	22	7	0.44
CMHL165	515590.7	6708732.5	384.0	36	-90/0.1	2	3	1	0.68
CMHL165	515590.7	6708732.5	384.0	36	-90/0.1	9	25	16	0.62
CMHL165	515590.7	6708732.5	384.0	36	-90/0.1	14	15	1	1.92
CMHL166	515578.3	6708731.9	384.3	36	-90/0.1	6	11	5	0.58
CMHL166	515578.3	6708731.9	384.3	36	-90/0.1	14	20	6	0.78
CMHL166	515578.3	6708731.9	384.3	36	-90/0.1	15	17	2	1.07
CMHL167	515562.7	6708731.0	384.6	36	-90/0.1	2	21	19	0.85
CMHL167	515562.7	6708731.0	384.6	36	-90/0.1	8	9	1	2.12
CMHL167	515562.7	6708731.0	384.6	36	-90/0.1	15	20	5	1.27
CMHL167	515562.7	6708731.0	384.6	36	-90/0.1	25	28	3	0.60
CMHL168	515550.4	6708730.9	384.8	36	-90/0.1	7	12	5	0.61
CMHL168	515550.4	6708730.9	384.8	36	-90/0.1	24	28	4	1.75
CMHL168	515550.4	6708730.9	384.8	36	-90/0.1	27	28	1	5.05
CMHL169	515541.0	6708730.8	384.8	36	-90/0.1	4	7	3	0.78
CMHL169	515541.0	6708730.8	384.8	36	-90/0.1	24	25	1	0.77
CMHL170	515526.0	6708730.5	384.7	36	-90/0.1	3	4	1	0.70
CMHL172	515505.5	6708731.0	384.6	36	-90/0.1	3	4	1	0.52
CMHL172	515505.5	6708731.0	384.6	36	-90/0.1	20	21	1	0.81
CMHL172	515505.5	6708731.0	384.6	36	-90/0.1	24	30	6	1.04
CMHL173	515489.1	6708740.5	384.6	36	-90/0.1	3	4	1	1.08
CMHL173	515489.1	6708740.5	384.6	36	-90/0.1	3	11	8	0.56
CMHL174	515490.1	6708750.6	384.8	36	-90/0.1	30	31	1	0.79
CMHL175	515491.7	6708766.3	385.3	36	-90/0.1	2	3	1	0.54
CMHL175	515491.7	6708766.3	385.3	36	-90/0.1	9	10	1	4.77
CMHL175	515491.7	6708766.3	385.3	36	-90/0.1	13	14	1	1.21
CMHL175	515491.7	6708766.3	385.3	36	-90/0.1	25	31	6	0.53
CMHL175	515491.7	6708766.3	385.3	36	-90/0.1	28	29	1	1.16
CMHL176	515493.9	6708781.7	385.4	36	-90/0.1	4	5	1	0.50
CMHL176	515493.9	6708781.7	385.4	36	-90/0.1	18	19	1	0.69
CMHL176	515493.9	6708781.7	385.4	36	-90/0.1	29	32	3	0.60
CMHL177	515494.4	6708791.2	385.2	36	-90/0.1	22	23	1	0.53
CMHL177	515494.4	6708791.2	385.2	36	-90/0.1	30	32	2	0.71
CMHL178	515498.6	6708806.6	385.3	36	-90/0.1	7	8	1	0.72
CMHL178	515498.6	6708806.6	385.3	36	-90/0.1	27	28	1	0.65
CMHL178	515498.6	6708806.6	385.3	36	-90/0.1	31	33	2	1.21
CMHL178	515498.6	6708806.6	385.3	36	-90/0.1	32	33	1	1.63
CMHL179	515498.9	6708817.5	385.1	36	-90/0.1	16	17	1	1.34
CMHL180	515502.1	6708828.9	385.0	36	-90/0.1	14	15	1	2.42
CMHL180	515502.1	6708828.9	385.0	36	-90/0.1	29	30	1	0.70
CMHL180	515502.1	6708828.9	385.0	36	-90/0.1	35	36	1	0.60
CMHL181	515513.3	6708830.3	385.8	36	-90/0.1	3	7	4	0.56
CMHL181	515513.3	6708830.3	385.8	36	-90/0.1	16	17	1	4.59
CMHL182	515655.6	6708745.8	385.0	36	-90/0.1	2	7	5	0.76
CMHL182	515655.6	6708745.8	385.0	36	-90/0.1	3	4	1	1.31
CMHL182	515655.6	6708745.8	385.0	36	-90/0.1	11	17	6	0.64
CMHL182	515655.6	6708745.8	385.0	36	-90/0.1	22	25	3	0.45
CMHL182	515655.6	6708745.8	385.0	36	-90/0.1	28	30	2	0.60
CMHL183	515694.7	6708745.1	383.3	36	-90/0.1	2	3	1	1.43
CMHL183	515694.7	6708745.1	383.3	36	-90/0.1	9	10	1	0.55
CMHL183	515694.7	6708745.1	383.3	36	-90/0.1	15	17	2	0.75
CMHL184	515746.4	6708748.8	380.2	36	-90/0.1	19	21	2	0.65

Hole No	Easting	Northing	RL	Hole Depth	Dip/Azi	From	To	Width	Grade (g/t Au)
CMHL184	515746.4	6708748.8	380.2	36	-90/0.1	24	25	1	0.73
CMHL184	515746.4	6708748.8	380.2	36	-90/0.1	30	34	4	0.68
CMHL186	515745.4	6708790.3	380.5	33	-90/0.1	15	16	1	1.02
CMHL186	515745.4	6708790.3	380.5	33	-90/0.1	21	22	1	1.30
CMHL186	515745.4	6708790.3	380.5	33	-90/0.1	21	25	4	0.91
CMHL187	515746.4	6708814.9	380.3	33	-90/0.1	20	25	5	0.71
CMHL187	515746.4	6708814.9	380.3	33	-90/0.1	21	22	1	1.06
CMHL188	515744.0	6708839.1	380.2	33	-90/0.1	17	21	4	1.06
CMHL188	515744.0	6708839.1	380.2	33	-90/0.1	19	21	2	1.55
CMHL189	515728.4	6708850.6	381.9	36	-90/0.1	20	28	8	0.67
CMHL189	515728.4	6708850.6	381.9	36	-90/0.1	27	28	1	1.08
CMHL190	515729.4	6708835.9	381.8	33	-90/0.1	16	17	1	0.50
CMHL190	515729.4	6708835.9	381.8	33	-90/0.1	20	22	2	0.75
CMHL191	515730.5	6708822.2	382.0	35	-90/0.1	18	22	4	1.12
CMHL191	515730.5	6708822.2	382.0	35	-90/0.1	20	22	2	1.52
CMHL191	515730.5	6708822.2	382.0	35	-90/0.1	26	28	2	0.58
CMHL191	515730.5	6708822.2	382.0	35	-90/0.1	31	33	2	0.56
CMHL192	515731.6	6708808.1	382.0	36	-90/0.1	16	21	5	0.62
CMHL193	515731.9	6708798.3	381.5	35	-90/0.1	28	29	1	0.59
CMHL194	515730.4	6708787.8	381.5	36	-90/0.1	21	23	2	0.73
CMHL194	515730.4	6708787.8	381.5	36	-90/0.1	28	32	4	0.35
CMHL195	515726.8	6708774.2	381.9	33	-90/0.1	8	9	1	7.00
CMHL195	515726.8	6708774.2	381.9	33	-90/0.1	8	12	4	2.07
CMHL195	515726.8	6708774.2	381.9	33	-90/0.1	25	26	1	0.61
CMHL196	515726.3	6708760.5	381.4	33	-90/0.1	9	14	5	0.68
CMHL196	515726.3	6708760.5	381.4	33	-90/0.1	21	22	1	0.52
CMHL197	515725.8	6708748.0	380.8	33	-90/0.1	3	5	2	0.53
CMHL197	515725.8	6708748.0	380.8	33	-90/0.1	12	13	1	0.66
CMHL197	515725.8	6708748.0	380.8	33	-90/0.1	32	33	1	0.78
CMHL198	515753.8	6708733.0	380.2	33	-90/0.1	15	27	12	0.69
CMHL198	515753.8	6708733.0	380.2	33	-90/0.1	20	21	1	1.17
CMHL198	515753.8	6708733.0	380.2	33	-90/0.1	26	27	1	1.04
CMHL199	515762.0	6708749.8	380.0	33	-90/0.1	17	22	5	0.46
CMHL199	515762.0	6708749.8	380.0	33	-90/0.1	27	28	1	0.56
CMHL200	515763.7	6708764.3	380.2	33	-90/0.1	14	23	9	0.79
CMHL200	515763.7	6708764.3	380.2	33	-90/0.1	16	19	3	1.39
CMHL200	515763.7	6708764.3	380.2	33	-90/0.1	26	27	1	0.68
CMHL201	515763.8	6708778.7	380.4	33	-90/0.1	8	9	1	1.09
CMHL201	515763.8	6708778.7	380.4	33	-90/0.1	14	25	11	0.67
CMHL201	515763.8	6708778.7	380.4	33	-90/0.1	20	21	1	1.17
CMHL201	515763.8	6708778.7	380.4	33	-90/0.1	30	32	2	0.56
CMHL202	515762.7	6708804.6	380.2	30	-90/0.1	19	21	2	0.90
CMHL202	515762.7	6708804.6	380.2	30	-90/0.1	20	21	1	1.09
CMHL202	515762.7	6708804.6	380.2	30	-90/0.1	26	27	1	0.66
CMHL203	515761.4	6708815.8	380.3	33	-90/0.1	4	8	4	0.82
CMHL203	515761.4	6708815.8	380.3	33	-90/0.1	6	7	1	1.13
CMHL203	515761.4	6708815.8	380.3	33	-90/0.1	21	25	4	0.52
CMHL204	515758.2	6708827.7	380.1	33	-90/0.1	14	17	3	0.70
CMHL204	515758.2	6708827.7	380.1	33	-90/0.1	16	17	1	1.11
CMHL204	515758.2	6708827.7	380.1	33	-90/0.1	23	28	5	0.51
CMHL205	515756.6	6708838.9	380.2	33	-90/0.1	16	17	1	0.77
CMHL205	515756.6	6708838.9	380.2	33	-90/0.1	22	26	4	0.54
CMHL206	515757.2	6708851.6	380.1	33	-90/0.1	19	27	8	0.60
CMHL207	515454.6	6708714.4	373.8	24	-90/0.1	3	5	2	0.62

Hole No	Easting	Northing	RL	Hole Depth	Dip/Azi	From	To	Width	Grade (g/t Au)
CMHL207	515454.6	6708714.4	373.8	24	-90/0.1	9	10	1	0.51
CMHL209	515454.7	6708749.6	376.4	24	-90/0.1	22	23	1	0.60
CMHL210	515453.1	6708765.7	377.0	27	-90/0.1	18	22	4	0.57
CMHL211	515452.6	6708778.7	376.7	27	-90/0.1	4	8	4	0.55
CMHL212	515452.7	6708792.1	376.4	27	-90/0.1	5	11	6	0.51
CMHL212	515452.7	6708792.1	376.4	27	-90/0.1	21	23	2	0.91
CMHL213	515453.9	6708803.9	376.5	27	-90/0.1	3	4	1	0.80
CMHL213	515453.9	6708803.9	376.5	27	-90/0.1	12	13	1	0.84
CMHL213	515453.9	6708803.9	376.5	27	-90/0.1	18	21	3	0.68
CMHL213	515453.9	6708803.9	376.5	27	-90/0.1	25	26	1	0.66
CMHL214	515456.1	6708817.4	376.6	27	-90/0.1	5	9	4	0.46
CMHL214	515456.1	6708817.4	376.6	27	-90/0.1	16	17	1	0.57
CMHL214	515456.1	6708817.4	376.6	27	-90/0.1	20	23	3	0.65
CMHL216	515458.9	6708827.5	376.7	27	-90/0.1	12	15	3	0.93
CMHL216	515458.9	6708827.5	376.7	27	-90/0.1	21	24	3	0.64
CMHL217	515462.5	6708840.8	377.1	27	-90/0.1	2	3	1	0.54
CMHL217	515462.5	6708840.8	377.1	27	-90/0.1	14	15	1	0.76
CMHL218	515464.3	6708850.4	377.3	27	-90/0.1	1	3	2	0.74
CMHL218	515464.3	6708850.4	377.3	27	-90/0.1	7	9	2	0.87
CMHL218	515464.3	6708850.4	377.3	27	-90/0.1	16	17	1	0.58
CMHL219	515447.7	6708763.7	376.9	26	-90/0.1	9	10	1	0.64
CMHL219	515447.7	6708763.7	376.9	26	-90/0.1	13	14	1	0.53
CMHL219	515447.7	6708763.7	376.9	26	-90/0.1	17	23	6	0.63
CMHL220	515440.6	6708790.7	373.7	24	-90/0.1	9	20	11	0.63
CMHL221	515447.6	6708842.5	373.6	24	-90/0.1	0	1	1	0.50
CMHL222	515449.6	6708848.8	373.7	24	-90/0.1	2	5	3	0.50
CMHL222	515449.6	6708848.8	373.7	24	-90/0.1	15	16	1	1.30
CMHL222	515449.6	6708848.8	373.7	24	-90/0.1	20	21	1	0.82
CMHL223	515452.6	6708858.4	373.6	24	-90/0.1	3	4	1	1.90
CMHL224	515486.3	6708891.0	372.4	27	-90/0.1	6	9	3	0.72
CMHL224	515486.3	6708891.0	372.4	27	-90/0.1	15	16	1	0.50
CMHL225	515525.8	6708892.7	372.8	27	-90/0.1	10	11	1	0.98
CMHL227	515580.9	6708893.5	373.5	27	-90/0.1	5	13	8	0.71
CMHL227	515580.9	6708893.5	373.5	27	-90/0.1	6	9	3	1.06
CMHL228	515603.9	6708894.2	372.7	27	-90/0.1	2	3	1	0.68
CMHL228	515603.9	6708894.2	372.7	27	-90/0.1	6	7	1	0.57
CMHL228	515603.9	6708894.2	372.7	27	-90/0.1	15	19	4	0.55
CMHL229	515628.1	6708895.6	372.4	27	-90/0.1	2	3	1	0.51
CMHL229	515628.1	6708895.6	372.4	27	-90/0.1	10	17	7	0.62
CMHL230	515654.1	6708895.9	372.3	27	-90/0.1	6	10	4	0.63
CMHL230	515654.1	6708895.9	372.3	27	-90/0.1	17	18	1	0.59
CMHL232	515704.3	6708897.3	371.9	27	-90/0.1	8	21	13	0.90
CMHL232	515704.3	6708897.3	371.9	27	-90/0.1	10	20	10	0.95
CMHL233	515728.3	6708898.2	371.3	27	-90/0.1	2	3	1	0.50
CMHL233	515728.3	6708898.2	371.3	27	-90/0.1	9	13	4	0.44
CMHL234	515753.2	6708899.5	370.6	24	-90/0.1	0	17	17	0.56
CMHL235	515778.6	6708899.1	369.8	18	-90/0.1	4	8	4	0.68
CMHL235	515778.6	6708899.1	369.8	18	-90/0.1	14	18	4	0.73
CMHL235	515778.6	6708899.1	369.8	18	-90/0.1	17	18	1	1.39
CMHL237	515539.8	6708817.1	386.0	36	-90/0.1	7	9	2	0.93
CMHL237	515539.8	6708817.1	386.0	36	-90/0.1	8	9	1	1.35
CMHL238	515553.2	6708817.5	385.8	36	-90/0.1	6	7	1	0.59
CMHL238	515553.2	6708817.5	385.8	36	-90/0.1	27	28	1	0.50
CMHL238	515553.2	6708817.5	385.8	36	-90/0.1	31	32	1	0.72

Hole No	Easting	Northing	RL	Hole Depth	Dip/Azi	From	To	Width	Grade (g/t Au)
CMHL239	515561.8	6708817.8	385.8	36	-90/0.1	1	2	1	2.00
CMHL239	515561.8	6708817.8	385.8	36	-90/0.1	8	15	7	0.70
CMHL239	515561.8	6708817.8	385.8	36	-90/0.1	22	23	1	1.81
CMHL240	515577.0	6708819.2	385.9	36	-90/0.1	1	3	2	0.63
CMHL240	515577.0	6708819.2	385.9	36	-90/0.1	11	14	3	0.58
CMHL240	515577.0	6708819.2	385.9	36	-90/0.1	20	22	2	0.70
CMHL241	515592.1	6708819.5	385.7	36	-90/0.1	4	6	2	0.77
CMHL242	515603.1	6708820.8	385.6	36	-90/0.1	6	12	6	0.65
CMHL242	515603.1	6708820.8	385.6	36	-90/0.1	15	16	1	0.89
CMHL243	515612.5	6708821.5	385.7	36	-90/0.1	20	25	5	0.64
CMHL244	515655.5	6708820.2	385.5	36	-90/0.1	3	6	3	0.47
CMHL244	515655.5	6708820.2	385.5	36	-90/0.1	11	17	6	0.41
CMHL244	515655.5	6708820.2	385.5	36	-90/0.1	24	31	7	0.52
CMHL245	515678.5	6708820.4	385.6	36	-90/0.1	29	31	2	0.65
CMHL246	515703.1	6708819.2	385.6	36	-90/0.1	14	27	13	0.59
CMHL246	515703.1	6708819.2	385.6	36	-90/0.1	22	23	1	1.05
CMHL247	515714.1	6708808.5	385.6	36	-90/0.1	3	4	1	0.81
CMHL247	515714.1	6708808.5	385.6	36	-90/0.1	20	22	2	0.67
CMHL247	515714.1	6708808.5	385.6	36	-90/0.1	28	29	1	0.63
CMHL248	515700.4	6708809.8	385.5	36	-90/0.1	5	6	1	0.67
CMHL248	515700.4	6708809.8	385.5	36	-90/0.1	18	19	1	3.70
CMHL248	515700.4	6708809.8	385.5	36	-90/0.1	18	20	2	2.24
CMHL249	515690.1	6708809.9	385.4	36	-90/0.1	7	8	1	0.54
CMHL249	515690.1	6708809.9	385.4	36	-90/0.1	14	15	1	0.75
CMHL249	515690.1	6708809.9	385.4	36	-90/0.1	23	24	1	1.43
CMHL249	515690.1	6708809.9	385.4	36	-90/0.1	23	28	5	0.75
CMHL250	515679.1	6708808.9	385.2	36	-90/0.1	11	15	4	0.43
CMHL250	515679.1	6708808.9	385.2	36	-90/0.1	22	30	8	0.61
CMHL251	515666.7	6708809.3	385.2	36	-90/0.1	5	6	1	0.86
CMHL251	515666.7	6708809.3	385.2	36	-90/0.1	24	29	5	0.57
CMHL252	515656.1	6708809.8	385.2	36	-90/0.1	9	10	1	2.75
CMHL252	515656.1	6708809.8	385.2	36	-90/0.1	13	14	1	1.21
CMHL252	515656.1	6708809.8	385.2	36	-90/0.1	13	15	2	0.91
CMHL252	515656.1	6708809.8	385.2	36	-90/0.1	21	28	7	0.54
CMHL253	515641.9	6708810.6	385.0	32	-90/0.1	3	7	4	0.97
CMHL253	515641.9	6708810.6	385.0	32	-90/0.1	3	10	7	0.84
CMHL253	515641.9	6708810.6	385.0	32	-90/0.1	13	17	4	0.47
CMHL253	515641.9	6708810.6	385.0	32	-90/0.1	21	22	1	0.70
CMHL253	515641.9	6708810.6	385.0	32	-90/0.1	25	29	4	0.41
CMHL254	515613.3	6708810.2	385.6	36	-90/0.1	3	7	4	0.57
CMHL254	515613.3	6708810.2	385.6	36	-90/0.1	12	13	1	0.54
CMHL254	515613.3	6708810.2	385.6	36	-90/0.1	22	24	2	0.59
CMHL255	515603.5	6708809.5	385.7	36	-90/0.1	0	5	5	1.17
CMHL255	515603.5	6708809.5	385.7	36	-90/0.1	2	4	2	2.07
CMHL255	515603.5	6708809.5	385.7	36	-90/0.1	15	16	1	0.90
CMHL256	515591.7	6708808.8	385.8	36	-90/0.1	0	3	3	0.62
CMHL256	515591.7	6708808.8	385.8	36	-90/0.1	16	18	2	1.92
CMHL256	515591.7	6708808.8	385.8	36	-90/0.1	16	22	6	1.09
CMHL256	515591.7	6708808.8	385.8	36	-90/0.1	21	22	1	1.24
CMHL257	515579.9	6708808.7	385.9	36	-90/0.1	1	3	2	0.81
CMHL257	515579.9	6708808.7	385.9	36	-90/0.1	6	7	1	0.55
CMHL257	515579.9	6708808.7	385.9	36	-90/0.1	12	16	4	0.57
CMHL257	515579.9	6708808.7	385.9	36	-90/0.1	19	20	1	0.67
CMHL258	515565.3	6708808.2	385.7	36	-90/0.1	12	19	7	0.67

Hole No	Easting	Northing	RL	Hole Depth	Dip/Azi	From	To	Width	Grade (g/t Au)
CMHL258	515565.3	6708808.2	385.7	36	-90/0.1	18	19	1	1.06
CMHL258	515565.3	6708808.2	385.7	36	-90/0.1	35	36	1	0.60
CMHL259	515553.0	6708807.5	385.7	36	-90/0.1	1	2	1	0.54
CMHL259	515553.0	6708807.5	385.7	36	-90/0.1	6	7	1	1.29
CMHL259	515553.0	6708807.5	385.7	36	-90/0.1	6	8	2	0.90
CMHL261	515528.6	6708806.7	385.9	38	-90/0.1	1	2	1	0.55
CMHL262	515512.7	6708808.0	386.3	36	-90/0.1	4	5	1	0.68
CMHL263	515552.3	6708796.7	386.4	36	-90/0.1	2	7	5	0.79
CMHL263	515552.3	6708796.7	386.4	36	-90/0.1	6	7	1	2.09
CMHL264	515577.3	6708796.8	386.1	36	-90/0.1	12	20	8	0.55
CMHL265	515602.4	6708796.3	385.9	36	-90/0.1	34	36	2	0.80
CMHL265	515602.4	6708796.3	385.9	36	-90/0.1	35	36	1	1.00
CMHL266	515629.4	6708795.9	385.8	39	-90/0.1	2	8	6	0.64
CMHL266	515629.4	6708795.9	385.8	39	-90/0.1	14	15	1	1.75
CMHL266	515629.4	6708795.9	385.8	39	-90/0.1	22	23	1	0.57
CMHL266	515629.4	6708795.9	385.8	39	-90/0.1	26	27	1	0.89
CMHL267	515655.1	6708797.2	385.4	36	-90/0.1	1	6	5	0.58
CMHL267	515655.1	6708797.2	385.4	36	-90/0.1	13	17	4	0.63
CMHL267	515655.1	6708797.2	385.4	36	-90/0.1	30	31	1	0.54
CMHL268	515679.3	6708796.9	385.4	19	-90/0.1	14	15	1	0.53
CMHL269	515703.5	6708795.5	385.6	36	-90/0.1	5	6	1	0.94
CMHL269	515703.5	6708795.5	385.6	36	-90/0.1	17	18	1	1.93
CMHL270	515711.5	6708784.8	385.5	36	-90/0.1	6	7	1	0.50
CMHL270	515711.5	6708784.8	385.5	36	-90/0.1	20	25	5	0.82
CMHL270	515711.5	6708784.8	385.5	36	-90/0.1	21	23	2	1.08
CMHL271	515700.6	6708784.8	385.5	36	-90/0.1	4	5	1	0.94
CMHL271	515700.6	6708784.8	385.5	36	-90/0.1	16	17	1	0.53
CMHL272	515686.7	6708784.9	385.4	36	-90/0.1	4	5	1	0.57
CMHL272	515686.7	6708784.9	385.4	36	-90/0.1	22	24	2	0.78
CMHL272	515686.7	6708784.9	385.4	36	-90/0.1	23	24	1	1.02
CMHL272	515686.7	6708784.9	385.4	36	-90/0.1	27	28	1	0.87
CMHL273	515677.7	6708784.9	385.6	59	-90/0.1	1	2	1	0.66
CMHL273	515677.7	6708784.9	385.6	59	-90/0.1	16	17	1	2.41
CMHL273	515677.7	6708784.9	385.6	59	-90/0.1	16	18	2	1.64
CMHL273	515677.7	6708784.9	385.6	59	-90/0.1	21	22	1	0.59
CMHL274	515665.0	6708784.9	385.5	36	-90/0.1	3	6	3	1.01
CMHL274	515665.0	6708784.9	385.5	36	-90/0.1	9	13	4	3.33
CMHL274	515665.0	6708784.9	385.5	36	-90/0.1	9	16	7	2.23
CMHL274	515665.0	6708784.9	385.5	36	-90/0.1	22	25	3	0.69
CMHL275	515654.2	6708785.0	385.3	36	-90/0.1	2	9	7	0.44
CMHL275	515654.2	6708785.0	385.3	36	-90/0.1	21	22	1	1.38
CMHL275	515654.2	6708785.0	385.3	36	-90/0.1	21	25	4	0.72
CMHL276	515642.8	6708785.0	385.1	36	-90/0.1	2	7	5	0.56
CMHL276	515642.8	6708785.0	385.1	36	-90/0.1	13	14	1	0.52
CMHL276	515642.8	6708785.0	385.1	36	-90/0.1	21	22	1	0.55
CMHL277	515579.0	6708785.1	385.8	71	-90/0.1	12	21	9	0.84
CMHL277	515579.0	6708785.1	385.8	71	-90/0.1	15	18	3	1.17
CMHL277	515579.0	6708785.1	385.8	71	-90/0.1	34	35	1	0.56
CMHL278	515577.9	6708741.4	386.2	76	-90/0.1	3	6	3	0.53
CMHL278	515577.9	6708741.4	386.2	76	-90/0.1	10	24	14	0.74
CMHL278	515577.9	6708741.4	386.2	76	-90/0.1	14	15	1	1.40
CMHL278	515577.9	6708741.4	386.2	76	-90/0.1	20	21	1	1.12
CMHL278	515577.9	6708741.4	386.2	76	-90/0.1	68	72	4	0.76
CMHL279	515487.4	6708730.4	384.1	55	-90/0.1	0	1	1	0.55

Hole No	Easting	Northing	RL	Hole Depth	Dip/Azi	From	To	Width	Grade (g/t Au)
CMHL279	515487.4	6708730.4	384.1	55	-90/0.1	6	9	3	0.63
CMHL279	515487.4	6708730.4	384.1	55	-90/0.1	16	17	1	1.98
CMHL279	515487.4	6708730.4	384.1	55	-90/0.1	16	26	10	0.75
CMHL279	515487.4	6708730.4	384.1	55	-90/0.1	29	30	1	0.92
CMHL280	515631.6	6708785.1	385.0	36	-90/0.1	1	4	3	0.78
CMHL280	515631.6	6708785.1	385.0	36	-90/0.1	3	4	1	1.16
CMHL280	515631.6	6708785.1	385.0	36	-90/0.1	7	8	1	0.62
CMHL280	515631.6	6708785.1	385.0	36	-90/0.1	18	19	1	0.88
CMHL281	515616.7	6708783.3	385.7	36	-90/0.1	6	7	1	0.53
CMHL282	515603.3	6708783.6	385.5	36	-90/0.1	31	32	1	0.61
CMHL283	515589.2	6708784.5	385.9	36	-90/0.1	14	22	8	0.49
CMHL283	515589.2	6708784.5	385.9	36	-90/0.1	34	35	1	0.50
CMHL284	515565.6	6708784.4	385.9	36	-90/0.1	13	19	6	1.23
CMHL285	515551.6	6708784.2	386.1	36	-90/0.1	1	2	1	1.08
CMHL285	515551.6	6708784.2	386.1	36	-90/0.1	1	3	2	0.81
CMHL285	515551.6	6708784.2	386.1	36	-90/0.1	18	19	1	0.55
CMHL286	515539.5	6708783.7	386.2	36	-90/0.1	4	5	1	1.17
CMHL286	515539.5	6708783.7	386.2	36	-90/0.1	4	9	5	0.75
CMHL286	515539.5	6708783.7	386.2	36	-90/0.1	13	14	1	0.71
CMHL286	515539.5	6708783.7	386.2	36	-90/0.1	29	32	3	0.97
CMHL286	515539.5	6708783.7	386.2	36	-90/0.1	30	31	1	1.05
CMHL287	515524.5	6708784.5	386.2	36	-90/0.1	29	33	4	0.66
CMHL287	515524.5	6708784.5	386.2	36	-90/0.1	30	31	1	1.25
CMHL288	515505.9	6708782.0	386.5	36	-90/0.1	5	6	1	0.52
CMHL288	515505.9	6708782.0	386.5	36	-90/0.1	22	24	2	0.65
CMHL289	515526.5	6708767.4	386.0	39	-90/0.1	33	34	1	0.70
CMHL291	515578.7	6708769.2	385.7	36	-90/0.1	5	18	13	0.56
CMHL291	515578.7	6708769.2	385.7	36	-90/0.1	14	15	1	1.05
CMHL291	515578.7	6708769.2	385.7	36	-90/0.1	33	35	2	0.71
CMHL292	515603.7	6708769.4	385.5	36	-90/0.1	33	36	3	0.55
CMHL293	515629.8	6708770.4	385.5	36	-90/0.1	22	23	1	0.50
CMHL293	515629.8	6708770.4	385.5	36	-90/0.1	27	28	1	1.26
CMHL294	515653.1	6708770.5	385.3	36	-90/0.1	2	7	5	0.50
CMHL294	515653.1	6708770.5	385.3	36	-90/0.1	11	16	5	0.59
CMHL294	515653.1	6708770.5	385.3	36	-90/0.1	21	26	5	0.64
CMHL295	515680.2	6708770.9	385.5	36	-90/0.1	11	15	4	0.75
CMHL296	515703.6	6708762.7	385.4	36	-90/0.1	16	17	1	0.60
CMHL296	515703.6	6708762.7	385.4	36	-90/0.1	21	22	1	0.70
CMHL296	515703.6	6708762.7	385.4	36	-90/0.1	25	29	4	0.46
CMHL297	515680.5	6708757.4	385.3	36	-90/0.1	0	8	8	1.47
CMHL297	515680.5	6708757.4	385.3	36	-90/0.1	3	6	3	3.03
CMHL297	515680.5	6708757.4	385.3	36	-90/0.1	12	18	6	0.64
CMHL298	515654.4	6708757.6	385.6	36	-90/0.1	0	6	6	1.07
CMHL298	515654.4	6708757.6	385.6	36	-90/0.1	3	6	3	1.48
CMHL298	515654.4	6708757.6	385.6	36	-90/0.1	14	16	2	1.38
CMHL298	515654.4	6708757.6	385.6	36	-90/0.1	14	17	3	1.09
CMHL298	515654.4	6708757.6	385.6	36	-90/0.1	23	26	3	0.67
CMHL299	515630.3	6708755.8	385.2	36	-90/0.1	5	7	2	0.67
CMHL299	515630.3	6708755.8	385.2	36	-90/0.1	23	26	3	0.55
CMHL300	515614.2	6708758.4	385.3	36	-90/0.1	3	8	5	0.94
CMHL300	515614.2	6708758.4	385.3	36	-90/0.1	6	8	2	1.21
CMHL300	515614.2	6708758.4	385.3	36	-90/0.1	21	28	7	0.62
CMHL301	515603.3	6708755.8	385.5	36	-90/0.1	2	10	8	0.60
CMHL301	515603.3	6708755.8	385.5	36	-90/0.1	14	17	3	0.47

Hole No	Easting	Northing	RL	Hole Depth	Dip/Azi	From	To	Width	Grade (g/t Au)
CMHL301	515603.3	6708755.8	385.5	36	-90/0.1	32	33	1	0.68
CMHL302	515589.6	6708754.1	2.0	36	-90/0.1	4	5	1	0.61
CMHL302	515589.6	6708754.1	2.0	36	-90/0.1	11	21	10	1.00
CMHL302	515589.6	6708754.1	2.0	36	-90/0.1	18	19	1	4.58
CMHL303	515580.1	6708753.6	385.6	36	-90/0.1	6	21	15	0.72
CMHL303	515580.1	6708753.6	385.6	36	-90/0.1	12	15	3	1.22
CMHL303	515580.1	6708753.6	385.6	36	-90/0.1	20	21	1	1.01
CMHL304	515565.9	6708752.4	385.7	36	-90/0.1	11	12	1	0.51
CMHL304	515565.9	6708752.4	385.7	36	-90/0.1	15	23	8	0.50
CMHL305	515553.4	6708751.7	385.6	36	-90/0.1	3	4	1	0.61
CMHL305	515553.4	6708751.7	385.6	36	-90/0.1	8	13	5	0.82
CMHL305	515553.4	6708751.7	385.6	36	-90/0.1	9	10	1	1.75
CMHL305	515553.4	6708751.7	385.6	36	-90/0.1	17	18	1	1.02
CMHL305	515553.4	6708751.7	385.6	36	-90/0.1	28	32	4	0.53
CMHL306	515541.0	6708751.0	385.6	36	-90/0.1	4	5	1	0.53
CMHL306	515541.0	6708751.0	385.6	36	-90/0.1	25	26	1	1.47
CMHL307	515525.8	6708751.6	385.9	36	-90/0.1	23	24	1	1.15
CMHL307	515525.8	6708751.6	385.9	36	-90/0.1	23	27	4	0.60
CMHL308	515515.5	6708751.5	386.0	37	-90/0.1	2	4	2	0.67
CMHL309	515500.8	6708750.4	386.3	36	-90/0.1	27	28	1	0.56
CMHL309	515500.8	6708750.4	386.3	36	-90/0.1	31	32	1	0.63
CMHL310	515501.9	6708741.9	386.6	36	-90/0.1	3	8	5	0.76
CMHL310	515501.9	6708741.9	386.6	36	-90/0.1	5	6	1	1.05
CMHL310	515501.9	6708741.9	386.6	36	-90/0.1	28	29	1	0.52
CMHL311	515524.8	6708738.3	386.6	39	-90/0.1	7	8	1	1.72
CMHL312	515548.4	6708739.5	386.3	36	-90/0.1	7	8	1	0.52
CMHL312	515548.4	6708739.5	386.3	36	-90/0.1	25	33	8	0.84
CMHL313	515600.3	6708745.0	385.9	39	-90/0.1	5	10	5	0.67
CMHL313	515600.3	6708745.0	385.9	39	-90/0.1	18	19	1	0.52
CMHL313	515600.3	6708745.0	385.9	39	-90/0.1	33	34	1	0.76
CMHL314	515628.0	6708747.8	385.3	31	-90/0.1	10	15	5	0.73
CMHL314	515628.0	6708747.8	385.3	31	-90/0.1	18	20	2	0.54
CMHL314	515628.0	6708747.8	385.3	31	-90/0.1	26	30	4	1.00
CMHL315	515674.2	6708745.4	384.1	33	-90/0.1	1	6	5	0.69
CMHL315	515674.2	6708745.4	384.1	33	-90/0.1	11	12	1	0.78
CMHL315	515674.2	6708745.4	384.1	33	-90/0.1	29	30	1	0.59
CMHL316	515625.0	6708831.9	386.3	39	-90/0.1	25	30	5	0.90
CMHL316	515625.0	6708831.9	386.3	39	-90/0.1	35	37	2	0.52
CMHL317	515625.4	6708810.4	386.4	36	-90/0.1	4	10	6	1.04
CMHL317	515625.4	6708810.4	386.4	36	-90/0.1	21	22	1	0.72
CMHL317	515625.4	6708810.4	386.4	36	-90/0.1	29	33	4	0.58
CMHL318	515713.6	6708835.6	385.5	36	-90/0.1	20	25	5	0.90
CMHL318	515713.6	6708835.6	385.5	36	-90/0.1	23	25	2	1.40
CMHL319	515761.8	6708790.8	380.3	33	-90/0.1	15	18	3	1.07
CMHL319	515761.8	6708790.8	380.3	33	-90/0.1	15	28	13	0.87
CMHL319	515761.8	6708790.8	380.3	33	-90/0.1	23	24	1	2.81
CMHL320	515774.4	6708721.9	376.7	63	-90/0.1	1	2	1	0.69
CMHL320	515774.4	6708721.9	376.7	63	-90/0.1	6	13	7	0.75
CMHL320	515774.4	6708721.9	376.7	63	-90/0.1	11	12	1	1.34
CMHL320	515774.4	6708721.9	376.7	63	-90/0.1	19	21	2	0.88
CMHL320	515774.4	6708721.9	376.7	63	-90/0.1	20	21	1	1.21
CMHL320	515774.4	6708721.9	376.7	63	-90/0.1	27	30	3	0.56
CMHL321	515787.9	6708739.4	376.7	30	-90/0.1	0	3	3	0.90
CMHL321	515787.9	6708739.4	376.7	30	-90/0.1	1	2	1	1.26

Hole No	Easting	Northing	RL	Hole Depth	Dip/Azi	From	To	Width	Grade (g/t Au)
CMHL321	515787.9	6708739.4	376.7	30	-90/0.1	6	9	3	0.79
CMHL321	515787.9	6708739.4	376.7	30	-90/0.1	13	21	8	0.75
CMHL321	515787.9	6708739.4	376.7	30	-90/0.1	18	19	1	1.77
CMHL323	515772.1	6708872.8	377.2	60	-90/0.1	10	11	1	1.11
CMHL323	515772.1	6708872.8	377.2	60	-90/0.1	10	20	10	0.60
CMHL323	515772.1	6708872.8	377.2	60	-90/0.1	23	24	1	1.79
CMHL325	515576.3	6708868.7	380.2	70	-90/0.1	1	3	2	1.61
CMHL325	515576.3	6708868.7	380.2	70	-90/0.1	1	8	7	1.19
CMHL325	515576.3	6708868.7	380.2	70	-90/0.1	6	7	1	2.17
CMHL325	515576.3	6708868.7	380.2	70	-90/0.1	14	16	2	0.71
CMHL326	515466.7	6708791.5	380.0	53	-90/0.1	1	3	2	0.66
CMHL326	515466.7	6708791.5	380.0	53	-90/0.1	7	11	4	0.50
CMHL326	515466.7	6708791.5	380.0	53	-90/0.1	19	23	4	0.58
CMHL327	515575.8	6708702.3	375.0	58	-90/0.1	3	5	2	1.48
CMHL327	515575.8	6708702.3	375.0	58	-90/0.1	4	5	1	2.10
CMHL327	515575.8	6708702.3	375.0	58	-90/0.1	8	9	1	0.65
CMHL328	515472.2	6708877.6	373.6	32	-90/0.1	9	10	1	0.59
CMRC0605	516908.2	6710645.0	345.7	294	-59.88/286.1	6	7	1	1.78
CMRC0605	516908.2	6710645.0	345.7	294	-59.88/286.1	45	46	1	1.08
CMRC0605	516908.2	6710645.0	345.7	294	-59.88/286.1	61	62	1	0.65
CMRC0605	516908.2	6710645.0	345.7	294	-59.88/286.1	119	124	5	0.80
CMRC0605	516908.2	6710645.0	345.7	294	-59.88/286.1	132	134	2	10.25
CMRC0605	516908.2	6710645.0	345.7	294	-59.88/286.1	137	141	4	0.45
CMRC0605	516908.2	6710645.0	345.7	294	-59.88/286.1	174	175	1	1.42
CMRC0605	516908.2	6710645.0	345.7	294	-59.88/286.1	179	193	14	1.68
CMRC0605	516908.2	6710645.0	345.7	294	-59.88/286.1	200	201	1	0.72
CMRC0605	516908.2	6710645.0	345.7	294	-59.88/286.1	207	209	2	3.86
CMRC0605	516908.2	6710645.0	345.7	294	-59.88/286.1	213	216	3	7.20
CMRC0605	516908.2	6710645.0	345.7	294	-59.88/286.1	221	225	4	1.56
CMRC0605	516908.2	6710645.0	345.7	294	-59.88/286.1	243	249	6	0.80
CMRC0605	516908.2	6710645.0	345.7	294	-59.88/286.1	252	254	2	0.89
CMRC0605	516908.2	6710645.0	345.7	294	-59.88/286.1	263	267	4	1.73
CMRC0605	516908.2	6710645.0	345.7	294	-59.88/286.1	277	278	1	0.52
CMRC0606	516904.5	6710558.3	341.2	216	-58.73/288.7	7	8	1	0.54
CMRC0606	516904.5	6710558.3	341.2	216	-58.73/288.7	23	28	5	0.66
CMRC0606	516904.5	6710558.3	341.2	216	-58.73/288.7	70	74	4	0.75
CMRC0606	516904.5	6710558.3	341.2	216	-58.73/288.7	78	80	2	6.04
CMRC0606	516904.5	6710558.3	341.2	216	-58.73/288.7	84	89	5	2.07
CMRC0606	516904.5	6710558.3	341.2	216	-58.73/288.7	150	152	2	0.77
CMRC0606	516904.5	6710558.3	341.2	216	-58.73/288.7	162	163	1	0.83
CMRC0606	516904.5	6710558.3	341.2	216	-58.73/288.7	169	176	7	0.80
CMRC0606	516904.5	6710558.3	341.2	216	-58.73/288.7	183	186	3	0.58
CMRC0606	516904.5	6710558.3	341.2	216	-58.73/288.7	194	196	2	10.69
CMRC0607	516835.2	6710331.2	335.2	246	-63.25/290.2	12	13	1	0.53
CMRC0607	516835.2	6710331.2	335.2	246	-63.25/290.2	50	54	4	0.63
CMRC0607	516835.2	6710331.2	335.2	246	-63.25/290.2	107	108	1	1.55
CMRC0607	516835.2	6710331.2	335.2	246	-63.25/290.2	112	113	1	2.70
CMRC0607	516835.2	6710331.2	335.2	246	-63.25/290.2	117	118	1	0.94
CMRC0607	516835.2	6710331.2	335.2	246	-63.25/290.2	134	136	2	12.48
CMRC0607	516835.2	6710331.2	335.2	246	-63.25/290.2	171	174	3	0.99
CMRC0607	516835.2	6710331.2	335.2	246	-63.25/290.2	180	183	3	2.43
CMRC0607	516835.2	6710331.2	335.2	246	-63.25/290.2	193	194	1	0.79
CMRC0607	516835.2	6710331.2	335.2	246	-63.25/290.2	200	201	1	0.63
CMRC0607	516835.2	6710331.2	335.2	246	-63.25/290.2	216	218	2	2.23

Hole No	Easting	Northing	RL	Hole Depth	Dip/Azi	From	To	Width	Grade (g/t Au)
CMRC0607	516835.2	6710331.2	335.2	246	-63.25/290.2	227	239	12	2.81
CMRC0608	516804.0	6710296.2	330.5	204	-58.88/289.6	6	10	4	0.69
CMRC0608	516804.0	6710296.2	330.5	204	-58.88/289.6	77	81	4	2.80
CMRC0608	516804.0	6710296.2	330.5	204	-58.88/289.6	87	90	3	0.79
CMRC0608	516804.0	6710296.2	330.5	204	-58.88/289.6	98	100	2	1.36
CMRC0608	516804.0	6710296.2	330.5	204	-58.88/289.6	108	109	1	0.78
CMRC0608	516804.0	6710296.2	330.5	204	-58.88/289.6	126	134	8	0.55
CMRC0608	516804.0	6710296.2	330.5	204	-58.88/289.6	159	162	3	1.32
CMRC0608	516804.0	6710296.2	330.5	204	-58.88/289.6	170	176	6	1.31
CMRC0608	516804.0	6710296.2	330.5	204	-58.88/289.6	188	189	1	5.01
CMRC0609	516825.0	6710291.1	329.9	246	-59.99/285.8	7	8	1	0.78
CMRC0609	516825.0	6710291.1	329.9	246	-59.99/285.8	101	102	1	0.57
CMRC0609	516825.0	6710291.1	329.9	246	-59.99/285.8	120	121	1	2.19
CMRC0609	516825.0	6710291.1	329.9	246	-59.99/285.8	130	132	2	1.15
CMRC0609	516825.0	6710291.1	329.9	246	-59.99/285.8	141	142	1	0.70
CMRC0609	516825.0	6710291.1	329.9	246	-59.99/285.8	180	181	1	0.52
CMRC0609	516825.0	6710291.1	329.9	246	-59.99/285.8	185	190	5	1.00
CMRC0609	516825.0	6710291.1	329.9	246	-59.99/285.8	196	199	3	1.03
CMRC0609	516825.0	6710291.1	329.9	246	-59.99/285.8	210	214	4	1.68
CMRC0609	516825.0	6710291.1	329.9	246	-59.99/285.8	218	219	1	2.47
CMRC0609	516825.0	6710291.1	329.9	246	-59.99/285.8	228	229	1	0.79
CMRC0609	516825.0	6710291.1	329.9	246	-59.99/285.8	235	236	1	1.65
CMRC0609	516825.0	6710291.1	329.9	246	-59.99/285.8	240	244	4	1.19
CMRC0610	516794.7	6710260.6	330.5	180	-55.93/288.6	94	95	1	4.15
CMRC0610	516794.7	6710260.6	330.5	180	-55.93/288.6	101	102	1	0.50
CMRC0610	516794.7	6710260.6	330.5	180	-55.93/288.6	109	110	1	33.70
CMRC0610	516794.7	6710260.6	330.5	180	-55.93/288.6	129	131	2	3.20
CMRC0610	516794.7	6710260.6	330.5	180	-55.93/288.6	139	140	1	0.69
CMRC0610	516794.7	6710260.6	330.5	180	-55.93/288.6	144	151	7	0.69
CMRC0610	516794.7	6710260.6	330.5	180	-55.93/288.6	158	159	1	0.71
CMRC0610	516794.7	6710260.6	330.5	180	-55.93/288.6	162	168	6	1.07
CMRC0611	516814.7	6710252.1	330.1	246	-59.31/285.8	89	90	1	0.99
CMRC0611	516814.7	6710252.1	330.1	246	-59.31/285.8	107	108	1	0.51
CMRC0611	516814.7	6710252.1	330.1	246	-59.31/285.8	114	115	1	1.32
CMRC0611	516814.7	6710252.1	330.1	246	-59.31/285.8	124	127	3	0.86
CMRC0611	516814.7	6710252.1	330.1	246	-59.31/285.8	132	133	1	5.53
CMRC0611	516814.7	6710252.1	330.1	246	-59.31/285.8	163	168	5	0.90
CMRC0611	516814.7	6710252.1	330.1	246	-59.31/285.8	176	178	2	2.47
CMRC0611	516814.7	6710252.1	330.1	246	-59.31/285.8	189	190	1	0.86
CMRC0611	516814.7	6710252.1	330.1	246	-59.31/285.8	194	204	10	1.92
CMRC0611	516814.7	6710252.1	330.1	246	-59.31/285.8	209	210	1	2.01
CMRC0611	516814.7	6710252.1	330.1	246	-59.31/285.8	221	225	4	0.58
CMRC0611	516814.7	6710252.1	330.1	246	-59.31/285.8	228	231	3	1.42
CMRC0612	516763.7	6710238.9	330.3	228	-53.23/298.5	8	10	2	0.76
CMRC0612	516763.7	6710238.9	330.3	228	-53.23/298.5	43	48	5	1.35
CMRC0612	516763.7	6710238.9	330.3	228	-53.23/298.5	65	66	1	0.69
CMRC0612	516763.7	6710238.9	330.3	228	-53.23/298.5	91	92	1	4.97
CMRC0612	516763.7	6710238.9	330.3	228	-53.23/298.5	102	105	3	1.51
CMRC0612	516763.7	6710238.9	330.3	228	-53.23/298.5	115	126	11	1.55
CMRC0612	516763.7	6710238.9	330.3	228	-53.23/298.5	130	132	2	3.26
CMRC0612	516763.7	6710238.9	330.3	228	-53.23/298.5	135	136	1	0.52
CMRC0612	516763.7	6710238.9	330.3	228	-53.23/298.5	141	142	1	0.56
CMRC0612	516763.7	6710238.9	330.3	228	-53.23/298.5	174	175	1	2.89
CMRC0612	516763.7	6710238.9	330.3	228	-53.23/298.5	215	216	1	1.06

Hole No	Easting	Northing	RL	Hole Depth	Dip/Azi	From	To	Width	Grade (g/t Au)
CMRC0612	516763.7	6710238.9	330.3	228	-53.23/298.5	220	222	2	0.76
CMRC0612	516763.7	6710238.9	330.3	228	-53.23/298.5	225	227	2	2.03
CMRC0613	516763.0	6710226.3	330.4	180	-48.36/302.5	6	10	4	0.73
CMRC0613	516763.0	6710226.3	330.4	180	-48.36/302.5	43	51	8	4.95
CMRC0613	516763.0	6710226.3	330.4	180	-48.36/302.5	57	61	4	0.53
CMRC0613	516763.0	6710226.3	330.4	180	-48.36/302.5	82	87	5	1.08
CMRC0613	516763.0	6710226.3	330.4	180	-48.36/302.5	104	106	2	1.59
CMRC0613	516763.0	6710226.3	330.4	180	-48.36/302.5	111	129	18	0.96
CMRC0613	516763.0	6710226.3	330.4	180	-48.36/302.5	132	138	6	0.42
CMRC0613	516763.0	6710226.3	330.4	180	-48.36/302.5	164	168	4	0.71
CMRC0614	516763.4	6710216.1	330.3	198	-59.66/285.5	4	6	2	0.78
CMRC0614	516763.4	6710216.1	330.3	198	-59.66/285.5	47	48	1	0.82
CMRC0614	516763.4	6710216.1	330.3	198	-59.66/285.5	74	82	8	3.77
CMRC0614	516763.4	6710216.1	330.3	198	-59.66/285.5	89	90	1	0.59
CMRC0614	516763.4	6710216.1	330.3	198	-59.66/285.5	96	100	4	2.54
CMRC0614	516763.4	6710216.1	330.3	198	-59.66/285.5	122	123	1	0.55
CMRC0614	516763.4	6710216.1	330.3	198	-59.66/285.5	126	130	4	0.67
CMRC0614	516763.4	6710216.1	330.3	198	-59.66/285.5	134	135	1	1.64
CMRC0614	516763.4	6710216.1	330.3	198	-59.66/285.5	139	140	1	12.30
CMRC0614	516763.4	6710216.1	330.3	198	-59.66/285.5	143	151	8	0.68
CMRC0614	516763.4	6710216.1	330.3	198	-59.66/285.5	156	161	5	1.91
CMRC0614	516763.4	6710216.1	330.3	198	-59.66/285.5	166	168	2	2.12
CMRC0614	516763.4	6710216.1	330.3	198	-59.66/285.5	186	191	5	3.76
CMRC0615	516780.8	6710220.7	330.5	240	-61.67/287.6	54	57	3	0.54
CMRC0615	516780.8	6710220.7	330.5	240	-61.67/287.6	89	90	1	0.50
CMRC0615	516780.8	6710220.7	330.5	240	-61.67/287.6	99	102	3	0.42
CMRC0615	516780.8	6710220.7	330.5	240	-61.67/287.6	105	108	3	0.75
CMRC0615	516780.8	6710220.7	330.5	240	-61.67/287.6	138	139	1	0.58
CMRC0615	516780.8	6710220.7	330.5	240	-61.67/287.6	144	146	2	14.06
CMRC0615	516780.8	6710220.7	330.5	240	-61.67/287.6	152	153	1	1.20
CMRC0615	516780.8	6710220.7	330.5	240	-61.67/287.6	158	163	5	0.80
CMRC0615	516780.8	6710220.7	330.5	240	-61.67/287.6	169	176	7	1.48
CMRC0615	516780.8	6710220.7	330.5	240	-61.67/287.6	183	193	10	2.78
CMRC0615	516780.8	6710220.7	330.5	240	-61.67/287.6	196	197	1	0.96
CMRC0615	516780.8	6710220.7	330.5	240	-61.67/287.6	225	227	2	2.58
CMRC0616	516801.2	6710215.5	330.3	246	-59.97/285.1	81	84	3	0.74
CMRC0616	516801.2	6710215.5	330.3	246	-59.97/285.1	111	114	3	0.53
CMRC0616	516801.2	6710215.5	330.3	246	-59.97/285.1	143	144	1	0.83
CMRC0616	516801.2	6710215.5	330.3	246	-59.97/285.1	152	153	1	0.55
CMRC0616	516801.2	6710215.5	330.3	246	-59.97/285.1	157	158	1	0.68
CMRC0616	516801.2	6710215.5	330.3	246	-59.97/285.1	170	174	4	5.87
CMRC0616	516801.2	6710215.5	330.3	246	-59.97/285.1	179	182	3	1.32
CMRC0616	516801.2	6710215.5	330.3	246	-59.97/285.1	190	191	1	0.51
CMRC0616	516801.2	6710215.5	330.3	246	-59.97/285.1	196	214	18	1.52
CMRC0616	516801.2	6710215.5	330.3	246	-59.97/285.1	225	226	1	0.68
CMRC0616	516801.2	6710215.5	330.3	246	-59.97/285.1	229	230	1	0.86
CMRC0617	516688.2	6710092.0	329.9	144	-59.67/303.4	0	1	1	0.55
CMRC0617	516688.2	6710092.0	329.9	144	-59.67/303.4	35	36	1	3.22
CMRC0617	516688.2	6710092.0	329.9	144	-59.67/303.4	42	43	1	0.69
CMRC0617	516688.2	6710092.0	329.9	144	-59.67/303.4	51	55	4	1.46
CMRC0617	516688.2	6710092.0	329.9	144	-59.67/303.4	68	69	1	0.75
CMRC0617	516688.2	6710092.0	329.9	144	-59.67/303.4	88	89	1	2.39
CMRC0617	516688.2	6710092.0	329.9	144	-59.67/303.4	97	100	3	0.56
CMRC0617	516688.2	6710092.0	329.9	144	-59.67/303.4	109	110	1	2.55

Hole No	Easting	Northing	RL	Hole Depth	Dip/Azi	From	To	Width	Grade (g/t Au)
CMRC0617	516688.2	6710092.0	329.9	144	-59.67/303.4	116	120	4	0.67
CMRC0618	516715.9	6710097.5	332.6	198	-48.35/303.8	1	7	6	0.84
CMRC0618	516715.9	6710097.5	332.6	198	-48.35/303.8	51	52	1	0.52
CMRC0618	516715.9	6710097.5	332.6	198	-48.35/303.8	71	72	1	1.76
CMRC0618	516715.9	6710097.5	332.6	198	-48.35/303.8	79	80	1	1.89
CMRC0618	516715.9	6710097.5	332.6	198	-48.35/303.8	101	102	1	0.71
CMRC0618	516715.9	6710097.5	332.6	198	-48.35/303.8	108	109	1	2.84
CMRC0618	516715.9	6710097.5	332.6	198	-48.35/303.8	117	126	9	1.06
CMRC0618	516715.9	6710097.5	332.6	198	-48.35/303.8	129	130	1	0.65
CMRC0618	516715.9	6710097.5	332.6	198	-48.35/303.8	133	135	2	0.59
CMRC0618	516715.9	6710097.5	332.6	198	-48.35/303.8	144	145	1	0.51
CMRC0618	516715.9	6710097.5	332.6	198	-48.35/303.8	153	158	5	0.82
CMRC0618	516715.9	6710097.5	332.6	198	-48.35/303.8	165	173	8	0.95
CMRC0618	516715.9	6710097.5	332.6	198	-48.35/303.8	184	185	1	0.63
CMRC0618	516715.9	6710097.5	332.6	198	-48.35/303.8	197	198	1	6.42
CMRC0619	516534.9	6710177.4	335.0	222	-50.73/119.4	43	49	6	1.19
CMRC0619	516534.9	6710177.4	335.0	222	-50.73/119.4	53	54	1	1.05
CMRC0619	516534.9	6710177.4	335.0	222	-50.73/119.4	60	61	1	0.51
CMRC0619	516534.9	6710177.4	335.0	222	-50.73/119.4	74	75	1	1.41
CMRC0619	516534.9	6710177.4	335.0	222	-50.73/119.4	92	95	3	0.65
CMRC0619	516534.9	6710177.4	335.0	222	-50.73/119.4	102	105	3	1.17
CMRC0619	516534.9	6710177.4	335.0	222	-50.73/119.4	108	109	1	1.11
CMRC0619	516534.9	6710177.4	335.0	222	-50.73/119.4	117	118	1	0.82
CMRC0619	516534.9	6710177.4	335.0	222	-50.73/119.4	122	123	1	0.65
CMRC0619	516534.9	6710177.4	335.0	222	-50.73/119.4	139	140	1	0.75
CMRC0619	516534.9	6710177.4	335.0	222	-50.73/119.4	150	153	3	0.57
CMRC0619	516534.9	6710177.4	335.0	222	-50.73/119.4	166	169	3	0.90
CMRC0619	516534.9	6710177.4	335.0	222	-50.73/119.4	187	190	3	1.11
CMRC0619	516534.9	6710177.4	335.0	222	-50.73/119.4	194	197	3	0.55
CMRC0619	516534.9	6710177.4	335.0	222	-50.73/119.4	200	201	1	1.47
CMRC0620	516457.9	6710024.6	336.9	186	-59.21/299	2	7	5	1.28
CMRC0620	516457.9	6710024.6	336.9	186	-59.21/299	13	14	1	1.38
CMRC0620	516457.9	6710024.6	336.9	186	-59.21/299	25	26	1	1.78
CMRC0620	516457.9	6710024.6	336.9	186	-59.21/299	50	51	1	0.77
CMRC0620	516457.9	6710024.6	336.9	186	-59.21/299	55	58	3	0.90
CMRC0620	516457.9	6710024.6	336.9	186	-59.21/299	76	82	6	1.16
CMRC0620	516457.9	6710024.6	336.9	186	-59.21/299	88	97	9	1.13
CMRC0620	516457.9	6710024.6	336.9	186	-59.21/299	100	101	1	8.62
CMRC0620	516457.9	6710024.6	336.9	186	-59.21/299	106	107	1	0.68
CMRC0620	516457.9	6710024.6	336.9	186	-59.21/299	150	152	2	1.84
CMRC0620	516457.9	6710024.6	336.9	186	-59.21/299	174	175	1	0.61
CMRC0621	516390.4	6709815.5	337.7	252	-51.43/302.7	71	72	1	0.52
CMRC0621	516390.4	6709815.5	337.7	252	-51.43/302.7	115	116	1	1.43
CMRC0621	516390.4	6709815.5	337.7	252	-51.43/302.7	153	174	21	1.96
CMRC0621	516390.4	6709815.5	337.7	252	-51.43/302.7	177	214	37	2.33
CMRC0621	516390.4	6709815.5	337.7	252	-51.43/302.7	221	222	1	0.90
CMRC0622	516254.1	6709603.1	341.1	216	-61.18/269.9	34	35	1	0.64
CMRC0622	516254.1	6709603.1	341.1	216	-61.18/269.9	42	44	2	0.65
CMRC0622	516254.1	6709603.1	341.1	216	-61.18/269.9	92	93	1	0.54
CMRC0622	516254.1	6709603.1	341.1	216	-61.18/269.9	101	104	3	0.85
CMRC0622	516254.1	6709603.1	341.1	216	-61.18/269.9	109	119	10	3.32
CMRC0622	516254.1	6709603.1	341.1	216	-61.18/269.9	132	133	1	1.80
CMRC0622	516254.1	6709603.1	341.1	216	-61.18/269.9	151	153	2	1.14
CMRC0622	516254.1	6709603.1	341.1	216	-61.18/269.9	157	161	4	0.73

Hole No	Easting	Northing	RL	Hole Depth	Dip/Azi	From	To	Width	Grade (g/t Au)
CMRC0622	516254.1	6709603.1	341.1	216	-61.18/269.9	164	171	7	0.88
CMRC0623	516260.9	6709576.2	341.7	222	-68.17/266.8	38	39	1	0.61
CMRC0623	516260.9	6709576.2	341.7	222	-68.17/266.8	45	46	1	3.13
CMRC0623	516260.9	6709576.2	341.7	222	-68.17/266.8	66	69	3	0.52
CMRC0623	516260.9	6709576.2	341.7	222	-68.17/266.8	153	154	1	0.66
CMRC0623	516260.9	6709576.2	341.7	222	-68.17/266.8	217	222	5	1.42
CMRC0624	516258.9	6709406.1	344.2	270	-59.76/271.6	116	117	1	0.63
CMRC0624	516258.9	6709406.1	344.2	270	-59.76/271.6	164	166	2	2.32
CMRC0624	516258.9	6709406.1	344.2	270	-59.76/271.6	180	186	6	11.81
CMRC0624	516258.9	6709406.1	344.2	270	-59.76/271.6	200	201	1	0.62
CMRC0624	516258.9	6709406.1	344.2	270	-59.76/271.6	211	212	1	0.70
CMRC0624	516258.9	6709406.1	344.2	270	-59.76/271.6	220	223	3	0.38
CMRC0624	516258.9	6709406.1	344.2	270	-59.76/271.6	227	254	27	1.71
CMRC0625	516290.0	6709405.5	348.5	324	-58.76/273.7	37	42	5	5.77
CMRC0625	516290.0	6709405.5	348.5	324	-58.76/273.7	81	83	2	1.01
CMRC0625	516290.0	6709405.5	348.5	324	-58.76/273.7	110	111	1	1.21
CMRC0625	516290.0	6709405.5	348.5	324	-58.76/273.7	131	134	3	0.79
CMRC0625	516290.0	6709405.5	348.5	324	-58.76/273.7	158	159	1	0.50
CMRC0625	516290.0	6709405.5	348.5	324	-58.76/273.7	206	207	1	1.39
CMRC0625	516290.0	6709405.5	348.5	324	-58.76/273.7	223	235	12	5.84
CMRC0625	516290.0	6709405.5	348.5	324	-58.76/273.7	264	265	1	0.79
CMRC0625	516290.0	6709405.5	348.5	324	-58.76/273.7	269	282	13	1.54
CMRC0625	516290.0	6709405.5	348.5	324	-58.76/273.7	287	293	6	0.99
CMRC0626	516320.5	6709373.8	345.9	348	-60.81/271.8	7	8	1	1.26
CMRC0626	516320.5	6709373.8	345.9	348	-60.81/271.8	39	40	1	0.54
CMRC0626	516320.5	6709373.8	345.9	348	-60.81/271.8	48	50	2	0.97
CMRC0626	516320.5	6709373.8	345.9	348	-60.81/271.8	53	58	5	1.66
CMRC0626	516320.5	6709373.8	345.9	348	-60.81/271.8	67	69	2	2.42
CMRC0626	516320.5	6709373.8	345.9	348	-60.81/271.8	88	89	1	0.67
CMRC0626	516320.5	6709373.8	345.9	348	-60.81/271.8	95	96	1	0.78
CMRC0626	516320.5	6709373.8	345.9	348	-60.81/271.8	106	107	1	0.58
CMRC0626	516320.5	6709373.8	345.9	348	-60.81/271.8	145	146	1	0.63
CMRC0626	516320.5	6709373.8	345.9	348	-60.81/271.8	149	150	1	6.54
CMRC0626	516320.5	6709373.8	345.9	348	-60.81/271.8	171	172	1	1.10
CMRC0626	516320.5	6709373.8	345.9	348	-60.81/271.8	203	204	1	0.57
CMRC0626	516320.5	6709373.8	345.9	348	-60.81/271.8	237	238	1	1.12
CMRC0626	516320.5	6709373.8	345.9	348	-60.81/271.8	244	265	21	4.33
CMRC0626	516320.5	6709373.8	345.9	348	-60.81/271.8	275	277	2	2.14
CMRC0626	516320.5	6709373.8	345.9	348	-60.81/271.8	294	300	6	1.58
CMRC0626	516320.5	6709373.8	345.9	348	-60.81/271.8	311	315	4	1.96
CMRC0627	516307.0	6709349.0	343.0	312	-58.62/270.1	2	3	1	1.30
CMRC0627	516307.0	6709349.0	343.0	312	-58.62/270.1	26	30	4	0.74
CMRC0627	516307.0	6709349.0	343.0	312	-58.62/270.1	33	51	18	4.48
CMRC0627	516307.0	6709349.0	343.0	312	-58.62/270.1	54	68	14	1.45
CMRC0627	516307.0	6709349.0	343.0	312	-58.62/270.1	95	96	1	0.91
CMRC0627	516307.0	6709349.0	343.0	312	-58.62/270.1	141	142	1	0.57
CMRC0627	516307.0	6709349.0	343.0	312	-58.62/270.1	159	161	2	2.45
CMRC0627	516307.0	6709349.0	343.0	312	-58.62/270.1	172	173	1	0.52
CMRC0627	516307.0	6709349.0	343.0	312	-58.62/270.1	192	197	5	1.30
CMRC0627	516307.0	6709349.0	343.0	312	-58.62/270.1	209	210	1	1.19
CMRC0627	516307.0	6709349.0	343.0	312	-58.62/270.1	227	228	1	1.00
CMRC0627	516307.0	6709349.0	343.0	312	-58.62/270.1	238	258	20	5.11
CMRC0627	516307.0	6709349.0	343.0	312	-58.62/270.1	278	283	5	0.99
CMRC0627	516307.0	6709349.0	343.0	312	-58.62/270.1	286	293	7	1.96

Hole No	Easting	Northing	RL	Hole Depth	Dip/Azi	From	To	Width	Grade (g/t Au)
CMRC0628	516301.7	6709326.1	339.5	318	-60.11/270.5	20	42	22	1.66
CMRC0628	516301.7	6709326.1	339.5	318	-60.11/270.5	46	51	5	1.80
CMRC0628	516301.7	6709326.1	339.5	318	-60.11/270.5	88	89	1	0.55
CMRC0628	516301.7	6709326.1	339.5	318	-60.11/270.5	93	96	3	1.57
CMRC0628	516301.7	6709326.1	339.5	318	-60.11/270.5	113	114	1	0.58
CMRC0628	516301.7	6709326.1	339.5	318	-60.11/270.5	156	157	1	1.12
CMRC0628	516301.7	6709326.1	339.5	318	-60.11/270.5	161	162	1	7.81
CMRC0628	516301.7	6709326.1	339.5	318	-60.11/270.5	165	169	4	4.97
CMRC0628	516301.7	6709326.1	339.5	318	-60.11/270.5	233	255	22	1.42
CMRC0628	516301.7	6709326.1	339.5	318	-60.11/270.5	264	269	5	0.72
CMRC0628	516301.7	6709326.1	339.5	318	-60.11/270.5	273	276	3	1.20
CMRC0628	516301.7	6709326.1	339.5	318	-60.11/270.5	279	285	6	1.34
CMRC0628	516301.7	6709326.1	339.5	318	-60.11/270.5	290	294	4	0.82
CMRC0629	516376.0	6709701.0	341.0	225	-64.05/306.2	24	25	1	0.96
CMRC0629	516376.0	6709701.0	341.0	225	-64.05/306.2	75	76	1	1.71
CMRC0629	516376.0	6709701.0	341.0	225	-64.05/306.2	80	81	1	1.34
CMRC0629	516376.0	6709701.0	341.0	225	-64.05/306.2	110	113	3	0.87
CMRC0629	516376.0	6709701.0	341.0	225	-64.05/306.2	146	147	1	0.86
CMRC0629	516376.0	6709701.0	341.0	225	-64.05/306.2	181	182	1	2.43
CMRC0629	516376.0	6709701.0	341.0	225	-64.05/306.2	195	196	1	2.09
CMRC0629	516376.0	6709701.0	341.0	225	-64.05/306.2	199	203	4	2.15
CMRC0629	516376.0	6709701.0	341.0	225	-64.05/306.2	213	215	2	0.76
CMRC0630	516179.8	6708856.0	339.6	234	-50.97/269.8	29	36	7	1.27
CMRC0630	516179.8	6708856.0	339.6	234	-50.97/269.8	55	56	1	1.43
CMRC0630	516179.8	6708856.0	339.6	234	-50.97/269.8	87	88	1	0.56
CMRC0630	516179.8	6708856.0	339.6	234	-50.97/269.8	95	96	1	1.34
CMRC0630	516179.8	6708856.0	339.6	234	-50.97/269.8	120	123	3	1.64
CMRC0630	516179.8	6708856.0	339.6	234	-50.97/269.8	131	133	2	2.11
CMRC0630	516179.8	6708856.0	339.6	234	-50.97/269.8	162	168	6	1.35
CMRC0630	516179.8	6708856.0	339.6	234	-50.97/269.8	173	177	4	0.99
CMRC0630	516179.8	6708856.0	339.6	234	-50.97/269.8	185	191	6	0.51
CMRC0630	516179.8	6708856.0	339.6	234	-50.97/269.8	203	204	1	0.72
CMRC0630	516179.8	6708856.0	339.6	234	-50.97/269.8	212	213	1	0.56
CMRC0630	516179.8	6708856.0	339.6	234	-50.97/269.8	216	222	6	1.63
CMRC0630	516179.8	6708856.0	339.6	234	-50.97/269.8	226	228	2	10.60
CMRC0631	516243.5	6709125.6	340.1	132	-55.38/271.9	30	33	3	0.68
CMRC0631	516243.5	6709125.6	340.1	132	-55.38/271.9	36	37	1	11.65
CMRC0631	516243.5	6709125.6	340.1	132	-55.38/271.9	79	83	4	0.82
CMRC0631	516243.5	6709125.6	340.1	132	-55.38/271.9	96	101	5	2.19
CMRC0631	516243.5	6709125.6	340.1	132	-55.38/271.9	122	124	2	0.60
CMRC0632	510242.0	6709129.0	341.0	129	-61.84/267.1	20	23	3	0.55
CMRC0632	510242.0	6709129.0	341.0	129	-61.84/267.1	27	30	3	1.26
CMRC0632	510242.0	6709129.0	341.0	129	-61.84/267.1	75	78	3	0.71
CMRC0632	510242.0	6709129.0	341.0	129	-61.84/267.1	83	84	1	0.99
CMRC0632	510242.0	6709129.0	341.0	129	-61.84/267.1	95	96	1	4.88
CMRC0632	510242.0	6709129.0	341.0	129	-61.84/267.1	100	102	2	0.91
CMRC0632	510242.0	6709129.0	341.0	129	-61.84/267.1	121	122	1	1.08
CMRC0632	510242.0	6709129.0	341.0	129	-61.84/267.1	125	127	2	2.80
CMRC0633	516169.0	6708706.0	341.0	257	-60.86/270	3	5	2	0.88
CMRC0633	516169.0	6708706.0	341.0	257	-60.86/270	28	29	1	1.18
CMRC0633	516169.0	6708706.0	341.0	257	-60.86/270	43	44	1	0.75
CMRC0633	516169.0	6708706.0	341.0	257	-60.86/270	48	51	3	1.05
CMRC0633	516169.0	6708706.0	341.0	257	-60.86/270	65	66	1	0.57
CMRC0633	516169.0	6708706.0	341.0	257	-60.86/270	95	96	1	0.51

Hole No	Easting	Northing	RL	Hole Depth	Dip/Azi	From	To	Width	Grade (g/t Au)
CMRC0633	516169.0	6708706.0	341.0	257	-60.86/270	123	124	1	0.55
CMRC0633	516169.0	6708706.0	341.0	257	-60.86/270	137	138	1	0.86
CMRC0633	516169.0	6708706.0	341.0	257	-60.86/270	159	161	2	1.39
CMRC0633	516169.0	6708706.0	341.0	257	-60.86/270	175	176	1	3.26
CMRC0633	516169.0	6708706.0	341.0	257	-60.86/270	187	198	11	2.63
CMRC0633	516169.0	6708706.0	341.0	257	-60.86/270	201	209	8	2.22
CMRC0633	516169.0	6708706.0	341.0	257	-60.86/270	226	227	1	1.44
CMRC0633	516169.0	6708706.0	341.0	257	-60.86/270	234	237	3	2.17
CMRC0633	516169.0	6708706.0	341.0	257	-60.86/270	245	246	1	1.23
CMRC0633	516169.0	6708706.0	341.0	257	-60.86/270	251	252	1	1.12
CMRC0634	516168.0	6708631.0	341.0	211	-62.82/269.8	23	24	1	0.57
CMRC0634	516168.0	6708631.0	341.0	211	-62.82/269.8	36	38	2	0.72
CMRC0634	516168.0	6708631.0	341.0	211	-62.82/269.8	45	46	1	1.02
CMRC0634	516168.0	6708631.0	341.0	211	-62.82/269.8	59	61	2	1.93
CMRC0634	516168.0	6708631.0	341.0	211	-62.82/269.8	95	96	1	1.13
CMRC0634	516168.0	6708631.0	341.0	211	-62.82/269.8	207	211	4	0.34
CMRC0635	516156.0	6708533.0	341.0	264	-59.01/271.6	28	29	1	1.12
CMRC0635	516156.0	6708533.0	341.0	264	-59.01/271.6	33	34	1	0.70
CMRC0635	516156.0	6708533.0	341.0	264	-59.01/271.6	47	53	6	2.68
CMRC0635	516156.0	6708533.0	341.0	264	-59.01/271.6	56	57	1	0.79
CMRC0635	516156.0	6708533.0	341.0	264	-59.01/271.6	61	62	1	0.60
CMRC0635	516156.0	6708533.0	341.0	264	-59.01/271.6	67	69	2	1.38
CMRC0635	516156.0	6708533.0	341.0	264	-59.01/271.6	74	78	4	0.48
CMRC0635	516156.0	6708533.0	341.0	264	-59.01/271.6	87	88	1	0.95
CMRC0635	516156.0	6708533.0	341.0	264	-59.01/271.6	93	97	4	0.49
CMRC0635	516156.0	6708533.0	341.0	264	-59.01/271.6	138	140	2	0.91
CMRC0635	516156.0	6708533.0	341.0	264	-59.01/271.6	150	152	2	3.17
CMRC0635	516156.0	6708533.0	341.0	264	-59.01/271.6	173	177	4	0.41
CMRC0635	516156.0	6708533.0	341.0	264	-59.01/271.6	183	190	7	1.82
CMRC0635	516156.0	6708533.0	341.0	264	-59.01/271.6	194	201	7	0.97
CMRC0635	516156.0	6708533.0	341.0	264	-59.01/271.6	205	207	2	2.31
CMRC0635	516156.0	6708533.0	341.0	264	-59.01/271.6	222	225	3	0.71
CMRC0635	516156.0	6708533.0	341.0	264	-59.01/271.6	231	234	3	1.15
CMRC0635	516156.0	6708533.0	341.0	264	-59.01/271.6	239	240	1	7.50
CMRC0635	516156.0	6708533.0	341.0	264	-59.01/271.6	251	254	3	1.29
CMRC0636	516152.0	6708484.0	341.0	300	-60.17/269.7	1	4	3	1.73
CMRC0636	516152.0	6708484.0	341.0	300	-60.17/269.7	48	50	2	0.86
CMRC0636	516152.0	6708484.0	341.0	300	-60.17/269.7	82	83	1	0.57
CMRC0636	516152.0	6708484.0	341.0	300	-60.17/269.7	128	129	1	2.52
CMRC0636	516152.0	6708484.0	341.0	300	-60.17/269.7	172	176	4	1.75
CMRC0636	516152.0	6708484.0	341.0	300	-60.17/269.7	181	191	10	1.96
CMRC0636	516152.0	6708484.0	341.0	300	-60.17/269.7	194	200	6	0.70
CMRC0636	516152.0	6708484.0	341.0	300	-60.17/269.7	203	204	1	0.96
CMRC0636	516152.0	6708484.0	341.0	300	-60.17/269.7	210	216	6	3.85
CMRC0636	516152.0	6708484.0	341.0	300	-60.17/269.7	219	220	1	1.17
CMRC0636	516152.0	6708484.0	341.0	300	-60.17/269.7	228	230	2	0.75
CMRC0636	516152.0	6708484.0	341.0	300	-60.17/269.7	235	238	3	2.91
CMRC0636	516152.0	6708484.0	341.0	300	-60.17/269.7	241	244	3	3.36
CMRC0636	516152.0	6708484.0	341.0	300	-60.17/269.7	258	261	3	0.60
CMRC0636	516152.0	6708484.0	341.0	300	-60.17/269.7	283	284	1	0.77
CMRC0637	516148.0	6708378.0	341.0	228	-41.57/269.7	72	74	2	0.78
CMRC0637	516148.0	6708378.0	341.0	228	-41.57/269.7	108	110	2	2.11
CMRC0637	516148.0	6708378.0	341.0	228	-41.57/269.7	117	118	1	0.65
CMRC0637	516148.0	6708378.0	341.0	228	-41.57/269.7	122	124	2	0.63

Hole No	Easting	Northing	RL	Hole Depth	Dip/Azi	From	To	Width	Grade (g/t Au)
CMRC0637	516148.0	6708378.0	341.0	228	-41.57/269.7	128	133	5	3.15
CMRC0637	516148.0	6708378.0	341.0	228	-41.57/269.7	138	139	1	3.05
CMRC0637	516148.0	6708378.0	341.0	228	-41.57/269.7	166	167	1	3.16
CMRC0637	516148.0	6708378.0	341.0	228	-41.57/269.7	170	171	1	0.61
CMRC0637	516148.0	6708378.0	341.0	228	-41.57/269.7	177	180	3	0.77
CMRC0637	516148.0	6708378.0	341.0	228	-41.57/269.7	210	212	2	0.65
CMRC0638	516143.0	6708356.0	349.0	198	-48.22/267.1	1	2	1	0.51
CMRC0638	516143.0	6708356.0	349.0	198	-48.22/267.1	6	7	1	0.84
CMRC0638	516143.0	6708356.0	349.0	198	-48.22/267.1	37	38	1	0.95
CMRC0638	516143.0	6708356.0	349.0	198	-48.22/267.1	73	74	1	0.92
CMRC0638	516143.0	6708356.0	349.0	198	-48.22/267.1	80	81	1	0.53
CMRC0638	516143.0	6708356.0	349.0	198	-48.22/267.1	118	119	1	2.61
CMRC0638	516143.0	6708356.0	349.0	198	-48.22/267.1	132	133	1	0.52
CMRC0638	516143.0	6708356.0	349.0	198	-48.22/267.1	146	147	1	1.88
CMRC0638	516143.0	6708356.0	349.0	198	-48.22/267.1	156	157	1	0.58
CMRC0638	516143.0	6708356.0	349.0	198	-48.22/267.1	165	166	1	0.64
CMRC0638	516143.0	6708356.0	349.0	198	-48.22/267.1	172	174	2	0.87
CMRC0638	516143.0	6708356.0	349.0	198	-48.22/267.1	182	183	1	1.89
CMRC0638	516143.0	6708356.0	349.0	198	-48.22/267.1	197	198	1	0.57
CMRC0639	516269.0	6708428.0	347.0	180	-60.85/269.2	4	10	6	1.24
CMRC0639	516269.0	6708428.0	347.0	180	-60.85/269.2	35	36	1	0.96
CMRC0639	516269.0	6708428.0	347.0	180	-60.85/269.2	41	50	9	0.72
CMRC0639	516269.0	6708428.0	347.0	180	-60.85/269.2	60	61	1	2.79
CMRC0639	516269.0	6708428.0	347.0	180	-60.85/269.2	69	71	2	1.00
CMRC0639	516269.0	6708428.0	347.0	180	-60.85/269.2	78	79	1	3.32
CMRC0639	516269.0	6708428.0	347.0	180	-60.85/269.2	84	90	6	9.53
CMRC0639	516269.0	6708428.0	347.0	180	-60.85/269.2	106	107	1	0.58
CMRC0639	516269.0	6708428.0	347.0	180	-60.85/269.2	142	143	1	0.60
CMRC0639	516269.0	6708428.0	347.0	180	-60.85/269.2	160	161	1	0.75
CMRC0639	516269.0	6708428.0	347.0	180	-60.85/269.2	172	174	2	1.13
CMRC0640	516249.0	6708402.0	348.0	156	-61.1/272.7	0	1	1	1.24
CMRC0640	516249.0	6708402.0	348.0	156	-61.1/272.7	6	7	1	0.76
CMRC0640	516249.0	6708402.0	348.0	156	-61.1/272.7	57	64	7	1.88
CMRC0640	516249.0	6708402.0	348.0	156	-61.1/272.7	71	73	2	0.66
CMRC0640	516249.0	6708402.0	348.0	156	-61.1/272.7	78	81	3	2.04
CMRC0640	516249.0	6708402.0	348.0	156	-61.1/272.7	85	86	1	0.87
CMRC0640	516249.0	6708402.0	348.0	156	-61.1/272.7	94	95	1	1.26
CMRC0640	516249.0	6708402.0	348.0	156	-61.1/272.7	103	104	1	0.70
CMRC0640	516249.0	6708402.0	348.0	156	-61.1/272.7	116	117	1	1.05
CMRC0640	516249.0	6708402.0	348.0	156	-61.1/272.7	124	126	2	1.03
CMRC0640	516249.0	6708402.0	348.0	156	-61.1/272.7	132	135	3	0.75
CMRC0640	516249.0	6708402.0	348.0	156	-61.1/272.7	146	147	1	0.56
CMRC0641	516359.0	6708130.0	349.0	228	-62.71/270.6	12	13	1	0.65
CMRC0641	516359.0	6708130.0	349.0	228	-62.71/270.6	27	31	4	0.68
CMRC0641	516359.0	6708130.0	349.0	228	-62.71/270.6	36	37	1	3.62
CMRC0641	516359.0	6708130.0	349.0	228	-62.71/270.6	40	44	4	0.71
CMRC0641	516359.0	6708130.0	349.0	228	-62.71/270.6	67	68	1	0.96
CMRC0641	516359.0	6708130.0	349.0	228	-62.71/270.6	73	74	1	2.12
CMRC0641	516359.0	6708130.0	349.0	228	-62.71/270.6	95	99	4	1.57
CMRC0641	516359.0	6708130.0	349.0	228	-62.71/270.6	102	103	1	0.78
CMRC0641	516359.0	6708130.0	349.0	228	-62.71/270.6	116	117	1	3.21
CMRC0641	516359.0	6708130.0	349.0	228	-62.71/270.6	122	123	1	1.95
CMRC0641	516359.0	6708130.0	349.0	228	-62.71/270.6	131	135	4	3.05
CMRC0641	516359.0	6708130.0	349.0	228	-62.71/270.6	158	163	5	3.51

Hole No	Easting	Northing	RL	Hole Depth	Dip/Azi	From	To	Width	Grade (g/t Au)
CMRC0641	516359.0	6708130.0	349.0	228	-62.71/270.6	167	168	1	0.56
CMRC0641	516359.0	6708130.0	349.0	228	-62.71/270.6	188	189	1	0.54
CMRC0641	516359.0	6708130.0	349.0	228	-62.71/270.6	201	204	3	0.72
CMRC0641	516359.0	6708130.0	349.0	228	-62.71/270.6	212	215	3	1.66
CMRC0641	516359.0	6708130.0	349.0	228	-62.71/270.6	218	220	2	0.56
CMRC0642	516394.0	6708101.0	349.0	202	-57.2/268.6	5	6	1	0.65
CMRC0642	516394.0	6708101.0	349.0	202	-57.2/268.6	71	72	1	1.07
CMRC0642	516394.0	6708101.0	349.0	202	-57.2/268.6	75	77	2	0.68
CMRC0642	516394.0	6708101.0	349.0	202	-57.2/268.6	107	113	6	0.61
CMRC0642	516394.0	6708101.0	349.0	202	-57.2/268.6	120	121	1	0.61
CMRC0642	516394.0	6708101.0	349.0	202	-57.2/268.6	134	140	6	1.55
CMRC0642	516394.0	6708101.0	349.0	202	-57.2/268.6	145	146	1	0.55
CMRC0642	516394.0	6708101.0	349.0	202	-57.2/268.6	163	164	1	0.57
CMRC0642	516394.0	6708101.0	349.0	202	-57.2/268.6	171	175	4	1.02
CMRC0642	516394.0	6708101.0	349.0	202	-57.2/268.6	186	187	1	0.51
CMRC0642	516394.0	6708101.0	349.0	202	-57.2/268.6	192	193	1	0.57
CMRC0642	516394.0	6708101.0	349.0	202	-57.2/268.6	197	198	1	0.61
CMRC0643	516366.0	6708078.0	349.0	198	-61.92/270.2	33	34	1	0.65
CMRC0643	516366.0	6708078.0	349.0	198	-61.92/270.2	42	49	7	0.92
CMRC0643	516366.0	6708078.0	349.0	198	-61.92/270.2	56	60	4	5.43
CMRC0643	516366.0	6708078.0	349.0	198	-61.92/270.2	76	77	1	1.36
CMRC0643	516366.0	6708078.0	349.0	198	-61.92/270.2	86	87	1	0.55
CMRC0643	516366.0	6708078.0	349.0	198	-61.92/270.2	107	108	1	1.03
CMRC0643	516366.0	6708078.0	349.0	198	-61.92/270.2	114	120	6	2.48
CMRC0643	516366.0	6708078.0	349.0	198	-61.92/270.2	125	133	8	0.52
CMRC0643	516366.0	6708078.0	349.0	198	-61.92/270.2	150	157	7	2.78
CMRC0643	516366.0	6708078.0	349.0	198	-61.92/270.2	166	167	1	0.62
CMRC0643	516366.0	6708078.0	349.0	198	-61.92/270.2	180	181	1	1.07
CMRC0643	516366.0	6708078.0	349.0	198	-61.92/270.2	184	190	6	3.04
CMRC0643	516366.0	6708078.0	349.0	198	-61.92/270.2	195	196	1	0.56
CMRC0644	516374.0	6708054.0	349.0	236	-60.42/271.4	1	2	1	0.56
CMRC0644	516374.0	6708054.0	349.0	236	-60.42/271.4	34	38	4	0.94
CMRC0644	516374.0	6708054.0	349.0	236	-60.42/271.4	50	51	1	1.59
CMRC0644	516374.0	6708054.0	349.0	236	-60.42/271.4	54	59	5	0.72
CMRC0644	516374.0	6708054.0	349.0	236	-60.42/271.4	74	77	3	0.51
CMRC0644	516374.0	6708054.0	349.0	236	-60.42/271.4	119	127	8	1.02
CMRC0644	516374.0	6708054.0	349.0	236	-60.42/271.4	130	133	3	0.90
CMRC0644	516374.0	6708054.0	349.0	236	-60.42/271.4	148	155	7	1.72
CMRC0644	516374.0	6708054.0	349.0	236	-60.42/271.4	158	159	1	0.70
CMRC0644	516374.0	6708054.0	349.0	236	-60.42/271.4	176	177	1	0.60
CMRC0644	516374.0	6708054.0	349.0	236	-60.42/271.4	198	200	2	2.41
CMRC0644	516374.0	6708054.0	349.0	236	-60.42/271.4	203	204	1	0.79
CMRC0644	516374.0	6708054.0	349.0	236	-60.42/271.4	210	212	2	0.65
CMRC0644	516374.0	6708054.0	349.0	236	-60.42/271.4	220	221	1	0.76
CMRC0644	516374.0	6708054.0	349.0	236	-60.42/271.4	227	228	1	0.54
CMRC0644	516374.0	6708054.0	349.0	236	-60.42/271.4	232	235	3	0.48
CMRC0645	516354.0	6708028.0	350.0	192	-64.93/275.2	36	38	2	3.84
CMRC0645	516354.0	6708028.0	350.0	192	-64.93/275.2	43	44	1	1.54
CMRC0645	516354.0	6708028.0	350.0	192	-64.93/275.2	47	48	1	2.63
CMRC0645	516354.0	6708028.0	350.0	192	-64.93/275.2	63	64	1	0.59
CMRC0645	516354.0	6708028.0	350.0	192	-64.93/275.2	68	70	2	1.26
CMRC0645	516354.0	6708028.0	350.0	192	-64.93/275.2	100	108	8	2.90
CMRC0645	516354.0	6708028.0	350.0	192	-64.93/275.2	113	114	1	0.78
CMRC0645	516354.0	6708028.0	350.0	192	-64.93/275.2	122	127	5	1.16

Hole No	Easting	Northing	RL	Hole Depth	Dip/Azi	From	To	Width	Grade (g/t Au)
CMRC0645	516354.0	6708028.0	350.0	192	-64.93/275.2	130	131	1	0.59
CMRC0645	516354.0	6708028.0	350.0	192	-64.93/275.2	142	144	2	1.66
CMRC0645	516354.0	6708028.0	350.0	192	-64.93/275.2	169	175	6	0.78
CMRC0645	516354.0	6708028.0	350.0	192	-64.93/275.2	182	186	4	0.77
CMRC0645	516354.0	6708028.0	350.0	192	-64.93/275.2	191	192	1	3.61
CMRC0646	516240.0	6708004.0	350.0	84	-59.88/269.8	40	41	1	0.77
CMRC0646	516240.0	6708004.0	350.0	84	-59.88/269.8	51	55	4	0.60
CMRC0647	516249.0	6707980.0	351.0	78	-59.47/267.3	60	62	2	1.81
CMRC0648	516363.0	6707902.0	350.0	180	-59.31/272.4	3	4	1	0.76
CMRC0648	516363.0	6707902.0	350.0	180	-59.31/272.4	39	40	1	0.89
CMRC0648	516363.0	6707902.0	350.0	180	-59.31/272.4	78	80	2	1.16
CMRC0648	516363.0	6707902.0	350.0	180	-59.31/272.4	90	91	1	0.52
CMRC0648	516363.0	6707902.0	350.0	180	-59.31/272.4	95	96	1	1.35
CMRC0648	516363.0	6707902.0	350.0	180	-59.31/272.4	99	100	1	1.46
CMRC0648	516363.0	6707902.0	350.0	180	-59.31/272.4	114	116	2	1.25
CMRC0648	516363.0	6707902.0	350.0	180	-59.31/272.4	129	131	2	3.51
CMRC0648	516363.0	6707902.0	350.0	180	-59.31/272.4	136	138	2	2.18
CMRC0648	516363.0	6707902.0	350.0	180	-59.31/272.4	163	164	1	0.53
CMRC0649	516321.0	6707878.0	351.0	132	-58.97/269.7	2	11	9	0.68
CMRC0649	516321.0	6707878.0	351.0	132	-58.97/269.7	24	27	3	1.31
CMRC0649	516321.0	6707878.0	351.0	132	-58.97/269.7	31	36	5	1.67
CMRC0649	516321.0	6707878.0	351.0	132	-58.97/269.7	40	51	11	0.87
CMRC0649	516321.0	6707878.0	351.0	132	-58.97/269.7	56	57	1	0.66
CMRC0649	516321.0	6707878.0	351.0	132	-58.97/269.7	64	69	5	1.91
CMRC0649	516321.0	6707878.0	351.0	132	-58.97/269.7	72	77	5	1.45
CMRC0649	516321.0	6707878.0	351.0	132	-58.97/269.7	81	88	7	1.20
CMRC0649	516321.0	6707878.0	351.0	132	-58.97/269.7	93	99	6	1.60
CMRC0650	516350.0	6707877.0	351.0	168	-61.66/270.8	0	1	1	0.69
CMRC0650	516350.0	6707877.0	351.0	168	-61.66/270.8	45	46	1	0.72
CMRC0650	516350.0	6707877.0	351.0	168	-61.66/270.8	63	71	8	0.99
CMRC0650	516350.0	6707877.0	351.0	168	-61.66/270.8	82	83	1	0.80
CMRC0650	516350.0	6707877.0	351.0	168	-61.66/270.8	90	91	1	1.85
CMRC0650	516350.0	6707877.0	351.0	168	-61.66/270.8	94	98	4	1.34
CMRC0650	516350.0	6707877.0	351.0	168	-61.66/270.8	101	107	6	1.21
CMRC0650	516350.0	6707877.0	351.0	168	-61.66/270.8	111	120	9	2.84
CMRC0650	516350.0	6707877.0	351.0	168	-61.66/270.8	130	131	1	0.88
CMRC0650	516350.0	6707877.0	351.0	168	-61.66/270.8	134	135	1	0.53
CMRC0651	516358.0	6707848.0	351.0	180	-57.42/272.4	2	3	1	0.50
CMRC0651	516358.0	6707848.0	351.0	180	-57.42/272.4	70	71	1	3.21
CMRC0651	516358.0	6707848.0	351.0	180	-57.42/272.4	75	80	5	2.88
CMRC0651	516358.0	6707848.0	351.0	180	-57.42/272.4	84	85	1	0.59
CMRC0651	516358.0	6707848.0	351.0	180	-57.42/272.4	94	95	1	1.35
CMRC0651	516358.0	6707848.0	351.0	180	-57.42/272.4	101	104	3	0.84
CMRC0651	516358.0	6707848.0	351.0	180	-57.42/272.4	118	119	1	0.57
CMRC0651	516358.0	6707848.0	351.0	180	-57.42/272.4	179	180	1	1.83
CMRC0653	516349.0	6707828.0	351.0	168	-63.08/276.6	49	50	1	0.53
CMRC0656	516333.0	6707678.0	354.0	156	-60.55/268.7	2	3	1	0.58
CMRC0656	516333.0	6707678.0	354.0	156	-60.55/268.7	60	67	7	1.02
CMRC0656	516333.0	6707678.0	354.0	156	-60.55/268.7	75	82	7	0.50
CMRC0656	516333.0	6707678.0	354.0	156	-60.55/268.7	126	127	1	0.64
CMRC0656	516333.0	6707678.0	354.0	156	-60.55/268.7	131	132	1	0.51
CMRC0657	516349.0	6707654.0	354.0	168	-59.06/265.5	70	71	1	1.78
CMRC0657	516349.0	6707654.0	354.0	168	-59.06/265.5	102	103	1	3.07
CMRC0657	516349.0	6707654.0	354.0	168	-59.06/265.5	109	110	1	0.65

Hole No	Easting	Northing	RL	Hole Depth	Dip/Azi	From	To	Width	Grade (g/t Au)
CMRC0657	516349.0	6707654.0	354.0	168	-59.06/265.5	114	115	1	2.12
CMRC0657	516349.0	6707654.0	354.0	168	-59.06/265.5	119	120	1	1.29
CMRC0657	516349.0	6707654.0	354.0	168	-59.06/265.5	135	141	6	1.06
CMRC0657	516349.0	6707654.0	354.0	168	-59.06/265.5	144	149	5	5.04
CMRC0658	516361.0	6707527.0	359.0	222	-56.59/268.4	3	4	1	0.57
CMRC0658	516361.0	6707527.0	359.0	222	-56.59/268.4	8	9	1	0.92
CMRC0658	516361.0	6707527.0	359.0	222	-56.59/268.4	50	51	1	0.78
CMRC0658	516361.0	6707527.0	359.0	222	-56.59/268.4	54	55	1	1.33
CMRC0658	516361.0	6707527.0	359.0	222	-56.59/268.4	61	62	1	0.96
CMRC0658	516361.0	6707527.0	359.0	222	-56.59/268.4	85	86	1	2.16
CMRC0658	516361.0	6707527.0	359.0	222	-56.59/268.4	106	107	1	0.55
CMRC0658	516361.0	6707527.0	359.0	222	-56.59/268.4	141	142	1	2.47
CMRC0658	516361.0	6707527.0	359.0	222	-56.59/268.4	151	152	1	1.50
CMRC0658	516361.0	6707527.0	359.0	222	-56.59/268.4	157	158	1	1.08
CMRC0658	516361.0	6707527.0	359.0	222	-56.59/268.4	161	162	1	0.80
CMRC0658	516361.0	6707527.0	359.0	222	-56.59/268.4	190	192	2	0.92
CMRC0659	516364.0	6707502.0	359.0	192	-59.73/271.4	43	49	6	0.74
CMRC0659	516364.0	6707502.0	359.0	192	-59.73/271.4	59	60	1	1.21
CMRC0659	516364.0	6707502.0	359.0	192	-59.73/271.4	70	71	1	0.73
CMRC0659	516364.0	6707502.0	359.0	192	-59.73/271.4	84	85	1	1.37
CMRC0659	516364.0	6707502.0	359.0	192	-59.73/271.4	115	117	2	1.38
CMRC0659	516364.0	6707502.0	359.0	192	-59.73/271.4	127	128	1	0.71
CMRC0659	516364.0	6707502.0	359.0	192	-59.73/271.4	133	134	1	1.10
CMRC0659	516364.0	6707502.0	359.0	192	-59.73/271.4	139	143	4	0.81
CMRC0659	516364.0	6707502.0	359.0	192	-59.73/271.4	146	147	1	0.52
CMRC0659	516364.0	6707502.0	359.0	192	-59.73/271.4	160	166	6	0.71
CMRC0659	516364.0	6707502.0	359.0	192	-59.73/271.4	185	187	2	2.37
CMRC0660	516364.0	6707477.0	359.0	216	-60.27/271.7	47	53	6	0.59
CMRC0660	516364.0	6707477.0	359.0	216	-60.27/271.7	56	62	6	0.67
CMRC0660	516364.0	6707477.0	359.0	216	-60.27/271.7	66	67	1	0.93
CMRC0660	516364.0	6707477.0	359.0	216	-60.27/271.7	88	90	2	11.95
CMRC0660	516364.0	6707477.0	359.0	216	-60.27/271.7	107	110	3	1.15
CMRC0660	516364.0	6707477.0	359.0	216	-60.27/271.7	129	130	1	1.82
CMRC0660	516364.0	6707477.0	359.0	216	-60.27/271.7	136	137	1	1.41
CMRC0660	516364.0	6707477.0	359.0	216	-60.27/271.7	157	158	1	1.56
CMRC0660	516364.0	6707477.0	359.0	216	-60.27/271.7	189	198	9	0.43
CMRC0661	516366.0	6707450.0	359.0	234	-59.04/273.5	64	65	1	0.55
CMRC0661	516366.0	6707450.0	359.0	234	-59.04/273.5	100	101	1	5.66
CMRC0661	516366.0	6707450.0	359.0	234	-59.04/273.5	104	105	1	0.57
CMRC0661	516366.0	6707450.0	359.0	234	-59.04/273.5	136	137	1	0.70
CMRC0661	516366.0	6707450.0	359.0	234	-59.04/273.5	140	142	2	4.50
CMRC0661	516366.0	6707450.0	359.0	234	-59.04/273.5	147	149	2	2.00
CMRC0661	516366.0	6707450.0	359.0	234	-59.04/273.5	156	157	1	1.69
CMRC0661	516366.0	6707450.0	359.0	234	-59.04/273.5	180	181	1	0.53
CMRC0661	516366.0	6707450.0	359.0	234	-59.04/273.5	204	206	2	1.85
CMRC0661	516366.0	6707450.0	359.0	234	-59.04/273.5	224	227	3	0.81
CMRC0662	516407.0	6707429.0	359.0	240	-53.32/275.2	3	5	2	2.54
CMRC0662	516407.0	6707429.0	359.0	240	-53.32/275.2	85	90	5	2.16
CMRC0662	516407.0	6707429.0	359.0	240	-53.32/275.2	117	118	1	0.56
CMRC0662	516407.0	6707429.0	359.0	240	-53.32/275.2	138	140	2	1.11
CMRC0662	516407.0	6707429.0	359.0	240	-53.32/275.2	173	174	1	0.52
CMRC0662	516407.0	6707429.0	359.0	240	-53.32/275.2	214	215	1	0.58
CMRC0662	516407.0	6707429.0	359.0	240	-53.32/275.2	219	220	1	0.80
CMRC0663	516386.0	6707378.0	359.0	204	-56.33/273.2	3	6	3	0.92

Hole No	Easting	Northing	RL	Hole Depth	Dip/Azi	From	To	Width	Grade (g/t Au)
CMRC0663	516386.0	6707378.0	359.0	204	-56.33/273.2	75	80	5	2.39
CMRC0663	516386.0	6707378.0	359.0	204	-56.33/273.2	85	86	1	0.59
CMRC0663	516386.0	6707378.0	359.0	204	-56.33/273.2	100	106	6	1.25
CMRC0663	516386.0	6707378.0	359.0	204	-56.33/273.2	114	115	1	1.61
CMRC0663	516386.0	6707378.0	359.0	204	-56.33/273.2	121	124	3	1.40
CMRC0663	516386.0	6707378.0	359.0	204	-56.33/273.2	145	149	4	0.50
CMRC0663	516386.0	6707378.0	359.0	204	-56.33/273.2	153	157	4	0.72
CMRC0663	516386.0	6707378.0	359.0	204	-56.33/273.2	173	174	1	2.32
CMRC0663	516386.0	6707378.0	359.0	204	-56.33/273.2	183	184	1	0.55
CMRC0664	516366.0	6707395.0	359.0	204	-58.69/271	7	8	1	2.16
CMRC0664	516366.0	6707395.0	359.0	204	-58.69/271	18	19	1	0.57
CMRC0664	516366.0	6707395.0	359.0	204	-58.69/271	61	65	4	1.97
CMRC0664	516366.0	6707395.0	359.0	204	-58.69/271	78	80	2	1.66
CMRC0664	516366.0	6707395.0	359.0	204	-58.69/271	116	118	2	0.90
CMRC0664	516366.0	6707395.0	359.0	204	-58.69/271	143	144	1	0.94
CMRC0664	516366.0	6707395.0	359.0	204	-58.69/271	184	186	2	2.24
CMRC0664	516366.0	6707395.0	359.0	204	-58.69/271	189	192	3	0.80
CMRC0664	516366.0	6707395.0	359.0	204	-58.69/271	196	197	1	1.01
CMRC0665	516265.1	6709304.7	339.0	276	-57.69/270.3	79	80	1	1.66
CMRC0665	516265.1	6709304.7	339.0	276	-57.69/270.3	115	118	3	1.99
CMRC0665	516265.1	6709304.7	339.0	276	-57.69/270.3	122	123	1	1.18
CMRC0665	516265.1	6709304.7	339.0	276	-57.69/270.3	148	150	2	2.27
CMRC0665	516265.1	6709304.7	339.0	276	-57.69/270.3	155	156	1	0.64
CMRC0665	516265.1	6709304.7	339.0	276	-57.69/270.3	159	160	1	2.20
CMRC0665	516265.1	6709304.7	339.0	276	-57.69/270.3	169	170	1	0.90
CMRC0665	516265.1	6709304.7	339.0	276	-57.69/270.3	206	216	10	3.95
CMRC0665	516265.1	6709304.7	339.0	276	-57.69/270.3	221	227	6	0.89
CMRC0665	516265.1	6709304.7	339.0	276	-57.69/270.3	230	238	8	0.74
CMRC0665	516265.1	6709304.7	339.0	276	-57.69/270.3	242	244	2	0.93
CMRC0665	516265.1	6709304.7	339.0	276	-57.69/270.3	247	248	1	0.51
CMRC0665	516265.1	6709304.7	339.0	276	-57.69/270.3	255	272	17	3.08
CMRC0665	516265.1	6709304.7	339.0	276	-57.69/270.3	275	276	1	0.88
CMRC0666	516296.2	6709304.7	339.0	372	-56.45/271.9	21	22	1	1.89
CMRC0666	516296.2	6709304.7	339.0	372	-56.45/271.9	25	37	12	1.82
CMRC0666	516296.2	6709304.7	339.0	372	-56.45/271.9	41	42	1	1.73
CMRC0666	516296.2	6709304.7	339.0	372	-56.45/271.9	45	47	2	1.86
CMRC0666	516296.2	6709304.7	339.0	372	-56.45/271.9	57	61	4	0.44
CMRC0666	516296.2	6709304.7	339.0	372	-56.45/271.9	82	84	2	0.80
CMRC0666	516296.2	6709304.7	339.0	372	-56.45/271.9	150	152	2	2.18
CMRC0666	516296.2	6709304.7	339.0	372	-56.45/271.9	182	183	1	3.96
CMRC0666	516296.2	6709304.7	339.0	372	-56.45/271.9	191	192	1	1.31
CMRC0666	516296.2	6709304.7	339.0	372	-56.45/271.9	198	199	1	0.54
CMRC0666	516296.2	6709304.7	339.0	372	-56.45/271.9	235	253	18	1.96
CMRC0666	516296.2	6709304.7	339.0	372	-56.45/271.9	261	269	8	1.01
CMRC0666	516296.2	6709304.7	339.0	372	-56.45/271.9	274	275	1	1.30
CMRC0666	516296.2	6709304.7	339.0	372	-56.45/271.9	279	290	11	1.13
CMRC0666	516296.2	6709304.7	339.0	372	-56.45/271.9	293	295	2	0.66
CMRC0666	516296.2	6709304.7	339.0	372	-56.45/271.9	342	346	4	1.54
CMRC0667	516324.0	6709327.0	339.0	378	-58.75/267.7	21	30	9	1.20
CMRC0667	516324.0	6709327.0	339.0	378	-58.75/267.7	61	84	23	1.17
CMRC0667	516324.0	6709327.0	339.0	378	-58.75/267.7	119	120	1	2.83
CMRC0667	516324.0	6709327.0	339.0	378	-58.75/267.7	145	146	1	2.02
CMRC0667	516324.0	6709327.0	339.0	378	-58.75/267.7	162	163	1	7.69
CMRC0667	516324.0	6709327.0	339.0	378	-58.75/267.7	167	170	3	0.63

Hole No	Easting	Northing	RL	Hole Depth	Dip/Azi	From	To	Width	Grade (g/t Au)
CMRC0667	516324.0	6709327.0	339.0	378	-58.75/267.7	179	180	1	2.74
CMRC0667	516324.0	6709327.0	339.0	378	-58.75/267.7	188	189	1	0.66
CMRC0667	516324.0	6709327.0	339.0	378	-58.75/267.7	196	197	1	1.07
CMRC0667	516324.0	6709327.0	339.0	378	-58.75/267.7	217	219	2	0.76
CMRC0667	516324.0	6709327.0	339.0	378	-58.75/267.7	238	240	2	0.56
CMRC0667	516324.0	6709327.0	339.0	378	-58.75/267.7	260	276	16	1.93
CMRC0667	516324.0	6709327.0	339.0	378	-58.75/267.7	293	296	3	1.58
CMRC0667	516324.0	6709327.0	339.0	378	-58.75/267.7	301	305	4	2.03
CMRC0667	516324.0	6709327.0	339.0	378	-58.75/267.7	312	314	2	1.99
CMRC0667	516324.0	6709327.0	339.0	378	-58.75/267.7	318	319	1	0.76
CMRC0668	516192.0	6708832.0	339.0	264	-51.08/271.7	58	59	1	1.18
CMRC0668	516192.0	6708832.0	339.0	264	-51.08/271.7	66	67	1	1.03
CMRC0668	516192.0	6708832.0	339.0	264	-51.08/271.7	76	77	1	0.65
CMRC0668	516192.0	6708832.0	339.0	264	-51.08/271.7	90	92	2	1.86
CMRC0668	516192.0	6708832.0	339.0	264	-51.08/271.7	96	97	1	1.03
CMRC0668	516192.0	6708832.0	339.0	264	-51.08/271.7	147	148	1	0.62
CMRC0668	516192.0	6708832.0	339.0	264	-51.08/271.7	158	160	2	0.69
CMRC0668	516192.0	6708832.0	339.0	264	-51.08/271.7	165	166	1	1.29
CMRC0668	516192.0	6708832.0	339.0	264	-51.08/271.7	174	175	1	0.97
CMRC0668	516192.0	6708832.0	339.0	264	-51.08/271.7	179	180	1	2.87
CMRC0668	516192.0	6708832.0	339.0	264	-51.08/271.7	184	190	6	2.07
CMRC0668	516192.0	6708832.0	339.0	264	-51.08/271.7	193	198	5	0.89
CMRC0668	516192.0	6708832.0	339.0	264	-51.08/271.7	224	225	1	0.67
CMRC0668	516192.0	6708832.0	339.0	264	-51.08/271.7	228	232	4	0.71
CMRC0668	516192.0	6708832.0	339.0	264	-51.08/271.7	240	241	1	1.23
CMRC0669	516203.0	6708781.0	339.0	276	-49.37/272.8	22	23	1	0.70
CMRC0669	516203.0	6708781.0	339.0	276	-49.37/272.8	69	70	1	2.01
CMRC0669	516203.0	6708781.0	339.0	276	-49.37/272.8	75	76	1	1.58
CMRC0669	516203.0	6708781.0	339.0	276	-49.37/272.8	87	88	1	0.61
CMRC0669	516203.0	6708781.0	339.0	276	-49.37/272.8	135	136	1	1.44
CMRC0669	516203.0	6708781.0	339.0	276	-49.37/272.8	162	163	1	0.52
CMRC0669	516203.0	6708781.0	339.0	276	-49.37/272.8	166	167	1	0.94
CMRC0669	516203.0	6708781.0	339.0	276	-49.37/272.8	172	173	1	2.77
CMRC0669	516203.0	6708781.0	339.0	276	-49.37/272.8	178	182	4	0.88
CMRC0669	516203.0	6708781.0	339.0	276	-49.37/272.8	201	202	1	0.53
CMRC0669	516203.0	6708781.0	339.0	276	-49.37/272.8	207	219	12	3.45
CMRC0669	516203.0	6708781.0	339.0	276	-49.37/272.8	222	223	1	0.50
CMRC0669	516203.0	6708781.0	339.0	276	-49.37/272.8	237	238	1	0.58
CMRC0669	516203.0	6708781.0	339.0	276	-49.37/272.8	245	249	4	0.82
CMRC0669	516203.0	6708781.0	339.0	276	-49.37/272.8	256	261	5	1.36
CMRC0669	516203.0	6708781.0	339.0	276	-49.37/272.8	265	270	5	1.13
CMRC0670	516171.0	6708732.0	343.0	228	-58.3/276.4	2	3	1	0.83
CMRC0670	516171.0	6708732.0	343.0	228	-58.3/276.4	16	17	1	1.18
CMRC0670	516171.0	6708732.0	343.0	228	-58.3/276.4	43	44	1	1.18
CMRC0670	516171.0	6708732.0	343.0	228	-58.3/276.4	69	70	1	0.82
CMRC0670	516171.0	6708732.0	343.0	228	-58.3/276.4	78	79	1	0.71
CMRC0670	516171.0	6708732.0	343.0	228	-58.3/276.4	105	106	1	0.64
CMRC0670	516171.0	6708732.0	343.0	228	-58.3/276.4	110	112	2	0.85
CMRC0670	516171.0	6708732.0	343.0	228	-58.3/276.4	117	118	1	0.66
CMRC0670	516171.0	6708732.0	343.0	228	-58.3/276.4	169	170	1	0.99
CMRC0670	516171.0	6708732.0	343.0	228	-58.3/276.4	186	187	1	2.88
CMRC0670	516171.0	6708732.0	343.0	228	-58.3/276.4	191	217	26	4.11
CMRC0671	516167.0	6708681.0	344.0	198	-55.43/272.5	1	7	6	0.90
CMRC0671	516167.0	6708681.0	344.0	198	-55.43/272.5	18	21	3	1.21

Hole No	Easting	Northing	RL	Hole Depth	Dip/Azi	From	To	Width	Grade (g/t Au)
CMRC0671	516167.0	6708681.0	344.0	198	-55.43/272.5	24	39	15	2.05
CMRC0671	516167.0	6708681.0	344.0	198	-55.43/272.5	48	49	1	0.98
CMRC0671	516167.0	6708681.0	344.0	198	-55.43/272.5	55	60	5	0.86
CMRC0671	516167.0	6708681.0	344.0	198	-55.43/272.5	66	67	1	1.09
CMRC0671	516167.0	6708681.0	344.0	198	-55.43/272.5	82	84	2	2.75
CMRC0671	516167.0	6708681.0	344.0	198	-55.43/272.5	90	91	1	1.02
CMRC0671	516167.0	6708681.0	344.0	198	-55.43/272.5	102	103	1	0.62
CMRC0671	516167.0	6708681.0	344.0	198	-55.43/272.5	187	198	11	2.38
CMRC0672	516189.0	6708683.0	344.0	168	-57.19/269.4	0	4	4	0.43
CMRC0672	516189.0	6708683.0	344.0	168	-57.19/269.4	26	42	16	1.00
CMRC0672	516189.0	6708683.0	344.0	168	-57.19/269.4	47	55	8	1.55
CMRC0672	516189.0	6708683.0	344.0	168	-57.19/269.4	80	81	1	2.88
CMRC0672	516189.0	6708683.0	344.0	168	-57.19/269.4	100	101	1	0.80
CMRC0672	516189.0	6708683.0	344.0	168	-57.19/269.4	119	120	1	0.91
CMRC0672	516189.0	6708683.0	344.0	168	-57.19/269.4	126	127	1	2.08
CMRC0672	516189.0	6708683.0	344.0	168	-57.19/269.4	136	137	1	2.25
CMRC0673	516171.0	6708636.0	344.0	174	-60.34/267	23	24	1	0.62
CMRC0673	516171.0	6708636.0	344.0	174	-60.34/267	27	31	4	1.04
CMRC0673	516171.0	6708636.0	344.0	174	-60.34/267	39	50	11	3.68
CMRC0673	516171.0	6708636.0	344.0	174	-60.34/267	67	68	1	1.63
CMRC0673	516171.0	6708636.0	344.0	174	-60.34/267	87	88	1	0.86
CMRC0673	516171.0	6708636.0	344.0	174	-60.34/267	98	104	6	1.52
CMRC0674	516045.0	6707704.0	360.0	168	-61.01/270.9	0	2	2	0.64
CMRC0674	516045.0	6707704.0	360.0	168	-61.01/270.9	44	48	4	1.16
CMRC0674	516045.0	6707704.0	360.0	168	-61.01/270.9	53	54	1	0.51
CMRC0674	516045.0	6707704.0	360.0	168	-61.01/270.9	101	103	2	0.97
CMRC0674	516045.0	6707704.0	360.0	168	-61.01/270.9	107	110	3	1.39
CMRC0674	516045.0	6707704.0	360.0	168	-61.01/270.9	115	117	2	0.99
CMRC0674	516045.0	6707704.0	360.0	168	-61.01/270.9	127	137	10	0.77
CMRC0674	516045.0	6707704.0	360.0	168	-61.01/270.9	140	141	1	0.53
CMRC0674	516045.0	6707704.0	360.0	168	-61.01/270.9	144	148	4	0.78
CMRC0675	516043.0	6707732.0	360.0	180	-55.82/267.9	0	1	1	0.78
CMRC0675	516043.0	6707732.0	360.0	180	-55.82/267.9	46	50	4	1.00
CMRC0675	516043.0	6707732.0	360.0	180	-55.82/267.9	70	79	9	1.21
CMRC0675	516043.0	6707732.0	360.0	180	-55.82/267.9	82	90	8	7.94
CMRC0675	516043.0	6707732.0	360.0	180	-55.82/267.9	95	96	1	1.03
CMRC0675	516043.0	6707732.0	360.0	180	-55.82/267.9	99	100	1	0.57
CMRC0675	516043.0	6707732.0	360.0	180	-55.82/267.9	110	114	4	6.47
CMRC0675	516043.0	6707732.0	360.0	180	-55.82/267.9	117	121	4	5.15
CMRC0676	516045.0	6707754.0	360.0	162	-58.49/271.2	0	2	2	0.69
CMRC0676	516045.0	6707754.0	360.0	162	-58.49/271.2	20	21	1	1.10
CMRC0676	516045.0	6707754.0	360.0	162	-58.49/271.2	48	52	4	1.04
CMRC0676	516045.0	6707754.0	360.0	162	-58.49/271.2	77	78	1	0.74
CMRC0676	516045.0	6707754.0	360.0	162	-58.49/271.2	81	84	3	1.68
CMRC0676	516045.0	6707754.0	360.0	162	-58.49/271.2	89	90	1	1.11
CMRC0676	516045.0	6707754.0	360.0	162	-58.49/271.2	107	111	4	1.28
CMRC0676	516045.0	6707754.0	360.0	162	-58.49/271.2	114	115	1	0.76
CMRC0676	516045.0	6707754.0	360.0	162	-58.49/271.2	121	131	10	1.30
CMRC0677	516043.0	6707785.0	359.0	156	-58.69/269.4	0	2	2	0.88
CMRC0677	516043.0	6707785.0	359.0	156	-58.69/269.4	22	23	1	0.73
CMRC0677	516043.0	6707785.0	359.0	156	-58.69/269.4	45	48	3	0.39
CMRC0677	516043.0	6707785.0	359.0	156	-58.69/269.4	52	54	2	0.83
CMRC0677	516043.0	6707785.0	359.0	156	-58.69/269.4	80	83	3	3.62
CMRC0677	516043.0	6707785.0	359.0	156	-58.69/269.4	107	120	13	1.97

Hole No	Easting	Northing	RL	Hole Depth	Dip/Azi	From	To	Width	Grade (g/t Au)
CMRC0678	516047.0	6707813.0	359.0	162	-60.8/267.8	0	2	2	0.52
CMRC0678	516047.0	6707813.0	359.0	162	-60.8/267.8	48	51	3	0.66
CMRC0678	516047.0	6707813.0	359.0	162	-60.8/267.8	62	63	1	1.49
CMRC0678	516047.0	6707813.0	359.0	162	-60.8/267.8	77	78	1	1.28
CMRC0678	516047.0	6707813.0	359.0	162	-60.8/267.8	86	88	2	0.97
CMRC0678	516047.0	6707813.0	359.0	162	-60.8/267.8	97	98	1	0.61
CMRC0678	516047.0	6707813.0	359.0	162	-60.8/267.8	108	109	1	0.83
CMRC0678	516047.0	6707813.0	359.0	162	-60.8/267.8	114	122	8	0.68
CMRC0678	516047.0	6707813.0	359.0	162	-60.8/267.8	125	128	3	0.71
CMRC0678	516047.0	6707813.0	359.0	162	-60.8/267.8	136	137	1	0.71
CMRC0679	516065.0	6707836.0	358.0	150	-60.47/269.9	0	2	2	0.68
CMRC0679	516065.0	6707836.0	358.0	150	-60.47/269.9	30	31	1	0.70
CMRC0679	516065.0	6707836.0	358.0	150	-60.47/269.9	51	54	3	1.05
CMRC0679	516065.0	6707836.0	358.0	150	-60.47/269.9	65	66	1	0.66
CMRC0679	516065.0	6707836.0	358.0	150	-60.47/269.9	105	106	1	0.58
CMRC0679	516065.0	6707836.0	358.0	150	-60.47/269.9	111	115	4	1.05
CMRC0679	516065.0	6707836.0	358.0	150	-60.47/269.9	134	135	1	2.18
CMRC0679	516065.0	6707836.0	358.0	150	-60.47/269.9	141	144	3	2.37
CMRC0680	515966.0	6706485.0	346.8	66	-59.05/269.6	42	43	1	1.17
CMRC0680	515966.0	6706485.0	346.8	66	-59.05/269.6	46	47	1	0.72
CMRC0680	515966.0	6706485.0	346.8	66	-59.05/269.6	63	66	3	0.42
CMRC0681	515958.0	6706538.0	347.0	84	-61.21/272.2	40	63	23	1.79
CMRC0681	515958.0	6706538.0	347.0	84	-61.21/272.2	66	67	1	0.91
CMRC0682	515949.0	6706512.0	347.0	60	-59.39/273.2	4	5	1	0.99
CMRC0682	515949.0	6706512.0	347.0	60	-59.39/273.2	49	50	1	0.53
CMRC0683	515975.0	6706512.0	347.0	72	-61.03/272.7	48	49	1	1.14
CMRC0683	515975.0	6706512.0	347.0	72	-61.03/272.7	66	67	1	0.75
CMRC0684	516379.0	6707353.0	355.0	216	-55/268	74	76	2	2.45
CMRC0684	516379.0	6707353.0	355.0	216	-55/268	95	96	1	0.59
CMRC0684	516379.0	6707353.0	355.0	216	-55/268	115	123	8	0.85
CMRC0684	516379.0	6707353.0	355.0	216	-55/268	138	147	9	0.55
CMRC0684	516379.0	6707353.0	355.0	216	-55/268	156	158	2	0.95
CMRC0684	516379.0	6707353.0	355.0	216	-55/268	162	163	1	1.22
CMRC0684	516379.0	6707353.0	355.0	216	-55/268	182	183	1	0.77
CMRC0685	516383.0	6707528.0	359.0	222	-55.26/270.2	5	10	5	0.44
CMRC0685	516383.0	6707528.0	359.0	222	-55.26/270.2	75	78	3	0.91
CMRC0685	516383.0	6707528.0	359.0	222	-55.26/270.2	105	107	2	1.40
CMRC0685	516383.0	6707528.0	359.0	222	-55.26/270.2	123	127	4	0.50
CMRC0685	516383.0	6707528.0	359.0	222	-55.26/270.2	157	159	2	3.35
CMRC0685	516383.0	6707528.0	359.0	222	-55.26/270.2	167	168	1	10.50
CMRC0685	516383.0	6707528.0	359.0	222	-55.26/270.2	172	174	2	1.18
CMRC0685	516383.0	6707528.0	359.0	222	-55.26/270.2	177	181	4	0.44
CMRC0685	516383.0	6707528.0	359.0	222	-55.26/270.2	211	214	3	1.46
CMRC0686	516932.0	6710678.0	341.5	264	-60.1/288.1	49	52	3	0.89
CMRC0686	516932.0	6710678.0	341.5	264	-60.1/288.1	110	114	4	0.82
CMRC0686	516932.0	6710678.0	341.5	264	-60.1/288.1	118	119	1	1.21
CMRC0686	516932.0	6710678.0	341.5	264	-60.1/288.1	180	181	1	1.38
CMRC0686	516932.0	6710678.0	341.5	264	-60.1/288.1	187	189	2	1.65
CMRC0686	516932.0	6710678.0	341.5	264	-60.1/288.1	199	200	1	0.75
CMRC0686	516932.0	6710678.0	341.5	264	-60.1/288.1	205	206	1	1.26
CMRC0686	516932.0	6710678.0	341.5	264	-60.1/288.1	210	217	7	1.32
CMRC0686	516932.0	6710678.0	341.5	264	-60.1/288.1	236	241	5	0.75
CMRC0686	516932.0	6710678.0	341.5	264	-60.1/288.1	244	245	1	0.79
CMRC0686	516932.0	6710678.0	341.5	264	-60.1/288.1	255	256	1	0.53

Hole No	Easting	Northing	RL	Hole Depth	Dip/Azi	From	To	Width	Grade (g/t Au)
CMRC0687	516919.0	6710642.0	344.0	222	-66.89/286.1	43	45	2	1.74
CMRC0687	516919.0	6710642.0	344.0	222	-66.89/286.1	103	110	7	1.16
CMRC0687	516919.0	6710642.0	344.0	222	-66.89/286.1	117	119	2	0.80
CMRC0687	516919.0	6710642.0	344.0	222	-66.89/286.1	128	129	1	0.94
CMRC0687	516919.0	6710642.0	344.0	222	-66.89/286.1	162	163	1	0.97
CMRC0687	516919.0	6710642.0	344.0	222	-66.89/286.1	209	210	1	2.09
CMRC0688	516867.0	6710407.0	341.8	264	-59.82/284.9	9	10	1	1.66
CMRC0688	516867.0	6710407.0	341.8	264	-59.82/284.9	21	22	1	0.63
CMRC0688	516867.0	6710407.0	341.8	264	-59.82/284.9	151	152	1	0.60
CMRC0688	516867.0	6710407.0	341.8	264	-59.82/284.9	167	171	4	0.55
CMRC0688	516867.0	6710407.0	341.8	264	-59.82/284.9	174	186	12	0.95
CMRC0688	516867.0	6710407.0	341.8	264	-59.82/284.9	193	200	7	2.00
CMRC0688	516867.0	6710407.0	341.8	264	-59.82/284.9	203	210	7	0.99
CMRC0688	516867.0	6710407.0	341.8	264	-59.82/284.9	221	226	5	3.81
CMRC0688	516867.0	6710407.0	341.8	264	-59.82/284.9	236	237	1	0.67
CMRC0688	516867.0	6710407.0	341.8	264	-59.82/284.9	252	253	1	1.77
CMRC0689	516850.0	6710374.0	342.0	276	-61.85/288.3	16	19	3	0.65
CMRC0689	516850.0	6710374.0	342.0	276	-61.85/288.3	45	46	1	0.94
CMRC0689	516850.0	6710374.0	342.0	276	-61.85/288.3	89	95	6	4.59
CMRC0689	516850.0	6710374.0	342.0	276	-61.85/288.3	110	115	5	6.26
CMRC0689	516850.0	6710374.0	342.0	276	-61.85/288.3	129	130	1	1.07
CMRC0689	516850.0	6710374.0	342.0	276	-61.85/288.3	177	178	1	0.65
CMRC0689	516850.0	6710374.0	342.0	276	-61.85/288.3	181	185	4	0.75
CMRC0689	516850.0	6710374.0	342.0	276	-61.85/288.3	190	191	1	0.68
CMRC0689	516850.0	6710374.0	342.0	276	-61.85/288.3	194	206	12	1.01
CMRC0689	516850.0	6710374.0	342.0	276	-61.85/288.3	210	217	7	2.66
CMRC0689	516850.0	6710374.0	342.0	276	-61.85/288.3	228	229	1	1.00
CMRC0689	516850.0	6710374.0	342.0	276	-61.85/288.3	235	244	9	1.44
CMRC0690	516333.0	6706780.0	346.9	216	-56.94/274.3	48	52	4	1.01
CMRC0690	516333.0	6706780.0	346.9	216	-56.94/274.3	80	85	5	0.52
CMRC0690	516333.0	6706780.0	346.9	216	-56.94/274.3	94	96	2	0.95
CMRC0690	516333.0	6706780.0	346.9	216	-56.94/274.3	102	104	2	1.95
CMRC0690	516333.0	6706780.0	346.9	216	-56.94/274.3	136	137	1	1.28
CMRC0690	516333.0	6706780.0	346.9	216	-56.94/274.3	145	146	1	1.39
CMRC0691	516308.0	6706712.0	345.0	138	-60.08/270	39	50	11	1.15
CMRC0691	516308.0	6706712.0	345.0	138	-60.08/270	70	75	5	3.84
CMRC0691	516308.0	6706712.0	345.0	138	-60.08/270	109	111	2	1.70
CMRC0691	516308.0	6706712.0	345.0	138	-60.08/270	115	116	1	0.54
CMRC0692	516291.0	6706660.0	345.0	126	-59.46/275.4	49	51	2	1.03
CMRC0692	516291.0	6706660.0	345.0	126	-59.46/275.4	54	60	6	3.12
CMRC0692	516291.0	6706660.0	345.0	126	-59.46/275.4	66	67	1	0.54
CMRC0692	516291.0	6706660.0	345.0	126	-59.46/275.4	85	87	2	1.96
CMRC0692	516291.0	6706660.0	345.0	126	-59.46/275.4	103	106	3	0.63
CMRC0692	516291.0	6706660.0	345.0	126	-59.46/275.4	113	114	1	0.86
CMRC0692	516291.0	6706660.0	345.0	126	-59.46/275.4	120	121	1	0.97
CMRC0693	516308.0	6706657.0	345.0	150	-60.44/272.2	48	49	1	0.94
CMRC0693	516308.0	6706657.0	345.0	150	-60.44/272.2	54	57	3	1.58
CMRC0693	516308.0	6706657.0	345.0	150	-60.44/272.2	61	62	1	2.71
CMRC0693	516308.0	6706657.0	345.0	150	-60.44/272.2	77	86	9	3.70
CMRC0693	516308.0	6706657.0	345.0	150	-60.44/272.2	105	115	10	2.13
CMRC0694	515995.0	6706685.0	347.0	138	-59.79/278	2	3	1	0.63
CMRC0694	515995.0	6706685.0	347.0	138	-59.79/278	41	50	9	1.99
CMRC0694	515995.0	6706685.0	347.0	138	-59.79/278	82	83	1	0.84
CMRC0694	515995.0	6706685.0	347.0	138	-59.79/278	92	94	2	1.36

Hole No	Easting	Northing	RL	Hole Depth	Dip/Azi	From	To	Width	Grade (g/t Au)
CMRC0694	515995.0	6706685.0	347.0	138	-59.79/278	106	107	1	0.54
CMRC0694	515995.0	6706685.0	347.0	138	-59.79/278	111	112	1	0.56
CMRC0694	515995.0	6706685.0	347.0	138	-59.79/278	120	121	1	0.92
CMRC0695	516013.1	6706685.3	347.0	168	-62.53/270.4	38	44	6	1.62
CMRC0695	516013.1	6706685.3	347.0	168	-62.53/270.4	57	58	1	3.86
CMRC0695	516013.1	6706685.3	347.0	168	-62.53/270.4	71	72	1	1.05
CMRC0695	516013.1	6706685.3	347.0	168	-62.53/270.4	77	78	1	4.55
CMRC0695	516013.1	6706685.3	347.0	168	-62.53/270.4	110	111	1	0.71
CMRC0695	516013.1	6706685.3	347.0	168	-62.53/270.4	122	123	1	1.60
CMRC0695	516013.1	6706685.3	347.0	168	-62.53/270.4	138	139	1	0.91
CMRC0695	516013.1	6706685.3	347.0	168	-62.53/270.4	144	147	3	2.17
CMRC0696	515994.0	6706636.0	347.0	138	-61.08/274	49	51	2	2.70
CMRC0696	515994.0	6706636.0	347.0	138	-61.08/274	56	57	1	1.10
CMRC0696	515994.0	6706636.0	347.0	138	-61.08/274	73	80	7	0.93
CMRC0696	515994.0	6706636.0	347.0	138	-61.08/274	84	95	11	5.39
CMRC0697	516011.0	6706637.0	347.0	144	-60.65/272.2	39	44	5	5.62
CMRC0697	516011.0	6706637.0	347.0	144	-60.65/272.2	53	54	1	0.90
CMRC0697	516011.0	6706637.0	347.0	144	-60.65/272.2	78	79	1	1.27
CMRC0697	516011.0	6706637.0	347.0	144	-60.65/272.2	95	100	5	2.57
CMRC0697	516011.0	6706637.0	347.0	144	-60.65/272.2	115	120	5	1.26
CMRC0698	516003.0	6706586.0	347.0	132	-60.91/272	14	15	1	0.70
CMRC0698	516003.0	6706586.0	347.0	132	-60.91/272	24	28	4	0.56
CMRC0698	516003.0	6706586.0	347.0	132	-60.91/272	46	48	2	0.68
CMRC0698	516003.0	6706586.0	347.0	132	-60.91/272	75	82	7	6.96
CMRC0698	516003.0	6706586.0	347.0	132	-60.91/272	111	112	1	3.81
CMRC0698	516003.0	6706586.0	347.0	132	-60.91/272	118	120	2	5.51
CMRC0699	516020.0	6706587.0	346.0	156	-58.52/270.1	45	54	9	9.90
CMRC0699	516020.0	6706587.0	346.0	156	-58.52/270.1	86	87	1	1.01
CMRC0699	516020.0	6706587.0	346.0	156	-58.52/270.1	90	91	1	3.12
CMRC0699	516020.0	6706587.0	346.0	156	-58.52/270.1	94	96	2	0.88
CMRC0700	516278.0	6705434.0	343.0	156	-49.95/275.5	46	54	8	0.80
CMRC0700	516278.0	6705434.0	343.0	156	-49.95/275.5	61	65	4	0.65
CMRC0700	516278.0	6705434.0	343.0	156	-49.95/275.5	70	71	1	0.56
CMRC0700	516278.0	6705434.0	343.0	156	-49.95/275.5	101	108	7	9.48
CMRC0700	516278.0	6705434.0	343.0	156	-49.95/275.5	121	126	5	1.10
CMRC0701	516134.0	6705382.0	344.0	174	-49.09/93.7	47	48	1	0.98
CMRC0701	516134.0	6705382.0	344.0	174	-49.09/93.7	52	53	1	1.85
CMRC0701	516134.0	6705382.0	344.0	174	-49.09/93.7	83	88	5	2.51
CMRC0701	516134.0	6705382.0	344.0	174	-49.09/93.7	91	92	1	0.54
CMRC0701	516134.0	6705382.0	344.0	174	-49.09/93.7	124	126	2	1.10
CMRC0702	516248.5	6708428.5	347.0	342	-53.36/273.5	6	9	3	1.56
CMRC0702	516248.5	6708428.5	347.0	342	-53.36/273.5	40	42	2	14.22
CMRC0702	516248.5	6708428.5	347.0	342	-53.36/273.5	47	50	3	3.45
CMRC0702	516248.5	6708428.5	347.0	342	-53.36/273.5	62	66	4	6.85
CMRC0702	516248.5	6708428.5	347.0	342	-53.36/273.5	71	72	1	0.84
CMRC0702	516248.5	6708428.5	347.0	342	-53.36/273.5	79	81	2	0.84
CMRC0702	516248.5	6708428.5	347.0	342	-53.36/273.5	98	99	1	0.55
CMRC0702	516248.5	6708428.5	347.0	342	-53.36/273.5	127	128	1	1.60
CMRC0702	516248.5	6708428.5	347.0	342	-53.36/273.5	133	136	3	0.83
CMRC0702	516248.5	6708428.5	347.0	342	-53.36/273.5	149	150	1	6.51
CMRC0702	516248.5	6708428.5	347.0	342	-53.36/273.5	173	174	1	0.55
CMRC0702	516248.5	6708428.5	347.0	342	-53.36/273.5	280	286	6	0.90
CMRC0702	516248.5	6708428.5	347.0	342	-53.36/273.5	293	295	2	0.83
CMRC0702	516248.5	6708428.5	347.0	342	-53.36/273.5	298	299	1	0.85

Hole No	Easting	Northing	RL	Hole Depth	Dip/Azi	From	To	Width	Grade (g/t Au)
CMRC0702	516248.5	6708428.5	347.0	342	-53.36/273.5	304	335	31	1.24
CMRC0703	516168.0	6708478.0	344.0	312	-63.24/273.6	0	6	6	1.12
CMRC0703	516168.0	6708478.0	344.0	312	-63.24/273.6	40	42	2	9.41
CMRC0703	516168.0	6708478.0	344.0	312	-63.24/273.6	48	51	3	1.62
CMRC0703	516168.0	6708478.0	344.0	312	-63.24/273.6	54	55	1	2.58
CMRC0703	516168.0	6708478.0	344.0	312	-63.24/273.6	77	78	1	0.61
CMRC0703	516168.0	6708478.0	344.0	312	-63.24/273.6	86	87	1	2.56
CMRC0703	516168.0	6708478.0	344.0	312	-63.24/273.6	144	146	2	1.58
CMRC0703	516168.0	6708478.0	344.0	312	-63.24/273.6	175	176	1	5.49
CMRC0703	516168.0	6708478.0	344.0	312	-63.24/273.6	229	257	28	0.95
CMRC0703	516168.0	6708478.0	344.0	312	-63.24/273.6	262	266	4	2.94
CMRC0703	516168.0	6708478.0	344.0	312	-63.24/273.6	270	271	1	2.90
CMRC0703	516168.0	6708478.0	344.0	312	-63.24/273.6	275	278	3	0.83
CMRC0703	516168.0	6708478.0	344.0	312	-63.24/273.6	286	290	4	0.72
CMRC0703	516168.0	6708478.0	344.0	312	-63.24/273.6	310	312	2	1.91
CMRC0704	516367.0	6709357.0	344.0	216	-61.58/269.9	1	2	1	1.32
CMRC0704	516367.0	6709357.0	344.0	216	-61.58/269.9	7	8	1	15.85
CMRC0704	516367.0	6709357.0	344.0	216	-61.58/269.9	81	82	1	0.64
CMRC0704	516367.0	6709357.0	344.0	216	-61.58/269.9	133	134	1	0.54
CMRC0704	516367.0	6709357.0	344.0	216	-61.58/269.9	137	138	1	5.01
CMRC0704	516367.0	6709357.0	344.0	216	-61.58/269.9	141	145	4	0.94
CMRC0704	516367.0	6709357.0	344.0	216	-61.58/269.9	156	157	1	1.36
CMRC0704	516367.0	6709357.0	344.0	216	-61.58/269.9	170	171	1	1.18
CMRC0704	516367.0	6709357.0	344.0	216	-61.58/269.9	189	190	1	0.76
CMRC0704	516367.0	6709357.0	344.0	216	-61.58/269.9	201	202	1	8.86
CMRC0705	516558.0	6710221.0	334.0	42	-61.5/314.7	1	3	2	0.60
CMRC0705	516558.0	6710221.0	334.0	42	-61.5/314.7	21	22	1	0.52
CMRC0705	516558.0	6710221.0	334.0	42	-61.5/314.7	29	30	1	0.57
CMRC0706	516558.0	6710221.0	334.0	102	-62.13/298.6	3	4	1	0.65
CMRC0706	516558.0	6710221.0	334.0	102	-62.13/298.6	68	69	1	0.63
CMRC0706	516558.0	6710221.0	334.0	102	-62.13/298.6	75	84	9	0.92
CMRC0706	516558.0	6710221.0	334.0	102	-62.13/298.6	89	91	2	0.77
CMRC0706	516558.0	6710221.0	334.0	102	-62.13/298.6	94	96	2	0.98
CMRC0707	516282.0	6709602.0	341.0	192	-64.58/263.7	38	39	1	3.06
CMRC0707	516282.0	6709602.0	341.0	192	-64.58/263.7	143	144	1	0.57
CMRC0707	516282.0	6709602.0	341.0	192	-64.58/263.7	155	162	7	2.10
CMRC0707	516282.0	6709602.0	341.0	192	-64.58/263.7	167	168	1	0.64
CMRC0707	516282.0	6709602.0	341.0	192	-64.58/263.7	177	179	2	1.46
CMRC0707	516282.0	6709602.0	341.0	192	-64.58/263.7	183	189	6	1.27
CMRC0708	516261.0	6709578.0	342.0	126	-52.74/266.8	42	43	1	0.75
CMRC0709	516561.0	6710189.0	334.0	144	-58.81/305	89	90	1	0.55
CMRC0709	516561.0	6710189.0	334.0	144	-58.81/305	97	98	1	0.87
CMRC0709	516561.0	6710189.0	334.0	144	-58.81/305	107	109	2	1.00
CMRC0709	516561.0	6710189.0	334.0	144	-58.81/305	128	129	1	0.61
CMRC0709	516561.0	6710189.0	334.0	144	-58.81/305	135	136	1	0.98
CMRC0710	517162.0	6711767.0	323.0	126	-58.53/121.3	1	2	1	0.79
CMRC0710	517162.0	6711767.0	323.0	126	-58.53/121.3	10	12	2	0.79
CMRC0711	517122.0	6711674.0	323.0	168	-57.69/129.7	1	2	1	0.71
CMRC0711	517122.0	6711674.0	323.0	168	-57.69/129.7	15	16	1	1.26
CMRC0711	517122.0	6711674.0	323.0	168	-57.69/129.7	25	28	3	1.46
CMRC0711	517122.0	6711674.0	323.0	168	-57.69/129.7	48	49	1	0.96
CMRC0711	517122.0	6711674.0	323.0	168	-57.69/129.7	75	80	5	1.25
CMRC0711	517122.0	6711674.0	323.0	168	-57.69/129.7	92	93	1	1.64
CMRC0711	517122.0	6711674.0	323.0	168	-57.69/129.7	98	99	1	0.66

Hole No	Easting	Northing	RL	Hole Depth	Dip/Azi	From	To	Width	Grade (g/t Au)
CMRC0711	517122.0	6711674.0	323.0	168	-57.69/129.7	151	152	1	1.87
CMRC0711	517122.0	6711674.0	323.0	168	-57.69/129.7	155	158	3	1.86
CMRC0712	517071.0	6711582.0	322.0	156	-60.46/123	38	49	11	1.30
CMRC0712	517071.0	6711582.0	322.0	156	-60.46/123	93	94	1	1.17
CMRC0712	517071.0	6711582.0	322.0	156	-60.46/123	105	106	1	0.51
CMRC0712	517071.0	6711582.0	322.0	156	-60.46/123	110	112	2	0.66
CMRC0712	517071.0	6711582.0	322.0	156	-60.46/123	117	118	1	0.69
CMRC0712	517071.0	6711582.0	322.0	156	-60.46/123	125	132	7	2.00

Karlawinda

Hole No	Easting	Northing	RL	Hole Depth	Dip/Azi	From	To	Width	Grade (g/t Au)
KBRC1965	209069	7366936	585	150	-60/197	107	108	1	18.83
KBRC1966	209096	7367011	585	180	-60/199	114	115	1	0.58
KBRC1966	209096	7367011	585	180	-60/199	120	123	3	0.48
KBRC1967	209124	7367086	585	198	-60/197	87	92	5	2.35
KBRC1967	209124	7367086	585	198	-60/197	139	140	1	1.12
KBRC1968	209153	7367166	585	210	-60/199	67	69	2	4.19
KBRC1968	209153	7367166	585	210	-60/199	106	107	1	0.55
KBRC1969	209472	7366874	585	120	-60/199	114	119	5	3.77
KBRC1980	209493	7366931	585	234	-60/196	79	80	1	2.58
KBRC1980	209493	7366931	585	234	-60/196	89	90	1	0.83
KBRC1980	209493	7366931	585	234	-60/196	145	155	10	1.51
KBRC1980	209493	7366931	585	234	-60/196	170	171	1	1.57
KBRC1981	209547	7367081	585	252	-60/197	55	56	1	0.7
KBRC1982	206826	7367669	587.78	156	-59/59	119	122	3	0.78
KBRC1983	206793	7367650	587.69	180	-59/59	108	110	2	0.58
KBRC1984	207026	7367325	585.17	144	-60/58	34	38	4	0.43
KBRC1985	206957	7367285	585.2	210	-59/59	48	52	4	2.73
KBRC1985	206957	7367285	585.2	210	-59/59	90	91	1	0.5
KBRC1985	206957	7367285	585.2	210	-59/59	122	123	1	0.53
KBRC1986	206888	7367244	585.01	222	-61/58	57	59	2	3.71
KBRC1986	206888	7367244	585.01	222	-61/58	113	114	1	0.83
KBRC1986	206888	7367244	585.01	222	-61/58	146	148	2	0.53
KBRC1987	206819	7367203	584.93	264	-60/58	71	75	4	11.25
KBRC1987	206819	7367203	584.93	264	-60/58	141	143	2	0.72
KBRC1987	206819	7367203	584.93	264	-60/58	148	149	1	0.56
KBRC1987	206819	7367203	584.93	264	-60/58	163	164	1	0.56
KBRC1987	206819	7367203	584.93	264	-60/58	242	248	6	6.54
KBRC1988	206748	7367162	584.83	288	-60/61	180	181	1	3.56
KBRC1989	206862	7367133	584.67	234	-60/58	151	155	4	0.65
KBRC1990	206794	7367093	584.67	294	-60/61	177	178	1	0.88
KBRC1990	206794	7367093	584.67	294	-60/61	186	188	2	0.58
KBRC1990	206794	7367093	584.67	294	-60/61	263	264	1	17.28
KBRC1990	206794	7367093	584.67	294	-60/61	268	271	3	2.64
KBRC1991	207102	7367274	584.69	168	-60/61	110	111	1	0.69
KBRC1994	207000	7367214	584.62	180	-61/59	41	42	1	0.59
KBRC1994	207000	7367214	584.62	180	-61/59	47	53	6	4.11
KBRC1994	207000	7367214	584.62	180	-61/59	77	78	1	0.5
KBRC1996	206905	7367316	585.34	150	-60/60	59	64	5	1.59
KBRC1996	206905	7367316	585.34	150	-60/60	88	90	2	1.78
KBRC1996	206905	7367316	585.34	150	-60/60	130	131	1	0.52
KBRC1997	206864	7367287	585.29	186	-60/59	64	65	1	7.58
KBRC1997	206864	7367287	585.29	186	-60/59	86	95	9	1.33
KBRC1998	206819	7367266	585.16	222	-60/60	75	87	12	2.74
KBRC1999	206793	7367309	585.35	228	-60/59	80	83	3	4.02
KBRC1999	206793	7367309	585.35	228	-60/59	182	183	1	0.51

Hole No	Easting	Northing	RL	Hole Depth	Dip/Azi	From	To	Width	Grade (g/t Au)
KBRC2001	207035	7367391	585.82	120	-61/59	37	41	4	2.86
KBRC2002	206992	7367366	585.56	120	-60/59	50	51	1	5.97
KBRC2003	206949	7367341	585.45	126	-59/59	54	55	1	1.23
KBRC2003	206949	7367341	585.45	126	-59/59	113	114	1	0.56
KBRC2004	206880	7367361	585.44	162	-60/59	64	66	2	5.06
KBRC2004	206880	7367361	585.44	162	-60/59	87	88	1	0.5
KBRC2004	206880	7367361	585.44	162	-60/59	94	96	2	0.95
KBRC2005	206837	7367334	585.37	198	-60/59	69	72	3	1.8
KBRC2005	206837	7367334	585.37	198	-60/59	90	91	1	0.9
KBRC2005	206837	7367334	585.37	198	-60/59	95	96	1	0.52
KBRC2006	206706	7367258	585.29	282	-60/61	270	271	1	1.95
KBRC2006	206706	7367258	585.29	282	-60/61	275	276	1	0.67
KBRC2008	206776	7367241	585.07	246	-60/59	152	153	1	0.51
KBRC2010	206967	7367409	586.16	126	-60/58	35	36	1	1.05
KBRC2011	206923	7367384	585.77	144	-60/59	63	66	3	0.75
KBRC2011	206923	7367384	585.77	144	-60/59	120	121	1	1.22
KBRC2013	206869	7367420	586.31	198	-60/59	75	76	1	4.82
KBRC2013	206869	7367420	586.31	198	-60/59	99	100	1	0.64
KBRC2013	206869	7367420	586.31	198	-60/59	104	105	1	1.58
KBRC2013	206869	7367420	586.31	198	-60/59	116	119	3	7.78
KBRC2013	206869	7367420	586.31	198	-60/59	124	128	4	0.69
KBRC2015	207213	7367246	584.57	168	-60/58	47	48	1	1.47
KBRC2017	207025	7367291	585.09	90	-60/59	39	42	3	5.34
KBRC2018	206979	7367265	585.22	120	-60/58	78	80	2	0.64
KBRC2018	206979	7367265	585.22	120	-60/58	112	113	1	0.56
KBRC2019	206935	7367239	584.97	114	-60/59	59	63	4	0.94
KBRC2019	206935	7367239	584.97	114	-60/59	68	75	7	1.28
KBRC2019	206935	7367239	584.97	114	-60/59	94	95	1	0.5
KBRC2020	206893	7367214	585.04	120	-60/59	86	88	2	1.36
KBRC2021	206992	7367303	585.27	102	-59/59	47	48	1	26.76
KBRC2022	206923	7367263	585.26	120	-60/59	52	53	1	0.55
KBRC2022	206923	7367263	585.26	120	-60/59	81	83	2	3.42
KBRC2022	206923	7367263	585.26	120	-60/59	110	112	2	1.37
KBRC2023	206853	7367224	585.03	120	-60/59	68	69	1	1.38
KBRC2023	206853	7367224	585.03	120	-60/59	76	80	4	0.61
KBRC2025	206850	7367189	584.89	132	-60/59	65	74	9	1.8
KBRC2029	207034	7367362	585.52	78	-60/59	32	33	1	1.63
KBRC2030	206993	7367338	585.42	90	-60/59	45	48	3	7.37
KBRC2030	206993	7367338	585.42	90	-60/59	70	72	2	1.03
KBRC2031	206950	7367313	585.34	114	-60/59	50	56	6	3.47
KBRC2031	206950	7367313	585.34	114	-60/59	90	92	2	0.55
KBRC2032	206907	7367288	585.23	126	-60/58	57	64	7	1.34
KBRC2032	206907	7367288	585.23	126	-60/58	83	84	1	0.78
KBRC2032	206907	7367288	585.23	126	-60/58	92	95	3	1.7
KBRC2033	206863	7367263	584.87	132	-60/59	64	65	1	0.71
KBRC2033	206863	7367263	584.87	132	-60/59	89	90	1	0.72
KBRC2034	206820	7367238	585.01	138	-60/59	85	90	5	0.94
KBRC2034	206820	7367238	585.01	138	-60/59	94	101	7	0.81
KBRC2036	206954	7367322	585.43	162	-57/4	59	60	1	4.31
KBRC2036	206954	7367322	585.43	162	-57/4	88	95	7	0.57
KBRC2036	206954	7367322	585.43	162	-57/4	102	103	1	1.16
KBRC2036	206954	7367322	585.43	162	-57/4	109	110	1	0.84
KBRC2038	206970	7367228	584.77	102	-60/59	54	56	2	1.37
KBRC2038	206970	7367228	584.77	102	-60/59	76	79	3	0.93
KBRC2039	207040	7367207	584.51	102	-60/59	82	84	2	0.91
KBRC2040	206996	7367182	584.4	102	-60/58	50	53	3	2.2
KBRC2040	206996	7367182	584.4	102	-60/58	67	68	1	0.58

Hole No	Easting	Northing	RL	Hole Depth	Dip/Azi	From	To	Width	Grade (g/t Au)
KBRC2041	206964	7367194	584.64	108	-60/59	60	61	1	0.98
KBRC2044	206891	7367394	585.79	138	-60/59	98	104	6	0.59
KBRC2044	206891	7367394	585.79	138	-60/59	118	120	2	5.78
KBRC2044	206891	7367394	585.79	138	-60/59	129	130	1	0.92
KBRC2045	206847	7367369	585.73	150	-60/59	70	71	1	0.88
KBRC2045	206847	7367369	585.73	150	-60/59	90	97	7	0.56
KBRC2045	206847	7367369	585.73	150	-60/59	138	139	1	0.56
KBRC2046	206804	7367344	585.42	162	-60/59	74	80	6	0.59
KBRC2046	206804	7367344	585.42	162	-60/59	90	94	4	1.51
KBRC2047	206758	7367317	585.32	162	-60/58	87	91	4	2.38
KBRC2047	206758	7367317	585.32	162	-60/58	97	99	2	1.43
KBRC2047	206758	7367317	585.32	162	-60/58	120	121	1	1.04
KBRC2048	206929	7367174	584.73	132	-60/59	68	73	5	0.83
KBRC2049	206857	7367378	585.83	108	-60/59	72	73	1	5.9
KBRC2049	206857	7367378	585.83	108	-60/59	96	98	2	2.76
KBRC2056	209258	7366870	585	210	-61/189	90	91	1	9.22
KBRC2056	209258	7366870	585	210	-61/189	109	110	1	2.45
KBRC2057	209282	7366947	585	210	-61/199	112	115	3	2.9
KBRC2059	209255	7366938	585	216	-60/198	101	102	1	3.75
KBRC2059	209255	7366938	585	216	-60/198	112	113	1	3.58
KBRC2060	209273	7366975	585	204	-60/201	112	114	2	0.55
KBRC2061	209496	7366841	585	192	-61/196	118	120	2	15
KBRC2062	209450	7366882	585	204	-61/198	114	117	3	1.26
KBRC2063	209467	7366919	585	210	-60/199	72	77	5	0.61
KBRC2063	209467	7366919	585	210	-60/199	130	137	7	3.13
KBRC2063	209467	7366919	585	210	-60/199	157	159	2	1.11
KBRC2063	209467	7366919	585	210	-60/199	176	178	2	2.46
KBRC2064	209514	7366902	585	210	-60/198	75	78	3	1.35
KBRC2064	209514	7366902	585	210	-60/198	137	140	3	2.12
KBRC2064	209514	7366902	585	210	-60/198	147	148	1	0.56
KBRC2064	209514	7366902	585	210	-60/198	156	157	1	1.26
KBRC2065	209526	7366938	585	210	-60/198	171	173	2	1.3
KBRC2066	209519	7367013	585	252	-59/198	167	168	1	3.02
KBRC2067	209409	7366870	585	174	-60/197	100	101	1	0.75
KBRC2067	209409	7366870	585	174	-60/197	113	115	2	1.5
KBRC2068	209436	7366951	585	204	-60/201	131	132	1	1.36
KBRC2068	209436	7366951	585	204	-60/201	138	139	1	7.33
KBRC2068	209436	7366951	585	204	-60/201	153	155	2	1.61

Appendix 3
JORC Code, 2012 Edition – Table 1

Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	• *Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.* • *Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.* • *Aspects of the determination of mineralisation that are Material to the Public Report.* • *In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.*	**KGP Resource update** Previous drilling at the Bibra deposit has been completed by two companies Independence Group (IGO) and Capricorn Metals Group LTD (CMM) using a combination of Reverse Circulation (RC) and diamond drilling (DD). The methods of collection have been very similar in terms of sampling procedures, drilling methods and sampling quality. Grade Control drilling in the form of aircore (AC) and RC has been completed on a mostly continual basis since late 2020 at the project. For RC drilling from 2019 onwards the standard method of sample collection includes the following: For Reverse Circulation (RC) drilling 2kg - 3kg samples are split from dry 1m bulk samples. The sample was collected through a cyclone and cone splitter. Once drilling reached fresh rock a fine spray of water was used to suppress dust and limit the loss of fines thorough the cyclone chimney. RC Field duplicates were collected at a ratio of 1:40 and collected at the same time as the original sample through the B chute of the cone splitter. Matrix matched CRMS and OREAS certified reference material (CRM) were inserted at a ratio of 1:40. The grade ranges of the CRM's were selected based on grade populations and economic grade ranges. Samples were sent to the laboratory where they were pulverised to produce a 50 g charge for fire assay. For RC drilling from 2015 to 2019 the standard method of sample collection includes the following: 2kg - 3kg samples are split from dry 1m bulk samples. The sample was collected through a cyclone and cone splitter. Once drilling reached fresh rock a fine spray of water was used to suppress dust and limit the loss of fines thorough the cyclone chimney. A second 2kg - 3kg sample was collected at the same time as the original sample. This sample was stored on site and retained for follow up analysis and testwork. The bulk sample of the main ore zone was discharged from the cyclone directly into green bags. The bulk sample from the waste was dumped into piles on the ground. During the sample collection process, the cone split original and duplicate calico samples and the reject green bag samples were weighed to test for biases and sample recoveries. The majority of the check work was undertaken through the main ore zones. Upon determination that there were no sampling problems in 2019 drilling continued without these measures. RC Field duplicates were collected at a ratio of 1:20 through the mineralised zones (1:40

Criteria	JORC Code explanation	Commentary
		elsewhere) and collected at the same time as the original sample through the B chute of the cone splitter. For the diamond drilling, core was half cut in half using a corewise automatic core saw. Matrix matched CRMS and OREAS certified reference material (CRM) were inserted at a ratio of 1:20 through the mineralised zone (1:40 elsewhere). The grade ranges of the CRM's were selected based on grade populations and economic grade ranges. In 2012, RC samples were collected for 1m intervals using a rig-mounted cone splitter. Wet samples were grab sampled and recorded as such in the database, few were within mineralised zones. NQ core was half-core sampled and HQ/HQ3 core was initially quarter-core sampled. Issues with quarter-coring in the regolith with complete disintegration of the sample and loss of material were identified, and reverted to half-core sampling with less water for better sample quality. Standards, blanks and field duplicates were inserted into each batch of samples submitted to the laboratory. Prior to 2011, RC samples were collected at the rig using a cone splitter. RC samples were originally composited to 2m by taking scoops from each of the 1m interval and submitted to Genalysis for sample preparation and analysis. Samples that returned values >0.5g/t Au were submitted as 1m samples to Genalysis. In 2011, RC samples were not composited and 1m interval samples were sent directly to Genalysis. A rig mounted cone splitter was used to split the samples. NQ2 core was half-core sampled and PQ and PQ3 core was quarter-core sampled using a manual core-cutting diamond saw without water in the oxide zone. The dry cutting was to prevent loss of clays for the metallurgical samples. Sample quality is considered to be good and all RC drilling within the resource area was dry. **Exploration Results** RC drilling at KGP and MGGP completed by Topdrill with the same techniques and process at both. For Reverse Circulation (RC) drilling 2kg - 3kg samples are split from dry 1m bulk samples. The sample was collected through a cyclone and cone splitter. Once drilling reached fresh rock a fine spray of water was used to suppress dust and limit the loss of fines thorough the cyclone chimney. For regional first pass RC drilling 1m sample was collected in a bucket and then tipped in neat lines on the ground. The piles were then sampled by using a spear to collect a field composite (4m RC) 2.0kg to 3.0kg sample which was then placed in a calico bag. Field duplicates were not collected for the regional RC drilling. CRM were inserted at a ratio of 1:30 composites for regional RC. The grade ranges of the CRM's were selected based on grade populations and economic grade ranges. +100-200ppb will then have their corresponding 1m rig split samples sent for fire assay with the below 1m QAQC applied appropriate for use in JORC resource reporting. 1m RC Field duplicates were collected at a ratio of 1:40 and collected at the same time as the original sample through the B chute of the cone splitter. Matrix matched CRMS and OREAS certified reference material (CRM) were inserted at a ratio of 1:40. The grade ranges of the CRM's were selected based on grade populations and economic grade ranges.

Criteria	JORC Code explanation	Commentary
		Samples were sent to the laboratory where they were pulverised to produce a 50 g charge for fire assay. For regional aircore exploration (AC) drilling a primary sample was collected from the drill rig. The sample was collected in a bucket and then tipped in neat lines on the ground. The piles were then sampled by using a spear to collect a field composite (4m AC) 2.0kg to 3.0kg sample which was then placed in a calico bag. The last 1m interval for each regional AC hole (EOH) was sampled separately for multi element analysis. Field duplicates were not collected for the regional AC drilling. CRM were inserted at a ratio of 1:30 composites for regional AC. The grade ranges of the CRM's were selected based on grade populations and economic grade ranges. Regional AC samples were sent to ALS laboratory where they were pulverised to produce a 25 g charge for aqua regia 51 elements including Au and element multielement analysis for the field composites using ALS code AuME-TL43analysis. Heap Leach AC was collected in 1m calicos using regional AC drilling techniques with a splitter off the cyclone,with drilling producing 2kg - 3kg samples which are split from dry 1m bulk samples. Field duplicates were collected at a ratio of 1:40 and collected at the same time as the original sample through the B chute of the cone splitter. Matrix matched CRMS and OREAS certified reference material (CRM) were inserted at a ratio of 1:40. The grade ranges of the CRM's were selected based on grade populations and economic grade ranges. Samples were sent to the laboratory where they were pulverised to produce a 50 g charge for fire assay.
Drilling techniques	• *Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).*	RC drilling rigs operated by Topdrill, Ranger, Profile and Blue Spec were used to collect chip samples over the numerous programmes. Some early drilling used face-sampling bits of 135mm diameter, with the majority of holes using 140mm diameter. Grade Control AC was completed using an 89mm AC blade bit and 140mm diameter for RC grade control. For exploration Prospect Drilling was used for AC drilling using an 89mm blade bit. Diamond drilling rigs operated by Westralian Diamond Drillers, Blue Spec, Boart and Foraco were used to collect diamond core samples over the numerous programmes. NQ2, PQ3, PQ, HQ3 and HQ are the core sizes collected. RC precollars were regularly used through barren zones and range from 20m to 200m. Core was orientated by Reflex ACE and Ezymark orientation tools.
Drill sample recovery	• *Method of recording and assessing core and chip sample recoveries and results assessed.* • *Measures taken to maximise sample recovery and ensure representative nature of the samples.* • *Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.*	Prior to 2019 during the sample collection process, the cone split original and duplicate calico samples and the reject green bag samples were weighed to test for biases and sample recoveries. The majority of the check work was undertaken through the main ore zones. This process showed that the majority of ore grade samples had recoveries greater than 80%. Recovery measurement and weighing of bulk sample was discontinued after samples were determined to be of good quality. Once drilling reached fresh rock a fine spray of water was used to suppress dust and limit the loss of fines thorough the cyclone chimney.

Criteria	JORC Code explanation	Commentary
		At the end of each metre the bit was lifted off the bottom to separate each metre drilled. The majority of samples were of good quality with ground water having minimal effect on sample quality or recovery. From the collection of recovery data, no identifiable bias exists. In 2012, RC sample recovery was variable, particularly in the regolith. Sample quality was recorded during logging and qualitative recovery codes were assigned to each sample. Sample weights were measured for each component of RC hole cuttings in mineralised zones, with results showing that regolith samples were generally poor quality (both under and over-weight samples) and quality was moderate in the other zones. Core was reassembled for mark-up and was measured, with metre marks and down-hole depths placed on the core. Depths were checked against driller's core blocks and discrepancies corrected after discussion with drillers. Core loss was recorded in the geological log. Core recovery was generally good. RC sample recovery prior to 2012 has been logged as good with samples kept dry during drilling. AC: Visual recovery information was collected at the time of the AC drilling. There is no obvious relationship between sample recovery and grade.
Logging	• *Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.* • *Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.* • *The total length and percentage of the relevant intersections logged.*	Reverse circulation chips were washed and stored in chip trays in 1m intervals for the entire length of each hole for resource drilling. Chips were visually inspected and logged to record lithology, weathering, alteration, mineralisation, veining and structure. Data on rocktype, deformation, colour, structure, alteration, veining, mineralisation and oxidation state were recorded. RQD, magnetic susceptibility and core recoveries were recorded. RC chips sample quality and weights were also recorded, including whether wet or dry. Grade control holes are logged for lithology, colour, veining, mineralisation, hardness and oxidation state. Logging is both qualitative and quantitative or semi-quantitative in nature. Core was photographed both dry and wet. AC: AC chips were washed and stored in chip trays in 1m intervals for the entire length of each hole. Holes of interest are retained, all others are disposed of. Chip trays of all EOH intervals are retained. Chip trays were stored on site in a sealed container. Chips were visually inspected and logged by an on-site geologist to record lithology (including rock type, oxidation state, weathering, grain size, colour, mineralogy, and texture), alteration, mineralisation, veining, structure, sample quality (dry/wet, contamination) and approximate water flow down hole. Mineralisation, veining and water flow were quantitative or semi-quantitative in nature; the remainder of logging was qualitative.

Criteria	JORC Code explanation	Commentary
Sub-sampling techniques and sample preparation	• *If core, whether cut or sawn and whether quarter, half or all core taken.* • *If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.* • *For all sample types, the nature, quality and appropriateness of the sample preparation technique.* • *Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.* • *Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.* • *Whether sample sizes are appropriate to the grain size of the material being sampled.*	For RC holes drilled since March 2016 (since hole KBRC284) samples were split from dry, 1m bulk sample via a cone splitter directly from the cyclone. The quality control procedure adopted through the process includes: Weighing of both Calico samples and reject sample to determine sample recovery compared to theoretical sample recovery and to check sample bias through the splitter. This practice was discontinued during the 2019 programme once good sample quality and recovery was verified. Field duplicates were collected at a ratio of 1:20 through the mineralised zones (1:40 elsewhere) prior to 2019, and 1:40 in all zones since, and collected at the same time as the original sample through the B chute of the cone splitter. OREAS certified reference material (CRM) was inserted at a ratio of 1:20 through the mineralised zone (1:40 elsewhere) prior to 2019, and 1:40 in all zones since. The grade ranges of the CRM's were selected based on grade populations and economic grade ranges. The duplicates and CRM's were submitted to the lab using unique sample ID's. 2kg – 3kg RC samples are submitted to the laboratory. Samples are oven dried at 105°C then jaw crushed to -10mm followed by a Boyd crush to a nominal -2mm. Samples were rotary split to 2.5kg. Samples were then pulverised in LM5 mills to 85% passing 75µm under sample preparation code EX03_05 which consists of a 5 minute extended preparation for RC/Soil/RAB. The extended time for the pulverisation is to improve the pulverisation of samples due to the presence of garnets in the samples. All the samples were analysed for Au using the FA50/MS technique which is a 50g lead collection fire assay. All core has been cut into half or quarter core for sampling. For early drillholes KBRC005-010, RC composite samples (2m) were submitted to Genalysis where they were sorted, dried and the total sample pulverised in a single stage mix and grind if the sample mass was <3kg. Samples >3kg mass were riffle split using a 50:50 splitter and one half pulverised. Samples were analysed for Au using an aqua regia digestion (AR10/OM) of a 10g pulp sample with ICP-MS determination. Samples that returned values >0.5g/t Au were submitted to Genalysis as 1m resplit samples and prepared in a similar manner as the composites. For drillholes from KBRC011 to KBRC283 (2009-2012), no compositing took place, 1m split RC samples and core samples were submitted to Genalysis for fire assay. Samples were oven dried at 105°C then jaw crushed to -10mm followed by a Boyd crush to a nominal -2mm. Samples were rotary split to 2.5kg (2012 drilling). Samples were then pulverised in LM5 mills to 85% passing 75µm. All the samples were analysed for Au using the FA50/AAS technique which is a 50g lead collection fire assay with analysis by Flame Atomic Absorption Spectrometry. The fire assay method is considered a suitable assaying method for total Au determination. The aqua regia digestion results (used for samples that were <0.5g/t Au) may not allow for total Au determination in the transition and fresh rock zones. Aqua regia

Criteria	JORC Code explanation	Commentary
		samples are only present for 5 holes and therefore represent only a very small percentage of the samples. For core and RC samples the sample preparation technique is appropriate and is standard industry practice for a gold deposit. Quality control for maximising representivity of samples included sample weights, insertion of field duplicates and laboratory duplicates. Regional AC samples were collected as 4m field composites using a spear from the individual 1m sample piles on the ground. Field duplicates were not collected for the regional AC drilling. CRM were inserted at a ratio of 1:30 composites for AC. The grade ranges of the CRM's were selected based on grade populations and economic grade ranges. The CRM's were submitted to the lab using unique sample ID's. 2kg – 3kg AC samples are submitted to the laboratory. Samples are oven dried at 105°C then crushed and pulverised. Heap Leach AC was collected in 1m calicos using regional AC drilling Techniques with a splitter off the cyclone, with drilling producing 2kg - 3kg samples which are split from dry 1m bulk samples. Field duplicates were collected at a ratio of 1:40 and collected at the same time as the original sample through the B chute of the cone splitter. Matrix matched CRMS and OREAS certified reference material (CRM) were inserted at a ratio of 1:40. The grade ranges of the CRM's were selected based on grade populations and economic grade ranges. Samples were sent to the laboratory where they were pulverised to produce a 50 g charge for fire assay.
Quality of assay data and laboratory tests	• *The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.* • *For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.* • *Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.*	In the 2021/2022/2023 drilling samples were submitted to MinAnalytical laboratory, ALS and Jinnings in Perth and completed by a single 50g fire assay, which is a total assay. In the 2019 drilling samples were submitted to Intertek and Aurum laboratories in Perth and completed by a single 50g fire assay, which is a total assay. Assaying at Intertek also included Pt and Pd analysis. Grade Control samples are assayed at Aurum by a single 50g fire assay. In the 2017 to 2018, drilling samples were submitted to Intertek laboratory in Perth and completed by a single fire assay. Analysis was also received for Pt and Pd. In the 2015 to 2016 drilling samples were submitted to the Intertek laboratory in Perth. In the main mineralised zone four fire assays from the sample pulp were completed, and only one in the waste zones. For samples prior to 2015, only single fire assay determination occurred on each sample. Analysis was also received for Pt and Pd. The samples from 2018 & 2015 drilling were determined for gold, pt, pd and additional elements/base metals, using ICP optical emission spectrometry and ICP mass spectrometry. Samples prior to 2015, were analysed using AAS. Field duplicates were collected at a ratio of 1:20 through the mineralised zones (1:40 elsewhere) and collected at the same time as the original sample through the B chute of the cone splitter. OREAS certified reference material (CRM) was inserted at a ratio of 1:20 through the mineralised zone (1:40 elsewhere), and 1:40 through all zones after 2019. The

Criteria	JORC Code explanation	Commentary
		grade ranges of the CRM's were selected based on grade populations and economic grade ranges. Twin holes from the different drilling programs showed that over an intercept, the grades and lengths of mineralisation compared well, whereas at the individual assay level the results show some variability. Regional AC drilling samples were submitted to ALS laboratory in Perth. No field duplicates were collected for the AC drilling. CRM were inserted at a ratio of 1:30 composites for the AC. The grade ranges of the CRM's were selected based on grade populations and economic grade ranges.
Verification of sampling and assaying	• *The verification of significant intersections by either independent or alternative company personnel.* • *The use of twinned holes.* • *Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.* • *Discuss any adjustment to assay data.*	Logging and sampling were recorded directly into a Micromine field marshal template prior to 2020, and Micromine Geobank template since 2020, which utilise lookup tables and in file validation on a Toughbook by the geologist on the rig. Validated data was sent to the database administrator in Perth who then carried out independent verifications using Maxwell's Datashed. Assay results when received were plotted on section and were verified against neighbouring holes. Analysis of the RC/diamond hole twinning up, showed that mineralised intervals above a cut-off grade of 0.3g/t Au were similar in length and moderately well correlated in grade. From time to time assays will be repeated if they fail company QAQC protocols, however no adjustments are made to assay data once accepted into the database.
Location of data points	• *Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.* • *Specification of the grid system used.* • *Quality and adequacy of topographic control.*	Drillhole collar positions for 2019 onwards drilling were surveyed after drilling using a Trimble RTK system, comprising an R10-2 Base and Receiver and a Trimble TSC3 Data Collector. The Base was set up on KB01 located on "Laterite Hill", which was adopted as control for the surveys. All surveys were checked against and closed off on KB01DRM to ensure accuracy. Down hole surveys were undertaken on 30m increments from end of hole, using a Reflex down hole gyroscopic tool. 2015 - 2018 drillhole collar positions were surveyed by Survey Group out of Port Hedland WA and Osbourne Park, WA. The survey was conducted using Trimble R8 RTK GPS base and rover, with an assumed positional accuracy of ±0.025m Horizontal and ±0.050m Vertical. Control used was installed by MHR Surveyors and issued to Survey Group by CMM. GPS base station was positioned over KB01 and checked against KB01DRM. Downhole surveys were collected by driller operated in-rod reflex north seeking gyro at the end of each hole. The measurements were taken every 10 to 30 metres. 2009 - 2012 drillhole collar positions were surveyed by licensed surveyors MHR Surveyors of Cottesloe, WA. The instrument used was a Trimble R8 GNSS RTK GPS (differential) system. Expected relative accuracies from the GPS base station were ±2cm in the horizontal and ±5cm in the vertical direction. Co-ordinates were surveyed in the MGA94 grid system. Downhole surveys were carried out by the drillers at about 50m intervals using a Reflex EZ shot digital downhole camera. Readings were taken in a non-magnetic stainless steel rod near the bottom of the drill string. The depth, dip, azimuth and magnetic field were recorded

Criteria	JORC Code explanation	Commentary
		at each survey point. Drillhole location data was initially captured in the MGA94 grid system and have been converted to a local grid for resource estimation work. The natural surface topography was modelled using a DTM generated from the 2012 airborne LiDAR survey conducted in November 2012 by AAM Pty Limited. The DTM was rotated in-house to the local grid coordinate system. Horizontal point accuracy is expected to be <0.33m and vertical accuracy to 0.15m. Ground control was established using RTK GPS and ALTM3100 Static GPS. The reference datum was GDA94 and the projection was MGA Zone 51, with the data supplied as 50cm and 1m contours in MGA Zone 51. Topographic control is of good quality and is considered adequate for resource estimation. The end of March 2023 depletion surface was surveyed by authorised site based surveys using drone technology. Regional AC drillhole collar positions were surveyed before and after drilling using a handheld GPS. Drillhole location data was captured in the MGA94 grid system. Down hole surveys were not undertaken for the any of the drilling due to the shallow nature of the holes. Any regional AC intercepts will be followed up with infill RC drilling using downhole surveys and more accurate collar survey technique. Heap Leach AC collar positions were surveyed using hand held GPS. Drillhole location data was initially captured in the MGA94 grid system. Before further resource evaluation work the drillhole locations will be picked up with DGPS by qualified surveyors.
Data spacing and distribution	• *Data spacing for reporting of Exploration Results.* • *Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.* • *Whether sample compositing has been applied.*	Drilling has been completed on a 50 x 50m and 25m x 25m and 25m x 50m grid for resource drilling, and 10m by 5m or 7.5m by 7.5m for grade control drilling. Drill spacing is sufficient for current resource classification. Samples were collected in 1 metre intervals and analysed for each metre down the hole. Whole hole is analysed at Bibra. At Tramore the upper portions of some holes were not sampled through the unmineralised Bangemall Basin. Prior to 2011 1m RC samples were collected at the rig using a cone splitter, with 2m composites taken from each of the 1m intervals and submitted to Genalysis for sample preparation and analysis. Samples that returned values >0.5g/t Au were submitted as 1m samples to Genalysis. Regional AC samples were collected and analysed for gold and multielement by 4m field composites down the hole, with the EOH individual metre sampled separately for multi element analysis. Hole spacing was predominantly 100m x 400m, 200m x 200m and 50m x 100m for AC. Heap Leach AC drilling was predominantly 12.5x12.5m spacing.
Orientation of data in relation to geological structure	• *Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.* • *If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.*	Drill lines are oriented across strike on an MGA grid. MGGP orebody dips at 80 degrees to the East and KGP 25 degrees to the west. Holes in the drill Programmes have been mostly drilled at inclination of -55 to -60 degrees at MGGP and KGP. The orientation of the drilling is suitable for the mineralisation style and

Criteria	JORC Code explanation	Commentary
		orientation of the target mineralisation. Where possible the AC exploration drilling programmes are planned to be drilled perpendicular to the orientation of the geology. Significant mineralisation intervals in the AC will be followed up with infill RC drilling to better understand the orientation of mineralisation.
Sample security	• *The measures taken to ensure sample security.*	Calico sample bags are sealed into green bags/polyweave bags and cable tied. These bags were then sealed in bulka bags by company personnel, dispatched by third party contractor, in-company reconciliation with laboratory assay returns.
Audits or reviews	• *The results of any audits or reviews of sampling techniques and data.*	All programmes are reviewed by company senior personnel. Prior to commencement of the 2016 drill program a meeting of industry specialists was held to discuss the sampling and analytical techniques to get consensus and or improvements on the drilling and sampling protocol. Prior to 2016, a review of practices documented in the IGO technical report supplied to Optiro Pty Ltd in 2012 as part of the resource estimate review did not highlight any significant issues. Optiro completed a resource audit of the 1606 and 1804 models which included auditing of the data. No fatal flaws were identified. The Competent Person for Exploration Results reported here has visited the project areas where sampling has taken place and has reviewed and confirmed the sampling procedures.

Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	• *Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.* • *The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.*	MGGP: The resource is located across mining tenements held by wholly owned Capricorn subsidiaries METROVEX PTY LTD and CRIMSON METALS PTY LTD; being M 59/772, E 59/2450, E 59/2594, E 59/2606, G 59/11, G 59/12, G 59/13, G 59/14, G 59/15, G 59/16, G 59/17, G 59/18, G 59/48, G 59/70, L 59/140, L 59/45, L 59/46, L 59/53, M 59/328, M 59/402, M 59/403, M 59/404, P 59/2286, P 59/2287, P 59/2290, P 59/2291, P 59/2306, P 59/2309, P 59/2310. All of the tenements are subject to a 1% NSR royalty to Avenger Projects Ltd, including gold production above 90,000 ounces. A royalty is also payable to St Barbara Limited on all gold production in excess of 20,000 ounces (excluding production from historic waste dumps and tailings) at the rate of $10 per ounce, applicable to leases M 59/328, M 59/402, M 59/403, M 59/404, G 59/11, G 59/12, G 59/13, G 59/14, G 59/15, G 59/16, G 59/17, G 59/18, L 59/45, L 59/46, L 59/53 No other known impediments exist to operate in the area. KGP: The Bibra deposit is located in M 52/1070 held by Greenmount Resources, a wholly owned subsidiary of Capricorn Metals. M52/1070 is within the area of granted E52/1711 exploration tenement in the Pilbara region

Criteria	JORC Code explanation	Commentary
		of Western Australia. E52/1711 was acquired from BHPB in 2008. South32 (via the spin-out from BHPB) retain a 2% NSR whilst BHPB a claw-back provision whereby BHPB can elect to acquire a 70% equity in the project only if JORC compliant reported resources of 5,000,000 ounces of gold and/or 120,000 tonnes of contained nickel have been delineated. The Nyiyaparli People hold Native Title over the area including E52/1711 and M52/1070. There is no known heritage or environmental impediments over the lease. No other known impediments exist to operate in the area.
Exploration done by other parties	• *Acknowledgment and appraisal of exploration by other parties.*	**MGGP**: The Mt Gibson Gold Deposit (Mt Gibson) has a history of minor gold production dating back to the 1930's when prospectors operated small gold workings at Paynes-Crusoe and Tobias Find. While the area was subject to previous prospecting and company exploration in smaller leaseholdings, the Mt. Gibson Gold Project was first held in more-or-less its present configuration and extent by Reynolds Australia, who commenced exploration in the early 1980's. Soil and laterite sampling resulted in several significant gold and base metal anomalies being defined; follow up rotary air blast (RAB), air core (AC), reverse circulation (RC) and diamond drilling Programmes outlined significant economic laterite and oxide resources. A joint venture between Reynolds Australia Metals and Forsayth Mining Limited (with FML as the operator) began operations in 1986, mining and processing 6.5 million tonnes of laterite ores defined by FML in 1984, followed later by oxide and sulphide ores defined by drilling beneath the laterite orebodies. The project was sold by Reynolds to Camelot Resources in 1995. Continuing exploration resulted in the discovery of further oxide resources, mainly on the Taurus Trend, and the underground quartz-sulphide deposit at Wombat. These resources were subsequently mined and processed, all mining being completed at the end of 1997 and final milling of low grade stockpiles completed in June of 1998. A 4Mt dump leach remained in operation until November 1998, producing 68,868 ounces of gold. Including the dump leach, a total of 16,477,882 tonnes of ore was processed during the life of the operation, for 868,478 ounces of gold at an overall average grade of 1.64g/t Au. **KGP**: Prior to Capricorn Metals, E52/1711 was held by Independence group (IGO) who undertook exploration between 2008 & 2014. Prior to Independence group, WMC (BHPB) explored the area from 2004 to 2008.
Geology	• *Deposit type, geological setting and style of mineralisation.*	**MGGP**: The Mt Gibson Gold Project tenements are located at the southern extremity of the Retaliation Greenstone Belt, in the SW portion of the Yalgoo-Singleton Greenstone Belt in the Murchison Province of the Yilgarn Craton. The tenements are mostly covered by a veneer of alluvial quartz sands and laterite gravels, with sporadic greenstone subcrop and outcrop, increasingly exposed in the north of the project area. The mineralised laterite gravels are situated slightly down-slope from the lode deposits on the Gibson trend. Regionally, the greenstone belt has been metamorphosed to middle amphibolite facies and hosts a number of Au-Cu deposits and prospects, including Golden Grove, 90km to the northwest of Mt.Gibson. The lode style mineralisation at Mt. Gibson is predominantly hosted by three main trends: **The Gibson Trend**

Criteria	JORC Code explanation	Commentary
		The majority of the known and mined mineralisation is hosted by this trend. It is hypothesised to have originally been a gold-copper-zinc rich Volcanogenic Hosted Massive Sulphide (VHMS) deposit that has been overprinted by a later hydrothermal gold mineralising event. This mineralised shear zone has an arcuate north-south to northeasterly strike (trending more north-easterly in the north) and extends for more than seven kilometres from the southern granite contact to beyond the Hornet ore body. The so-called "Mine Sequence" is around 400 metres wide and consists of a parcel of sheared, metamorphosed and chlorite-biotite-muscovite altered mafic volcanics. Numerous felsic porphyries intrude the Mine Sequence. Mineralisation is hosted within multiple sets of elongate lodes with strong strike continuity, which anastomose and pinch-swell along strike and to depth. The main lode systems include Hornet, Enterprise, Orion and S2. **The Taurus Trend** The north-westerly trending Taurus Trend lies west of and diagonal to the Gibson Trend. Mineralisation is intimately associated with an apparently continuous felsic unit emplaced into the northwest trending shear and was discovered late in the life of the mining operation. It is characterised by discontinuous ore bodies, and strongly mineralised quartz-sulphide veining. The ore bodies on this trend include Sheldon and Wombat which, although not as continuous in strike as the ore bodies on the Gibson Trend, show a higher gold tenor. **The Highway Trend** The Highway Trend is a northeast trending shear zone, hosted by a mafic sequence in the western terrain, 11km northwest of the main mining area. This trend hosts the Highway ore body, and the Phoenix and Aquarius Prospects. It shares many of the characteristics of the Gibson trend, but it appears to lack the VHMS mineralising event and has generally been regarded as a predominantly low-grade system, although work from previous explores suggest it may have greater persistence and significance than previously thought and hence justifies further attention. The project area also hosts a number of BIF and quartz hosted small mineral occurrences including Paynes-Crusoe and MacDonald's Find. **KGP**: Bibra is part of a large-scale Archaean aged gold mineralised system. The resource is hosted within a package of deformed meta-sediments which has developed on at least two parallel, shallow dipping structures; Laterite oxide mineralization has developed over the structures close to surface. The primary mineralisation is strata-bound with lineations identified as controlling higher-grade shoots. The deposit is oxidized to average depths of 50-70m.
Drill hole Information	• *A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:* ○ *easting and northing of the drill hole collar* ○ *elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar* ○ *dip and azimuth of the hole* ○ *down hole length and interception depth* ○ *hole length.*	All relevant drillhole information can be found in section 1 – "Sampling techniques", "Drilling techniques" and "Drill Sample Recovery" and the significant intercepts table.

Criteria	JORC Code explanation	Commentary
	• *If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.*	
Data aggregation methods	• *In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated.* • *Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.* • *The assumptions used for any reporting of metal equivalent values should be clearly stated.*	Reported intercepts include a minimum of 0.5g/t Au value over a minimum length of 1m with a maximum 2m length of consecutive internal waste. No upper cuts have been applied. No aggregation methods have been applied for the rockchips. No metal equivalent values are used.
Relationship between mineralisation widths and intercept lengths	• *These relationships are particularly important in the reporting of Exploration Results.* • *If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.* • *If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').*	**MGGP**: The mineralisation dips steeply to the east, and drilling is generally orientated at 60 degrees to the west, meaning intercepts are roughly perpendicular to mineralisation in the majority of cases. Some vertical holes drilled from the base of mined pits and are therefore at a high degree to the mineralisation. **KGP**: At Bibra, the geometry of the mineralisation has already been defined from previous drilling programs. The intersection angle between drill angle and the perpendicular angle to the ore zone is less than 10 degrees.
Diagrams	• *Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.*	Refer to the diagrams in the body of this report and within previous ASX announcements.
Balanced reporting	• *Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	The accompanying document is considered to be a balanced report with a suitable cautionary note.
Other substantive exploration data	• *Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.*	Systematic metallurgical testwork programs over 2012 to 2019 on master and variability composites from diamond core identifies mineralisation as free milling and amenable to cyanidation, which has been validated by production since 2021. Geotechnical logging has been completed for determining ground conditions for open pit mining.
Further work	• *The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling).* • *Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.*	Resource Definition programs will continue to identify and delineate extensions and repeats at both projects.

Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	JORC Code explanation	Commentary
Database integrity	• *Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.*	Since 2014 drilling has been collected in the field by geologists and field assistants using Micromine's Field Marshall, and now Geobank, program with in-built Validation. Once hole information was finalised on site the information was emailed to the CMM Database

Criteria	JORC Code explanation	Commentary
	• *Data validation procedures used.*	Administrator to load into Datashed SQL database. Prior to 2014, data has been collected by the geologists and field staff in either Excel spreadsheets or acQuire data entry objects on laptops for RC and diamond drilling and loaded into SQL acQuire software. The inherited validated data from IGO was imported into a Datashed SQL database by Maxwell Geoscience. Analytical data was received from the laboratories in electronic ASCII files of varying format and were merged with sampling data already present in the database. Assays received from laboratories were imported by the Database Administrator into the database. Any data files which did not validate were investigated and rectified by field staff or Database Administrator.
Site visits	• *Comment on any site visits undertaken by the Competent Person and the outcome of those visits.* • *If no site visits have been undertaken indicate why this is the case.*	The competent person has made a site visit to Karlawinda as part of this study. All exploration and resource development drilling programmes are subject to review by experienced senior CMM technical staff. These reviews have been completed from the commencement of drilling and continue to the present in recent drilling and mining operations, enabling the competent person to inspect/verify mineralisation controls.
Geological interpretation	• *Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.* • *Nature of the data used and of any assumptions made.* • *The effect, if any, of alternative interpretations on Mineral Resource estimation.* • *The use of geology in guiding and controlling Mineral Resource estimation.* • *The factors affecting continuity both of grade and geology.*	Confidence in the geological interpretation is high. Stratigraphy is consistent and can be correlated between holes and along strike. Production has been ongoing since 2021 enabling validation of this. Geological logging and structural measurements from drillholes have been used to construct the geological model. Sections were interpreted, digitised and a 3D wireframe model constructed. Geological continuity has been assumed along strike and down-dip. The geological interpretation is robust. The geological model was built by on the ground geologists who logged and relogged and interpreted the geology to ensure the geological interpretation was consistent. With the current drill spacing it is unlikely that an alternative interpretation will develop. There is currently sufficient drilling to map the stratigraphic units and laterite zone. The geological model has been used to guide mineralisation envelopes and subsequent mineralisation wireframe modelling. Geological continuity has been assumed along strike and down-dip based on the drilling data. In general, continuity both geologically and grade-wise is good. Grades and thickness are more consistent down-dip than along strike.
Dimensions	• *The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.*	The mineralisation wireframes have been projected down-dip based on wider spaced drilling intercepts; however, this extrapolation has been removed from the resource estimate by limiting the reported tonnes and grade to within a conceptual optimal pit shell ($2,200/oz Au). The main laterite zone extends 1250m along strike and 1150m across. It ranges from 2m to

Criteria	JORC Code explanation	Commentary
		15m in vertical thickness. The primary mineralisation extends below the laterite zone for a further vertical depth of 345m. The transition/fresh rock boundary is about 60m below surface. The primary mineralisation has 4 main sub-parallel zones and several smaller zones. Overall, these zones extend for 1800m along strike (N-S) and 1800m across.
Estimation and modelling techniques	• *The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.* • *The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.* • *The assumptions made regarding recovery of by-products.* • *Estimation of deleterious elements or other non-grade variables of economic significance (eg sulphur for acid mine drainage characterisation).* • *In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.* • *Any assumptions behind modelling of selective mining units.* • *Any assumptions about correlation between variables.* • *Description of how the geological interpretation was used to control the resource estimates.* • *Discussion of basis for using or not using grade cutting or capping.* • *The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.*	The MRE has been estimated using Ordinary Kriging (OK) in Surpac with no change of support. The OK estimation was constrained within Au mineralisation domains generated in Surpac. These were defined from the resource drilling and guided by a geological model created in Micromine. OK is considered an appropriate grade estimation method for the mineralisation given drilling density and mineralisation style, which has allowed the development of robust and high confidence estimation constraints and parameters. The grade estimate is based on 1m down-the-hole composites of the resource dataset created in Surpac each located by their mid-point co-ordinates and assigned a length weighted average gold grade. 1m composite length was chosen because it is a multiple of the most common sampling interval (1.0 metre). Statistical analysis identified a high-grade population which was flagged in the model using an indicator estimate at 1g/t Au. This enabled a high-grade restriction to be used involving those flagged blocks being estimated by a composite file within that flagged area cut to a higher upper-cut. The remaining portions of the domain are estimated with the total domain composite file cut to a lower uppercut. The high-grade restriction and high-grade cuts (as described below) have been applied to composites to limit the influence of higher-grade data. Statistical and geostatistical analysis was completed on the domain coded composite file (1m composites). This included exploration data analysis, boundary analysis and grade estimation trials. The variography applied to grade estimation has been generated using Surpac. These investigations have been completed on each ore domain separately. An independent multiple indicator kriging (MIK) check estimate was completed as part of the previous 2020 MRE which compared within acceptable levels to the Capricorn OK estimate. Metal is within 10% between the two models at multiple scales of reporting. The site based Grade Control estimate was utilised as the check estimate for the current study, which compares within 5% for tonnes and grade. No by-products are present or modelled. No deleterious elements have been estimated or are important to the project economics\planning. Block dimensions are 10m (east) by 10m (north) by 5m (elevation) (with sub-blocking in the Z direction to 2.5m to better suit the flat lying laterite mineralisation) (5m by 5m by 2.5m at KGP East) and was chosen as it approximates SMU for the deposit, and a quarter to half the drill hole spacing. The oxide/fresh interpolation utilised 3 estimation passes, with category 1 adopting a 40m

Criteria	JORC Code explanation	Commentary
		octant search (25m for KGP East), 16 minimum/64 maximum composites used and a maximum of 4 composites per drill hole, with only 4 adjacent octants allowed to fail the search criteria. Category 2 uses a 60m (50m for KGP East) search distance, 16 minimum/64 maximum composites, 4 maximum per hole and 4 adjacent octants allowed to fail the criteria. Category 3 uses a 100m (100m for KGP East) search distance, 8 minimum/64 maximum composites, 4 maximum per hole and 8 adjacent octants allowed to fail the criteria. The laterite portion of the deposit is estimated into the sub-blocked Z size of 2.5m. The search on each category is orientated to align to the orientation of the mineralisation of each specific domain. No selective mining units were assumed in this estimate. No correlated variables have been investigated or estimated. The grade estimate is based on mineralisation constraints which have been interpreted based on a lithological and weathering interpretation, and a nominal 0.1g/t Au lower cut-off grade. The mineralisation constraints have been used as hard boundaries for grade estimation wherein only composite samples within that domain are used to estimate blocks coded as within that domain. Statistical investigations have been completed to test the change in statistical and spatial characteristics of the domains grouped by weathering showing there to be little variation between profiles, hence they have been estimated inclusively. A review of the composite data captured within the mineralisation constraints was completed to assess the need for high grade cutting (capping). This assessment was completed both statistically and spatially to determine if the high-grade data clusters or were isolated. On the basis of the investigation it was decided to utilise a high-grade restriction, and appropriate high-grade cuts were applied to all estimation domains. The grade estimate was checked against the input drilling/composite data both visually on section (cross and long section) and in plan, and statistically on swath plots as well as against production and grade control.
Moisture	• *Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.*	Tonnages have been estimated on a dry basis.
Cut-off parameters	• *The basis of the adopted cut-off grade(s) or quality parameters applied.*	The MRE is reported at a cutoff grade of 0.3g/t for laterite, 0.3g/t for oxide, 0.4g/t for transitional and 0.4g/t for fresh. This is determined from standardised parameters used to generate the open pit MRE reporting shell, and also takes into account actual mining practices.
Mining factors or assumptions	• *Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.*	Currently a contractor-operated open-pit mining option is the basis for the cut-off grade. Ore and waste is paddock blasted on 5m benches and subsequently excavated as 2.5m flitches utilising a conventional excavator and truck mining fleet to facilitate moderate ore excavation selectivity.

Criteria	JORC Code explanation	Commentary
Metallurgical factors or assumptions	• *The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.*	Test work was completed during 2017 using 32 composite samples from 779 metres of core. The Bibra ore is classified as free milling, with a high gravity recoverable gold component (up to 45%). Overall, gravity plus leach gold recoveries are in the range of 93% to 96%. The Bibra ore is relatively clean, with minimal to no cyanide or oxygen consuming gangue minerals present in the ore, leading to low residual WAD cyanide levels (<50ppm) in the leach circuit tailings solution. No testwork has yet been undertaken on KGP East ore zones. A gold recovery value of 95% was used in the generation of the open pit MRE reporting shells.
Environmental factors or assumptions	• *Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.*	Waste rock from open pit operations is placed in a waste rock landform adjacent to open pit operations, progressively contoured and revegetated throughout mine life. Process plant residue is disposed of in a surface tailings storage facility (TSF). Adoption of an upstream, central decant design utilises mine waste material for dam wall construction and facilitates water recovery to supplement process water requirements. Sufficient volumes of oxide material, able to be made sufficiently impermeable, is available in the overburden stream to enable acceptable TSF construction.
Bulk density	• *Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.* • *The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit.* • *Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.*	Bulk density values have been calculated from 3,976 measurements collected on site and at laboratory using the water immersion method. Data has been separated into lithological and weathering datasets and mean density values derived.
Classification	• *The basis for the classification of the Mineral Resources into varying confidence categories.* • *Whether appropriate account has been taken of all relevant factors (ie relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).* • *Whether the result appropriately reflects the Competent Person's view of the deposit.*	The Measured, Indicated and Inferred classification reflects the relative confidence in the estimate, the confidence in the geological interpretation, the drilling spacing, input data, the assay repeatability and the continuity of the mineralisation. The strategy adopted in the current study uses category 1 and 2 from the 3-pass octant search strategy to guide interpretation of a classification surface where Indicated is above the surface and Inferred being below. This results in a geologically sensible classification whereby Category 1 and 2 are surrounded by data in close proximity. Category 3 blocks may occur on the peripheries of drilling but are still related to drilling data within reasonable distances. No measured has been applied in the classification method. This classification reflects the Competent Person's view of the deposit.
Audits or reviews	• *The results of any audits or reviews of Mineral Resource estimates.*	The resource model has been reviewed for fatal flaws internally, although no audit has been completed on the MRE. An independent check estimate was completed using MIK as part of the 2020 study and compared within acceptable levels, as does the site based grade control estimation.

Criteria	JORC Code explanation	Commentary
Discussion of relative accuracy/ confidence	• *Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.* • *The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.* • *These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.*	The confidence level is reflected in the classification of the estimate. Mineralisation modelled but outside the $2,200/oz Au reporting shell has been excluded from the estimate. The Mineral Resource estimate is an undiluted global estimate. Production data compares very closely to the resource estimate with, giving high confidence to the performance going forward.

Section 4 Estimation and Reporting of Ore Reserves

(Criteria listed in section 1, and where relevant in sections 2 and 3, also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral Resource estimate for conversion to Ore Reserves	• *Description of the Mineral Resource estimate used as a basis for the conversion to an Ore Reserve.* • *Clear statement as to whether the Mineral Resources are reported additional to, or inclusive of, the Ore Reserves.*	The Mineral Resource estimate for the Bibra deposit which formed the basis of this Ore Reserve estimate was compiled by the Capricorn Competent Persons utilising relevant data. The estimate is based on Reverse Circulation (RC) holes and diamond holes of exploration drilling and assay data, as well as Aircore (AC) and RC grade control data. The data set, geological interpretation and model was validated using Capricorn's internal and Quality Assurance and Quality Control (QAQC) processes and compared to production. Ordinary Kriging was utilised to estimate the resource. The individual block size for estimation was 10 m x 10 m x 5 m, with sub-blocking at 2.5m in the Z direction for effective boundary definition for the laterite portion of the deposit. The Mineral Resources are reported inclusive of the Ore Reserve.
Site visits	• *Comment on any site visits undertaken by the Competent Person and the outcome of those visits.* • *If no site visits have been undertaken indicate why this is the case.*	The Competent Person did not conduct a site visit. This is because: • They are already familiar with the region and project • As it is an operating mine with actual costs/results/data along with the availability of drone imagery and videos.
Study status	• *The type and level of study undertaken to enable Mineral Resources to be converted to Ore Reserves.* • *The Code requires that a study to at least Pre-Feasibility Study level has been undertaken to convert Mineral Resources to Ore Reserves. Such studies will have been carried out and will have determined a mine plan that is technically achievable and economically viable, and that material Modifying Factors have been considered.*	The Karlawinda Gold Project is a fully operational open pit mining operation with an operating stand-alone CIL processing facility. The Karlawinda Gold Project was the subject of a full feasibility study in 2017. The current study has included all aspects of the operation of the existing mine including all inputs related to operational costs and actual production parameters. Financial modelling completed as well as operational performance shows that the project is economically viable under current assumptions.
Cut-off parameters	• *The basis of the cut-off grade(s) or quality parameters applied.*	Variable economic cut-off grades have been applied in estimating the Ore Reserve. Cut-off grade is calculated in consideration of the following parameters: ▪ Gold price of $1,800 AUD

Criteria	JORC Code explanation	Commentary
		▪ Operating costs including ore costs (eg grade control, ROM re-handle) ▪ Process recovery ▪ Transport and refining costs ▪ General and administrative cost ▪ Royalty costs. Cutoff grades are 0.3 g/t Au Laterite, 0.3 g/t Oxide, 0.4 g/t Transitional, 0.4 g/t Fresh.
Mining factors or assumptions	• *The method and assumptions used as reported in the Pre-Feasibility or Feasibility Study to convert the Mineral Resource to an Ore Reserve (i.e. either by application of appropriate factors by optimisation or by preliminary or detailed design).* • *The choice, nature and appropriateness of the selected mining method(s) and other mining parameters including associated design issues such as pre-strip, access, etc.* • *The assumptions made regarding geotechnical parameters (eg pit slopes, stope sizes, etc), grade control and pre-production drilling.* • *The major assumptions made and Mineral Resource model used for pit and stope optimisation (if appropriate).* • *The mining dilution factors used.* • *The mining recovery factors used.* • *Any minimum mining widths used.* • *The manner in which Inferred Mineral Resources are utilised in mining studies and the sensitivity of the outcome to their inclusion.* • *The infrastructure requirements of the selected mining methods.*	The Bibra deposit is mined by open pit mining methods utilising conventional mining equipment. The final pit design is the basis of the Ore Reserve estimate. The selected mining method, design and extraction sequence are tailored to suit orebody characteristics, minimise dilution and ore loss, defer waste movement and capital expenditure, utilise proposed process plant capacity and expedite free cash generation in a safe manner. Geotechnical modelling has been completed by an external consultant on the basis of field logging and laboratory testing of selected dedicated diamond drill core samples from 16 geotechnical diamond drillholes. The recommended geotechnical design parameters assume dry slopes based on adequate dewatering and/or depressurisation ahead of mining. The low-angle dip of the deposit (28º to West) allows for a designed overall wall angle on the Footwall (Eastern side of pit) between ramps of 25º. The western wall (Hanging Wall) of the pit is designed to have an overall slope of 49.8º. A separate hydrogeological report was prepared by independent consultants which considered the infrastructure required to effectively dewater the open pit and pit slopes. This study was supported by the development of test bores and field test pumping analysis. Only open pit mining has been considered in the Mineral Resource and Ore Reserve studies. Mining dilution and recovery modifying factors have not been applied to the Ore Reserve. This has been accounted for in the MRE, and is supported by reconciliation data.. The mining schedule is based on realistic mining productivity and equipment utilisation estimates and also considered the vertical rate of mining development. No Inferred Mineral Resources were used in Ore Reserve calculations. The operational mine plan includes waste rock dumps, a ROM pad, a surface water diversion channel, surface dewatering bores, light and heavy vehicle workshop facilities, explosives storage and supply facilities and technical services and administration facilities.
Metallurgical factors or assumptions	• *The metallurgical process proposed and the appropriateness of that process to the style of mineralisation.* • *Whether the metallurgical process is well-tested technology or novel in nature.* • *The nature, amount and representativeness of metallurgical test work undertaken, the nature of the metallurgical domaining applied and the corresponding metallurgical recovery factors applied.* • *Any assumptions or allowances made for deleterious elements.* • *The existence of any bulk sample or pilot scale test work and the degree to which such*	A processing flowsheet, materials balance, water balance, equipment identification, mechanical and electrical layouts were all developed to FS standard. A tertiary crushing single Ball Mill comminution circuit followed by a conventional gravity and carbon in leach (CIL) process is in operation. This process is considered appropriate for the Bibra ore, which is classified as free-milling.

Criteria	JORC Code explanation	Commentary
	samples are considered representative of the orebody as a whole. • *For minerals that are defined by a specification, has the ore reserve estimation been based on the appropriate mineralogy to meet the specifications?*	The metallurgical process is commonly used in the Australian and international gold mining industry and is considered to be well-tested and proven technology. Significant comminution, extraction, and physical properties testing has been carried out on approximately 2,000kg of half-HQ and NQ diamond drilling core samples from 24 drillholes, and 300kg of RC chip samples. This has been carried out on laterite, oxide, saprock, transitional, and fresh ore types which were obtained across the Bibra deposit and to a depth of approximately 200m. Estimated plant gold recovery ranges from 91.8% to 94.1% depending on grind size and ore type, which has been validated by production. No deleterious elements of significance have been determined from metallurgical test work and mineralogy investigations.
Environmental	• *The status of studies of potential environmental impacts of the mining and processing operation. Details of waste rock characterisation and the consideration of potential sites, status of design options considered and, where applicable, the status of approvals for process residue storage and waste dumps should be reported.*	Environmental studies have been completed for the existing mining operation at Karlawinda Gold Project, and all approvals are in place. A Native Vegetation Clearing Permit has been granted for the project site. The Mining Proposal will be updated for mining and processing of the increased Ore Reserve. Waste rock and tailings characterisation work has been completed and all waste types and tailings are non-acid forming and have limited metal leachate potential. Waste rock and tailings storage locations have been selected based on suitable geographical characteristics and proximity to the pit and plant. Department of Water and Environmental Regulation (DWER) have granted a works approval under the Environmental Protection Act 1986 to construct the gold processing plant and tailings storage facility, inert and putrescible landfill and sewage facility at the Karlawinda Gold Project. An application will be made to amend these approvals to allow for the processing of the increased Ore Reserve.
Infrastructure	• *The existence of appropriate infrastructure: availability of land for plant development, power, water, transportation (particularly for bulk commodities), labour, accommodation; or the ease with which the infrastructure can be provided, or accessed.*	The project site is within economic distances of existing infrastructure in the east Pilbara region. Services and consumable supplies are delivered by existing roads and a new 40 km Access Road from the Great Northern Highway to the Karlawinda Project. Land availability is unlikely to be an issue, with the mining and exploration tenure held by Capricorn more than covering all project needs. The project lies at the northern boundary of the Weelerrana cattle station. Tailings disposal is within an Integrated Waste Landform whereby tailings are encapsulated by mining waste, rather than having separate waste dumps and tailings facilities. The workforce is Fly In-Fly Out (FIFO) to a CMM bult airstrip and based at a camp on site during rostered days on. Pump testing, modelling and operational abstraction from the Karlawinda borefield indicate that there is sufficient groundwater to service the needs of the Project for the life-of-mine. Power is generated on site utilising natural gas, which is delivered via a 56 km pipeline.

Criteria	JORC Code explanation	Commentary
Costs	• *The derivation of, or assumptions made, regarding projected capital costs in the study.* • *The methodology used to estimate operating costs.* • *Allowances made for the content of deleterious elements.* • *The derivation of assumptions made of metal or commodity price(s), for the principal minerals and co- products.* • *The source of exchange rates used in the study.* • *Derivation of transportation charges.* • *The basis for forecasting or source of treatment and refining charges, penalties for failure to meet specification, etc.* • *The allowances made for royalties payable, both Government and private.*	The economic analysis in support of these Ore Reserves was based on total operating costs. Mining costs applied in the optimisation used the existing Karlawinda Gold Project mining contract rates with logical extrapolations of the existing rates to the extension of the open cut required for changes to the Ore Reserve. The costs have been modified by rise and fall. Drill and blast costs were derived by applying contract costs, expected patterns and powder factors and cross checking these with drill and blast costs to date, and modified by rise and fall. Grade control costs were derived from existing grade control drilling and sampling costs. No transportation charges have been applied in economic analysis. Ore is delivered directly from the pit to the ROM beside the existing plant at contract rates. Gold transportation costs to the Mint are included in the refining component of the milling charges. Treatment costs applied in the Ore Reserve analysis are actual costs from processing of ore. No allowance is made for deleterious elements since testwork to date on ore from Bibra has not shown the presence of deleterious elements. Administration costs are based on actual costs from the operation. All financial analyses and gold price have been expressed in Australian dollars so no direct exchange rates have been applied. An allowance has been made for all royalties, including an allowance of 2.5% of revenue for royalties payable to the Western Australian State Government and a 2% allowance for the current commercial royalty to a third party. The terms of the royalty payable to the other private party is covered by confidentiality restrictions.
Revenue factors	• *The derivation of, or assumptions made regarding revenue factors including head grade, metal or commodity price(s) exchange rates, transportation and treatment charges, penalties, net smelter returns, etc.* • *The derivation of assumptions made of metal or commodity price(s), for the principal metals, minerals and co-products.*	The mined ore head grades are estimated utilising industry accepted geostatistical techniques with the application of relevant mining Modifying Factors. Gold price and exchange rates have been determined by Capricorn on the basis of current market trends and by peer company comparison. A$1,800/oz is used for the open pit optimisation and lower-cut calculation for the Ore Reserve estimation process. A higher revenue factor shell of A$1,900/oz was selected as the guide to the final pit design limits. The financial model is run at A$2,500/oz, and 165 koz are hedged at A$2,250/oz.
Market assessment	• *The demand, supply and stock situation for the particular commodity, consumption trends and factors likely to affect supply and demand into the future.* • *A customer and competitor analysis along with the identification of likely market windows for the product.* • *Price and volume forecasts and the basis for these forecasts.* • *For industrial minerals the customer specification, testing and acceptance requirements prior to a supply contract.*	There is a transparent market for the sale of gold.

Criteria	JORC Code explanation	Commentary
Economic	• *The inputs to the economic analysis to produce the net present value (NPV) in the study, the source and confidence of these economic inputs including estimated inflation, discount rate, etc.* • *NPV ranges and sensitivity to variations in the significant assumptions and inputs.*	Inputs from the open pit mining, processing, sustaining capital and contingencies have been scheduled and costed to generate the cost estimate. Cost inputs have been estimated from actual costs, quotations and/or by competent specialists. The Ore Reserve returns a positive NPV based on the assumed commodity price of A$2,500/oz and the Competent Person is satisfied that the project economics that make up the Ore Reserve retains a suitable profit margin against reasonable future commodity price movements. Sensitivity analysis has indicated that the project drivers are gold prices, grade, metallurgical recoveries followed by operating costs; NPV remains favourable for the sensitivity tests within reasonable ranges.
Social	• *The status of agreements with key stakeholders and matters leading to social licence to operate.*	A Native Title Access Agreement has been signed for the Project (ASX Announcement 24 Nov 2016). After the Native Title Access Agreement, a Mining Lease was granted over the project area (ASX Announcement 24 Nov 2016) and several Miscellaneous Licences to cover the infrastructure corridors have been granted.
Other	• *To the extent relevant, the impact of the following on the project and/or on the estimation and classification of the Ore Reserves:* • *Any identified material naturally occurring risks.* • *The status of material legal agreements and marketing arrangements.* • *The status of governmental agreements and approvals critical to the viability of the project, such as mineral tenement status, and government and statutory approvals. There must be reasonable grounds to expect that all necessary Government approvals will be received within the timeframes anticipated in the Pre-Feasibility or Feasibility study. Highlight and discuss the materiality of any unresolved matter that is dependent on a third party on which extraction of the reserve is contingent.*	Flooding risk has been analysed by an independent external expert and deemed to be minimal, with the project located near the top of a small catchment system. No significant species have been identified that would be significantly impacted by the Project in a manner that could not be adequately managed. Construction of the project was completed in June 2021.
Classification	• *The basis for the classification of the Ore Reserves into varying confidence categories.* • *Whether the result appropriately reflects the Competent Person's view of the deposit.* • *The proportion of Probable Ore Reserves that have been derived from Measured Mineral Resources (if any).*	The main basis of classification of Ore Reserves is the underlying Mineral Resource classification. All Probable Ore Reserves derive from Indicated Mineral Resources in accordance with JORC Code (2012) guidelines. The results of the Ore Reserve estimate reflect the Competent Person's view of the deposit. No Probable Ore Reserves are derived from Measured Mineral Resources. No inferred Mineral Resource is included in the Ore Reserves.
Audits or reviews	• *The results of any audits or reviews of Ore Reserve estimates.*	An internal review of the Ore Reserve estimate has been carried out.
Discussion of relative accuracy/ confidence	• *Where appropriate a statement of the relative accuracy and confidence level in the Ore Reserve estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the reserve within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors which could affect the relative accuracy and confidence of the estimate.*	In the opinion of the Competent Person, cost assumptions and modifying factors applied in the process of estimating Ore Reserves are reasonable. Gold price and exchange rate assumptions were set out by Capricorn and are subject to market forces and present an area of uncertainty.

Criteria	JORC Code explanation	Commentary
	• *The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.* • *Accuracy and confidence discussions should extend to specific discussions of any applied Modifying Factors that may have a material impact on Ore Reserve viability, or for which there are remaining areas of uncertainty at the current study stage.* • *It is recognised that this may not be possible or appropriate in all circumstances. These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.*	